

**FASTER-III,  
A GENERALIZED-GEOMETRY MONTE CARLO  
COMPUTER PROGRAM FOR THE TRANSPORT  
OF NEUTRONS AND GAMMA RAYS**

**VOLUME II -USERS MANUAL**

**by**

**T. M. Jordan**

**prepared for**

**NATIONAL AERONAUTICS AND SPACE ADMINISTRATION**

**CONTRACT NAS3-14400**

**NOVEMBER 1970**

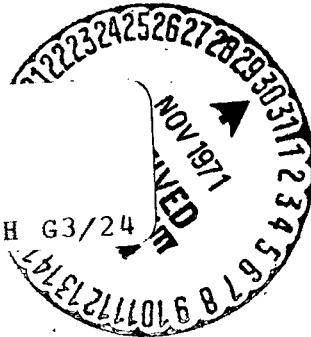
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Technical Management  
NASA Lewis Research Center  
Cleveland, Ohio  
Millard L. Wohl

A.R.T. RESEARCH CORPORATION  
1100 Glendon Avenue  
Los Angeles, California 90024

## **ABSTRACT**

A description of the FASTER-III program for Monte Carlo calculation of photon and neutron transport in complex geometries is presented. Major revisions include the capability of calculating minimum weight shield configurations for primary and secondary radiation and optimal importance sampling parameters. The program description includes a users manual describing the preparation of input data cards, the printout from a sample problem including the data card images, definitions of Fortran variables, the program logic, and the control cards required to run on the IBM 7094, IBM 360, UNIVAC 1108 and CDC 6600 computers.

## Section 1

### INTRODUCTION

The FASTER-III program is designed for accurate calculations of photon and neutron fluxes at specified points in a complex geometry. Alternatively, the program will compute fluxes averaged over specified regions and surfaces of the geometry. The Monte Carlo method is employed in the generation and tracking of particle histories. Importance sampling is employed in all the random sampling phases of the particle histories to minimize the variance of calculated fluxes.

The program is designed to permit the user to prepare data for the most simple or complex problem with very little data manipulation other than entering numbers on data cards. The most simple problem would require the compositions and microscopic cross sections for the materials, the radiation source description, the equations for the surfaces bounding material regions, the description of the material regions, and the locations of the detectors. More complex problems may involve multiple radiation sources, optional outputs such as the flux by order-of-scatter, user-supplied importance sampling parameters, etc..

Among the many options available to the user is the capability of performing minimum weight shield calculations for rectangular, cylindrical, and/or spherical shield systems subject to specified constraints on primary and secondary response functions. The program will also calculate, as an option, optimal values of importance sampling parameters which can then be used in subsequent similar problems.

## Section 2

### PROGRAM DOCUMENTATION

The documentation for the program is detailed in the appendices to this report. This provides the most flexibility for any additions, modifications and corrections.

#### 2.1 Data Preparation

The instructions for preparing data cards are given in Appendix A. The input data has been divided into many "input sections". The user supplies only those sections necessary to describe a problem. Alternatively, for multiple problem runs, only those input sections which change are input.

The program will accept data cards in either fixed-field or variable-field formats as outlined in Appendix A. The printout from the problem includes the data card images for a permanent record of the problem input.

The discussion of the input sections includes information on how to interpret any printout resulting from that input.

#### 2.2 Sample Printout

The complete printout from a sample problem is contained in Appendix B. The printout includes the data card images. The data cards include numerous comments which should help relate the input data to the input instructions in Appendix A.

#### 2.3 Fortran Variables

The fixed location integer and real variables are stored in named common blocks. These variables are defined in Appendix C. Many of the variables are the starting location, in blank common, of variable-dimensioned arrays. The definitions of these

location variables includes the name and dimensionality of the associated array.

#### 2.4 Program Logic

The program logic for data input and particle tracking is shown in Appendix D. This appendix also includes a short discussion of the role played by each of the subprograms.

#### 2.5 Machine Considerations

Appendix E lists the control cards required for a compile and execute on the IBM 7094, IBM 360, UNIVAC 1108 and CDC 6600 computers. This appendix also gives the procedure for converting from single to double precision and for making installation-dependent changes such as input and output unit designations.

## Appendix A

### INPUT INSTRUCTIONS

This appendix details the preparation of input data for the program. The printout resulting from the various inputs is also described. An understanding of the program logic may clarify the role played by various inputs. This logic is discussed in Appendix D, Program Description.

#### 1. Input Logic

The data required by the program has been divided into many "input sections". Each input section is classified as, belonging to one of the following general categories:

- 1) Material properties -- compositions, cross sections, etc.
- 2) Source distributions -- spatial, angular, energy, etc.
- 3) Geometry -- bounding surfaces, material regions, etc.
- 4) Output requests -- detectors, response functions, edits, etc.
- 5) Importance sampling -- scaling parameters, energy importance, etc.
- 6) Control -- execute, stop, define tapes, etc.

Each category includes one or more input sections.

The general order of input should follow the above pattern. While the input section order is not always critical, there are instances where one input section defines parameters which

are essential to the correct processing of data in a subsequent input section. If the input order given in this manual is adhered to, no problems of this nature will occur.

The reason for dividing the data into so many input sections is to simplify the setup of multiple-case problems. Thus, each case uses the data of the previous case except for parameters changed through one or more input sections.

The program has been designed so that all input data will be scanned for errors. Thus, if any input errors are detected by the program, an error indicator is set and a message is entered on the printout. The problem will not be run if any errors are detected. However, processing of input will continue as long as no unforeseen catastrophic error occurs.

Most error messages are associated with particular input sections and are discussed in conjunction with the instructions for those sections. One error, however, which can occur in many of the input sections has to do with data storage allocation.

In general, all data arrays are packed into blank common using variable dimensioning techniques. The length of blank common is sufficient for fairly complex problems. However, unusually large problems -- particularly problems which request many of the optional output edits -- may exceed the available storage.

The error message associated with insufficient storage is

NØGØ\*DATA REQUIRES IJKL LOCATIONS\*NØGØ

where IJKL represents the computed storage requirement.

Once the available storage is exceeded, the program scans the rest of the input only to the extent necessary to determine

the maximum storage requirement for the problem. The user is then able to decide whether to decrease the problem size or go to a more spacious computer.

An error which may occur on multiple-case problems has to do with manipulating arrays whose dimensions have changed. The program attempts to preserve the array so that all old elements within the new limits are preserved. All old elements outside the new limits are discarded and any new elements outside the old limits are given a value of zero.

If storage is tight, there is insufficient room to perform the above process and elements may not be preserved. The error message is

NØGØ\*STØRAGE CØNFLICT ØN ARRAY XYZ\*NØGØ

where XYZ denotes the name of a data array.

Editing of input continues but the problem will not be run.

If this problem occurs, it can be circumvented by setting up the problem as an independent case, i.e., the difficulty can only occur on change case problems.

## 2. Input Sections

The various input sections have several common features in terms of card input and the internal machinations of the program. In particular, each input section is signaled to the program by a "header card". The header card for each input section has a unique three letter "identifier" in card columns 1-3. For example, the data section for describing the radiation SØUrce has the identifier SØU. The remainder of the header card may be blank or contain any mixture of alphanumeric data.

Until the input process is terminated, e.g., by the Stop input section, the program searches for a header card with a recognized identifier. At the commencement of the search, a line of asterisks is entered on the printout. Data cards are then read, scanned for the identifier, and if no identifier is found, printed as a "comment card". These lines of printout have the form:

CARD IMAGE \*\*\*.000.XXX.H

card image

The value of XXX is a serial numbering of the comment cards since the search for a header card started. The H indicates the header card input format. If a new printout page is started during the search another line of asterisks is printed at the top of the page.

This search for the input section identifier has several convenient features. It permits the entering of any number of comment cards into the printout for later identification. It allows the program to quit processing a particular input section because of an error condition and proceed to the next input section. It also permits continued input processing when the number of data cards in an input section is not correct.

When a valid header card is recognized two lines are entered on the printout.

\*\*\*\*\*1234567890123....890

CARD IMAGE ABC.000.001.H

card image

where ABC denotes the input section identifier, 000 denotes the zeroth input statement of section ABC, 001 denotes the first card for the zeroth input statement, and H denotes input via the header card format.

The remainder of the data cards in the recognized input section will then be printed unless a "no print" flag was turned on by prior processing of the PRInt input section.

If a new printout page is started after the header card is found, and before the search starts for the next input section, two lines are entered on the printout, a line of asterisks, and a line identical to the one printed over the header card.

After the header card is recognized, the data cards must correspond to the detailed input formats for that input section. In particular, the first data card following the header card in every input section must be the "option card". The option card contains integer data representing input option flags, other options, and array limits. None, one, or more data cards may follow the option card depending on the data section and the input option flags. The option card will always appear on the printout immediately below the header card as

CARD IMAGE ABC.001.001.I

card image

where ABC denotes the input section, the first 001 denotes the first input statement following the header card, the second 001 denotes the first card of that input statement, and the I denotes an integer format interpretation of the card.

The following logic is employed on all option cards. The first integer word IN1, on the option card tells the program whether the limits and options (if any) for that input section should be interpreted from third and following fields on the card. If  $IN1 \leq 0$ , they are not interpreted. If  $IN1 > 0$ , they

are interpreted unless the input section does not involve any. Normally, IN1 would be greater than zero on the first case. IN1 would be zero on a change case where the limits and options from the previous case still apply.

The second integer word, IN2, on the option card tells the program whether subsequent data cards (if any) for that input section will be input. The general procedure here is if IN2=0, no other input is provided for the input section and, if IN2>0, input is provided (unless that input section has no other input). In some instances, IN2 may also denote the quantity of input, e.g., the number of material regions being described.

In a few instances IN2<0, may tell the program to compute the remainder of the input with no additional data cards for the input section. In particular, this is the case for all of the importance sampling parameters. The importance sampling parameters will also be computed if they are never input for any case.

After the option card has been fully interpreted according to the defined input section, storage is then allocated, according to the latest maximum dimensions, for all data arrays (if any) associated with input data. If the data will fit, the remainder of the cards for that section are interpreted. If the data will not fit the program generates the following error message

**\*\*\*INPUT SECTION DATA LIST, INSUFFICIENT STORAGE FOR ACTUAL INPUT\*\*\***

The search for the next input section then commences.

Several other error messages may be generated during the processing of an input section. If another input section must be processed first, the following message appears

NØGØ\* ABC INPUT SECTION MUST BE INPUT BEFORE THE XYZ INPUT SECTION  
\*NØGØ

and the search for the next input section commences. If the

input section involves any ordered arrays and inversions in the order of the array elements are detected the following message is generated

NØGØ\* N INVERSIONS IN THE FØLLØWING DATA \*NØGØ

The array is then listed with the label ERROR ARRAY appended at the left side of each printout line.

Several of the input sections involve user-supplied indices on which data is stored. If one of these indices is outside the permissible range established by input limits, the following message is printed

NØGØ\* I IS ØUTSIDE THE RANGE 1-IMAX \*NØGØ

where IMAX is the upper limit on I. The value of I is set to one by the program and input continues.

### 3. Fixed Field Input Formats

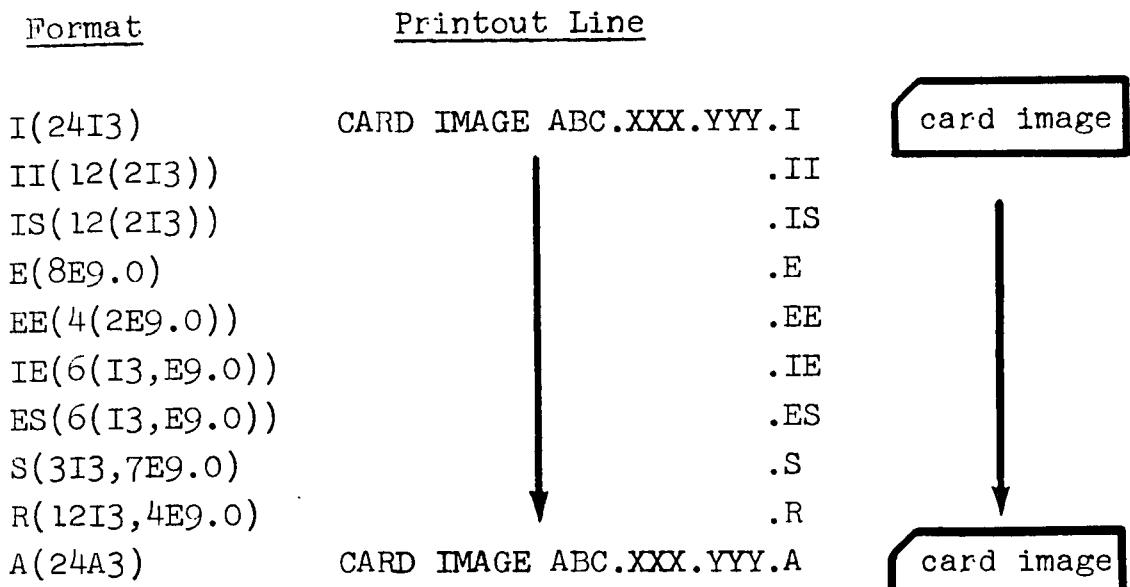
The program uses a variety of fixed field formats for input data. These formats have varying combinations of the following data fields:

I3 field (3 card columns), integer data

E9.0 field (9 card columns), decimal data

Only card columns 1 through 72 are used for the data fields.

The formats and the appearance of the corresponding printout for a card read by that format are summarized below:



I denotes an all integer format with a maximum of 24 integers on the card, E denotes an all decimal format with 8 pieces of data per card. The II and EE indicate formats where the data is input as logical pairs, e.g.,  $[x_i, f(x_i)]$ ,  $i = 1, 2, \dots$ . The IS and ES formats are used for logical pair input where the first number of the pair is the index of the second number, e.g.,  $[i, f_i]$ ,  $j = 1, 2, \dots$ . The S and R formats were so designated because they were first used for the description of surfaces and regions respectively.

All alphanumeric data is entered in a 24A3 format, 3 columns per data word, 24 words per card. If alphanumeric data is read during the header card search, the format is designated H.

If such data is read as a normal part of the data for an input section it would appear as the A format shown above.

The ABC in the printout line indicates the input section as mentioned before, XXX is an internal serial number for the input statements encountered in section ABC, and YYY is the serial number of the physical data cards input via input statement XXX.

Now, as to why all the card images have the information SECTION.INPUT STATEMENT.CARDCOUNT.FORMAT appended to them. With the exception of alphanumeric data which is always fixed field, the integer and decimal data are actually interpreted via a variable field format to be described later. Since the resulting printout line contains the card image, it is impossible to tell how the card is interpreted unless a catastrophic error causes the program to bomb off the machine while giving a reverse call sequence. By scanning the printout with the appended information it becomes rather easy to verify that the card was interpreted in the correct input section via the correct format, and, with a little more effort, that the interpretation occurred with the proper sequential input statement and card count.

Since a variable format is actually used for interpreting the integer and decimal data from the card image, one relaxation in the ASA standards has been made. Namely, all leading and trailing blanks in a data field are ignored rather than being treated as zeros. Therefore, integers, including the exponents of decimal data, do not need to be right adjusted in the data field. Embedded blanks are treated as zeros in the usual manner.

#### 4. Variable Field Input Formats

The program will also accept integer and decimal data in a variable length field format. Alphanumeric data is always entered in the fixed A3 field of the H and A formats.

The data formats given in the detailed input instructions correspond to using the fixed field input. The use of the variable length field is signaled to the program by a comma in the first column of the data card. The absence of the comma therefore indicates the use of the fixed field format for that card. With appropriate care, the two formats can be used interchangeably even within a multiple card input statement.

The rules followed in preparing variable length field data are summarized below:

- a) Card column 1 must contain a comma (,),
- b) before any data is interpreted from the card, the locations receiving the data are filled with zeros except for the IS and ES formats where the locations are not defined,
- c) data fields are separated by commas,
- d) a slash (/) indicates immediate termination of input for the input statement -- equivalent to a zero fill, except for the IS and ES formats, due to b) above,
- e) any number of blank columns -- including none -- between two commas is interpreted as a minus zero,
- f) data is entered only in card columns 1 through 72,

- g) the comma in card column 1 in multiple card input statements should be visualized as a comma in column 73 of the preceding card, i.e., the multiple cards should be visualized as one long card

1	72-73	144-145	216-217
,	,	,	,

card 1            card 2            card 3            card 4 ...

e.g., a comma in column 72 of one card followed by a comma in column 1 of the next card is equivalent to inputting one piece of data interpreted as a minus zero,

- h) data lists on a card exceeding the list length of the input statement are assumed to belong to the next input statement,
- i) a slash followed by a comma (/,) terminates input for the present input statement but signifies the next input statement will continue interpreting data from the same card; anything else after the slash indicates the next input statement will start with the next card,
- j) if a slash is not followed by a comma, the remainder of the card is ignored and can be used for comments,
- k) the program has a repeat feature such that if an asterisk (\*) is encountered between two consecutive commas on the same card the columns preceding the asterisk are the number of entries (a minimum of 1) of the columns following the asterisk; this repeat

option can be used to non-zero fill since the repeat does not continue into the next input statement and the repeat is truncated -- without an error indication -- if the number of repeats exceeds the length of the input statement list,

- 1) all alphanumeric data is entered in a fixed field format starting in column 1.

Comment cards can be placed anywhere in a data deck except immediately preceding A format alphanumeric data cards.

Comment cards should contain a C in column 1 and column 2 should be blank. The remainder of the columns can contain any combination of alphanumeric information.

There are two error messages which are generated during the interpretation of data cards. Either error will suppress the execution of the problem even though the input will continue. The first message has to do with non-numeric data within the field

NØGØ\*INVALID PUNCHES IN CØLUMNS II-JJ ØF CARD ABC.XXX.YYY.F\*NØGØ  
where F is the card format under which the card was originally interpreted (with variable field input, various formats may be used on the same physical card). An invalid punch is interpreted as a zero.

The second message has to do with the exponent of decimal data

NØGØ\*THE ABSØLUTE VALUE ØF THE EXPØNENT IN CØLUMNS  
II-JJ ØF CARD ABC.XXX.YYY.F EXCEEDS ZZ\*NØGØ

where ZZ is presently 38. The exponent is then fixed in magnitude at 38 with the correct sign.

##### 5. Input Section Formats

The remainder of this section covers the detailed input instructions for the input sections available to the user

of the program. The header card identifiers are listed in Table A.1 in the same order as they appear in the instructions. The same order should be used in supplying data with the obvious exception of the control input sections. Control input sections should be supplied in the order the user wants the control functions performed with respect to the other input sections.

In the description of individual cards in an input section, each card is given an identification of the form ABC.XX.F(format) where ABC denotes the input section identifier, XX denotes a serial number, and F denotes a format type. Note that the serial numbering system used on the input section card description is not necessarily the input statement number printed out when the card is input. It will be for most input sections, however.

After the card identification is given, a few words are used to give the card a more meaningful title. Below this, the data on the card are then described. If the data are all of the same type there may be a simple explanation of what the data is, its units (if any), and the order in which it is input. If the data on the card have different functions then the data words are numbered consecutively as they appear on the card and are then described individually.

If variable length input formats are being used, it should be noted that the option card input statement expects 24 integers. These and other input statement list lengths are given in the input instructions.

PRECEDING PAGE BLANK NOT FILMED

TABLE A.1  
LIST OF INPUT SECTIONS

ZERout Core  
TAPe Units  
LABEL for Printout  
MATERIAL Compositions  
MIXture Table  
GAMma Ray Cross Sections  
PHoton Cross Sections  
MULTigroup Neutron Cross Sections  
NEUtron Cross Sections  
SECondary Production Cross Sections  
ADDress Modification  
SOURce Distributions  
PRfiles of Source Time Dependence  
SURfaces  
HELical Surfaces  
REGions  
CYLindrical Geometry  
SPHerical Geometry  
AIR Density  
CHEck Ray Trace  
COrrelated Calculations  
DETectors  
FLUX Groups  
RESPonse Functions  
BIRth Regions  
ORDer of Scatter  
SCATTERing Regions  
BOundary Crossings  
ANGular Fluxes

TABLE A.1 (Cont'd)

Solid Angle Fluxes  
TRANslation Time  
MOMents of Temporal Fluxes  
TIME Interval Fluxes  
GRoup Edit on Fluxes  
NORMal Derivatives  
MINimum Weight Shield  
DEPosition in Regions  
LEAkage of Energy  
CHANnel Detectors  
NISE Functions  
PLot Output  
QUIck Plot of Results  
OPTimum Importance Parameters  
BIAsing Options  
PSEudo Spherical Source  
RELative Source Importance  
RATios of Source Variable Importance  
PREferred Point  
SPAtial Importance  
CAPture Importance  
SHort Circuit  
ROTate and Translate  
ARRay Direct Input  
DUMP Requests  
PRInt Suppression  
NEXT Case  
EXECute the Problem  
CONTinue a Previous Run  
STOP Processing

ZERout Core

This section permits a complete erasure of all data in core so that only subsequent data cards define the succeeding problem. The random number generator is not reset, so a different random number sequence will be used for the subsequent problem than would be used if the problem were actually the first problem in this run.

ZER.O.H(24A3) Header Card

Must have ZER in columns 1-3.

ZER.l.I(24I3) Option Card

1.-24. Input but not used.

## TAPe Units

This section defines the logical designations of any tape units used by the program.

### TAP.O.H(24A3) Header Card

Must contain TAP in columns 1-3.

### TAP.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-8 from this card.

2. IN2, not used.

3. M3, logical designation of the cross section tape unit

4. M4, logical designation of the restart tape unit.

5. M5, logical designation of the collision tape unit.

6. M6, logical designation of the secondary source tape unit.

7. M7, logical designation of the census tape unit.

8. M8, logical designation of the scratch tape unit.

9.-24. Input but not used.

A zero indicates the tape unit is not used. Supply a zero tape unit designation unless directed otherwise in the input instructions for the remainder of the problem.

Affixing a minus sign to a nonzero unit designation means that unit will not be rewound when this card is read. All positively designated units will be rewound.

### LABel for Printout

This section provides for entering two lines of descriptive information at the top of each printout page. If not used, the printout headings will contain asterisks.

#### LAB.0.H(24A3) Header Card

Must have LAB in columns 1-3.

#### LAB.1.I(24I3) Option Card

1. IN1, not used.

2. IN2, (0,>0)=(no,yes) cards LAB.2 and LAB.3 are input.

3-24. Input but not used.

#### LAB.2.A(24A3) First Label Card

Any mixture of alphanumeric data.

#### LAB.3.A(24A3) Second Label Card

Any mixture of alphanumeric data.

## MATERIAL Compositions

This input section defines the number of different material compositions to be used in this and possibly succeeding problems. More materials can be defined than are actually designated later to be located in specific regions.

The definition of the compositions requires the input of the constituent isotopes or elements and their partial density in each material.

The compositions are defined independent of the microscopic cross sections since the composition data may be used in forming macroscopic cross sections for more than one radiation type in a given computer run.

The order in which element data is provided here must also be followed in later supplying the microscopic cross section data.

### MAT.O.H(24A3) Header Card

Must have MAT in columns 1-3.

### MAT.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret limits and options from this card, data words 3, 4, and 5 below.
  2. IN2, (0,>0)=(no,yes) data cards MAT.2 are being input.
  3. NIMAX, number of elements and/or isotopes.
  4. NMMAX, number of materials to be formed from the elements.
  5. NUNITD, (0,1)=( $10^{24}$  atoms/cc, gram/cc) partial density units option.
- 6.-24. Input but not used.

MAT.2.E(8E9.0) Compositions

Supply this card for each element  $I=1,2,\dots, NIMAX$  starting a new card for each element.

1. ATW( $I$ ), atomic weight of element  $I$  (amu)

2. ATN( $I$ ), atomic number of element  $I$

3. ATD( $1,I$ )  
•  
•  
•  
ATD( $NMMAX,I$ ) } , density of element  $I$  in material 1,  
material 2, ..., through material  $NMMAX$

NOTES:

The partial densities for each material should sum to the correct reference density for the material. These densities can then be scaled in the geometry description to account for regions which have a lesser or greater density. For example, the compositions for all materials can be specified to yield a reference density of 1.0 gm/cc. Then the geometry description would include density scale factors equal to the actual density in each region.

### MIXture Table

This input section is used to set up a table of materials for which only the hydrogen content varies from specified materials described in the MATERial input section. This capability is provided for neutron and photon problems only.

#### MIX.O.H(24A3) Header Card

Must have MIX in columns 1-3.

#### MIX.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
  2. IN2, (0,>0)=(no,yes) card MIX.2 is being input.
  3. MIXED, total number of mixtures to be formed.
  4. NUNITD, (0,1)=( $10^{24}$  atoms/cc, grams/cc) hydrogen density units.
- 5.-24. Input but not used.

#### MIX.2.IE(6(I3,E9.0)) Mixtures

Supply MIXED pairs of data. The first member of the pair is an integer denoting the basic material comprising the mixture -- a zero indicates none. The second member of each pair is a decimal number giving the hydrogen content-- replacing the hydrogen content in the base material--of the mixture with units according to NUNITD above.

The mixtures defined through this data are given material indices of NMMAX+1, ..., NMMAX+MIXED, where NMMAX is the number of basic materials.

### GAMma Ray Cross Sections

This input section provides the microscopic cross section data necessary for tracking gamma rays. This data includes the number of energy groups to be used in this problem, the energy group boundaries, and the microscopic total cross section data for each element described in the MAT input section.

#### GAM.0.H(24A3) Header Card

Must have GAM in columns 1-3.

#### GAM.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret limits and options from this card, data word 3 below.
2. IN2, (0,>0)=(no,yes) data cards GAM.2, etc. are being input.
3. NEPMAX, number of photon energy groups.
- 4.-24. Input but not used.

#### GAM.2.E(8E9.0) Energy Groups Boundaries

This card gives the energy group boundaries in Mev in order of decreasing energy, ELP(1), ELP(2), ..., ELP(NEPMAX+1). The cross section data below can be input at different energy points and is then log-log interpolated to get cross sections at these energy points.

Supply a set of cards GAM.3, GAM.4, ... for each element, I=1, 2, ..., NIMAX, in the same order as the compositions were input.

GAM.3.I(24I3) Element Option Card

1. LRL $\emptyset$ PT=0, total cross sections are read on card GAM.5 for energy points defined according to NETAB below.  
LRL $\emptyset$ PT=1, total cross sections are input via card GAM.6 at energy points defined on card GAM.6.
2. NUNITX,(0,1)=(barns/atom,cm<sup>2</sup>/gm) cross section unit option.
3. NETAB < 0, cross section input energy points are the same as those on the GAM.2 card.  
NETAB=0, energy points are the same as for the previously input element.  
NETAB>0, energy break points are input via card GAM.4 below.  
NETAB is not used if LRL $\emptyset$ PT=1.
4. MX, number of points in the total cross section input.
- 5.-24. Input but not used.

GAM.4.E(8E9.0) Energy Points

Supply this card if NETAB>0, with NETAB energy points in Mev using decreasing energies.

GAM.5.E(8E9.0) Cross Sections

Supply this card if LRL $\emptyset$ PT=0 with MX microscopic total cross sections for the first MX GAM.2 energy points or the first MX GAM.4 energy points, XST(1), XST(2), ... XST(MX).

GAM.6.EE(4(2E9.0)) Energies and Cross Sections

Supply this card if LRL/PT=1 with MX pairs of energy and cross section, ETP(1), XST(1), ETP(2), XST(2), ..., ETP(MX), XST(MX).

## PH $\emptyset$ ton Cross Section

This input section provides microscopic photon cross section data. Input includes the photon energy group structure. Cross section data are tabulated for a separate energy point table and are log-log interpolated to obtain the data for the photon energy group boundaries. During calculations, linear interpolation is used for intermediate energies.

Cross section data for the elements must be supplied in the order associated with the MATerial compositions.

### PH $\emptyset$ .O.H(24A3) Header Card

Must have PH $\emptyset$  in columns 1-3.

### PH $\emptyset$ .1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-5 from this card.

2. IN2, (0,>0)=(no,yes) cards PH $\emptyset$ .2, etc. are being input.

3. NEPMAX, number of photon energy groups.

4. NF $\emptyset$ RM, number of points in the tabulated form factors for coherent and Compton scattering.

NF $\emptyset$ RM=0, coherent scattering is neglected; all electrons are assumed free.

5. NEDGES, maximum number of photoelectric edges for any element.

NEDGES=0, the photoelectric process is neglected in the generation of florescence and/or photoelectrons.

6.-24. Input but not used.

PHØ.2.E(8E9.0) Energy Groups

Photon energy group boundaries are supplied in Mev and descending values, ELP(1), ELP(2), ..., ELP(NEPMAX+1).

PHØ.3.E(8E9.0) Form Factor Argument

Omit this card if NFØRM=0. Supply NFØRM values of the electron momentum ( $q$ , dimensionless), increasing values, at which form factor data will be tabulated. See cards PHØ.7 and PHØ.8 for more detailed discussion.

Supply PHØ.4, etc., cards in sets; one set per element.

PHØ.4.I(24I3) Element Option Card

1. LRLØPT=0, microscopic cross sections are input for the energies defined through data word 3 below.

LRLØPT=1, energy points and cross sections are input in logical pairs; four pairs per card,  $E_i$ ,  $\sigma_i$ ,  $i = 1, 2, \dots$

LRLØPT=2, energy points are input starting on one set of cards  $E_i$ ,  $i = 1, 2, \dots$  followed by cross sections starting on another set of cards,  $\sigma_i$ ,  $i = 1, 2, \dots$

2. NUNITX, (0,1)=(barns/atom, cm<sup>2</sup>/gm) cross section units.

3. NETAB, used only if LRLØPT=0.

NETAB<0, energy points for input are identical to card PHØ.2 data.

NETAB=0, energy points defined for the previous element are used for input data.

NETAB>0, energy points are being input.

4. MXST, points in total cross section. If not input, MXST=0, the total cross section is calculated by summing partial cross sections as defined below.
5. MXSI, points in incoherent scattering (Compton). If not input, MXSI=0, the cross section is computed internally neglecting electron binding effects.
6. MXSC, points in coherent scattering (Rayleigh). If not input, MXSC=0, the cross section is set to zero, consistent with the Compton option above.
7. MXSP, points in pair production data. Cross section set to zero if MXSP=0.
8. MXSE, points in the photoelectric data. Cross section set to zero if MXSE=0.
9. MEDGES, number of edges for this element.
10. MXCOM, (0,>0)=(no,yes) Compton form factors are input.
11. MXCOH, (0,>0)=(no,yes) coherent form factors are input.
- 12.-24. Input but not used.

PHØ.5.E(8E9.0) Tabulation Energies

Input this card only if NETAB>0. Supply NETAB energies (Mev) in descending values.

PHØ.6.{ E{8E9.0} } Microscopic Cross Sections  
{EE{4(2E9.0)}

Input card PHØ.6 for each cross section type for which the input list length, data words 4 through 8 above, is greater than zero. Input in that order according to the discussion

for LRLOPT and NETAB on card PHØ.4. Start a new card for each cross section type (and separate tabulation energies if LRLOPT=2).

PHØ.7.E(8E9.0) Form Factor-Incoherent

Omit this card if MXCØM=0. Supply NFØRM values of  $1 - \frac{1}{Z} k(q, Z)$  if MXCØM=1 or  $k(q, Z)$  if MXCØM=2, where  $k(q, Z) = \sum_{i=1}^Z |f_o^{(i)}(q)|^2$

is the form factor as a function of q corresponding to the q points listed on the PHØ.3 card.

$q = \alpha \sqrt{1 - 2\mu\rho + \rho^2}$ ,  $\alpha = E_\gamma / m_o c^2$ ,  $\rho = [1 + \alpha(1 - \mu)]^{-1}$ , and  $\mu$  is the cosine of the photon scattering angle.

PHØ.8.E(8E9.0) Form Factor - Coherent

Omit this card if MXCØH=0. Supply NFØRM values of  $\frac{1}{Z} |F(q, Z)|^2$  if MXCØH=1 or  $F(q, Z)$  if MXCØH=2 where  $F(q, Z)$  is the form factor as a function of momentum corresponding to the q points listed on the PHØ.3 card and  $q = \alpha \sqrt{2(1 - \mu)}$  where  $\alpha$  and  $\mu$  are defined in conjunction with the PHØ.7 card.

PHØ.9.E(8E9.0) Photoelectric Edges

Omit this card if MEDGES=0. Supply four pieces of data for each edge J -- two edges per card -- in the order of increasing edge energy.

EDG(J), edge energy in Mev.

SED(J), edge cross section (maximum) - units according to NUNITX.

$FL\phi(J)$ , fluorescence yield.

$FLE(J)$ , fluorescence energy (Mev).

NOTES:

The photon energy group structure supplied on card PH $\phi$ .2 is also used for the output of photon fluxes unless an alternate output group structure is supplied via the FLUX group input section.

Form factor data consistent with the use of  $MXC\phi M=MXC\phi H=2$  can be obtained for many elements from AFWL-TR-65-171, Volume 1. The values of ETA at which these form factors are tabulated are 137 times the q values expected by this program on card PH $\phi$ .3.

This program will also accept LRL format cross sections. All the above definitions hold except that any of the partial cross sections controlled by data words 4 through 8 will be accepted in the LRL format by affixing a minus sign to the data word. This format contains several integers in columns 1 through 14 of each data card followed by three pairs of energy and cross section in fields of 10 columns each with the energies in ascending order. The first 14 columns of the card are ignored by the program. Data entered using this option is designated as L format data.

## MULTigroup Neutron Cross Sections

This input section provides multigroup cross section data for tracking neutrons. The data includes the number of energy groups and several other limits and options. The data also describes the energy group structure and the microscopic cross sections for each element.

The program has numerous options for processing cross section data, including:

- 1) transport correction or removal of the transport correction from the total and elastic transfer cross sections,
- 2) processing of  $P_2$  cross section data to obtain histogram transfer probabilities which preserve moments and are nonnegative,
- 3) acceptance of DTF-IV format cross section data from either cards or tape.

These and other options are described below.

### MUL.O.H(24A3) Header Card

Must have MUL in columns 1-3.

### MUL.1.I(24I3) Option Card

1. IN1, (0,1)=(no,yes) interpret limits and options, data words 3-10 below.
2. IN2, (0,1)=(no,yes) input data cards MUL.2, etc.

3. NEMMAX, number of neutron energy groups.
4. NØRDER, 1 + order of Legendre expansion of cross section data.
5. NDØWN, 1 + maximum group-to-group transfer from elastic collisions. DTF-IV format data will be collapsed to this value if it is exceeded.
6. INELAS, number of groups from which nonelastic transfer can be initiated.
7. NTRANS, 1 + maximum group-to-group transfer from non-elastic collisions.
8. LFIXUP, (0,>0)=(no,yes) use histogram model for  $P_\ell$  scattering (use it!).
9. MGSLØW, number of groups which will not be treated explicitly. Neutrons scattered into the lowest MGSLØW groups are assumed to slow down locally and the flux from these groups are an estimate only. The estimate is better than a strict Monte Carlo calculation in most cases.
10. NUNITX, (0,1)=(barns/atom, cm<sup>2</sup>/gm) cross section units options.
- 11.-24. Input but not used.

#### MUL.2.E(8E9.0) Neutron Energy Group Boundaries

This card gives the neutron energy group boundaries in Mev in order of decreasing energy, ELM(1), ELM(2), ... ELM(NEMMAX+1).

Supply the following cards in sets, one set for each element,  
 $I = 1, 2, \dots, NIMAX$ , in the same order as was used to input  
material compositions.

MUL.3.I(24I3) Element Option Card - FASTER Format

1. LMAX, 1 + order of Legendre expansion of cross sections for this element. Affixing a minus sign to LMAX indicates the total cross section data which follows has been transport corrected.  $LMAX \leq NORDER+1$ . If  $LMAX=NORDER+1$ , the cross sections are truncated with a correction factor.
2. NDSM, 1 + maximum elastic group transfer for this element.
3. KMAX, number of groups for which inelastic transfer is initiated for this element.
4. KMX(1),  
      :  
      :  
      KMX(J), 1 + maximum group transfer for nonelastic transfer initiated in group J.  
      :  
      :  
      KMX(KMAX)

MUL.4.E(8E9.0) Total Cross Section - FASTER Format

Total (or transport if  $LMAX < 0$ ) cross section for each energy group.

MUL.5.E(8E9.0) Elastic Transfer Cross Sections - FASTER Format

Omit this card for hydrogen. This contains the Legendre coefficients for elastic transfer in the following sequence:

New card - coefficients for  $P_0$  in group transfer, NEMMAX entries.

New card - coefficients for  $P_0$  down 1 group transfer,  
NEMMAX-1 entries.

•  
•  
•

New card - coefficients for  $P_0$  down NDSM-1 groups transfer,  
NEMMAX+1-NDSM entries.

New card - coefficients for  $P_1$  in group transfer, NEMMAX entries.

•  
•  
•

New card - coefficients for  $P_{LMAX-1}$  down NDSM-1 groups transfer,  
NEMMAX+1-NDSM entries.

MUL.6.E(8E9.0) Nonelastic Transfer Cross Sections - FASTER  
Format

Omit this card for hydrogen or if KMAX=0. Nonelastic transfer  
is assumed isotropic and is supplied in the following sequence:

New card - cross sections for transfer from group 1 to groups 1  
through KMX(1).

New card - cross sections for transfer from group 2 to groups  
2 through 2+KMX(2)-1.

•  
•

New card - cross sections for transfer from group KMAX to  
groups KMAX through KMAX+KMX(KMAX)-1.

MUL.7.I(24I3) Element Option Card - DTF-IV Format

1. LMAX, same definition as card MUL.3.
2. NDSM, location of the in group scattering cross section  
in the data table with a minus sign affixed (the minus  
tells the program that the DTF format is being used).

3. KMAX, length of the cross section table for each energy group.
4. IDEL>0, identification of the  $P_0$  cross section array for this element on tape M3 (requires prior input of the TAPE input section).  
IDEL=0, cross section input from cards.
5. MELAST, number of energy groups in input data set.  
Only the first NEMMAX groups are used.  
MELAST=0, NEMMAX group data are assumed to be input.
6. NGTSEC=0, no effect.  
NGTSEC=1, this is a coupled neutron-photon cross section set and, if the SEC input section has been input, the microscopic production cross sections are stripped from the input and added to the macroscopic secondary production cross sections.

7-24. Input but not used.

MUL.8.F(6(I2,A1,E9.0)) Cross sections

This card contains the cross section data in the following order:

$((\sigma_{k,j,\ell}, k=1, \text{KMAX}), j=1, \text{MAX0(NEMMAX,MELAST)}), \ell=1, \text{LMAX})$

A limited version of the DTF format capabilities is provided.  
The following interpretations of the data fields are made:

If all three fields of the triplet I2, A1, E9.0 are blank, no data is assumed. If the first two fields I2, A1 of the triplet are blank and the third field E9.0 is not blank, one

data word is assumed. If the first field I2 is not blank, then the numerical value of this field is assumed to be the number of repeats of the data in the third field. Many other input options are available in the DTF-IV format depending on the entry in the second A1 field of each triplet. These options are not included in this program.

## NEUtron Cross Sections

This input section supplies point value cross sections for neutron transport problems. All cross sections are in barns/atom.

### NEU.O.H(24A3) Header Card

Has NEU in columns 1-3.

### NEU.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-8 from this card.
2. IN2, (0,>0)=(no,yes) cards NEU.2, etc. are being input.
3. NNEMAX, number of energy groups.
4. NAAMAX, number of points used to tabulate anisotropic elastic scattering distributions. These distributions will be linearly interpolated during the calculations.
5. MAXANI, maximum number of energy groups for any element for which elastic scattering is anisotropic in the center-of-mass coordinate system.
6. NANISØ, total number of different anisotropic angular distributions for all elements.
7. NØNELA, maximum number of groups for which nonelastic scattering can occur.
8. NDRØPS, maximum number of groups to which a neutron may be transferred via a nonelastic event.
- 9.-24. Input but not used.

### NEU.2.E(8E9.0) Energy Groups

Supply the neutron energy group boundaries (Mev) in the order of decreasing energy, ELN(1), ELN(2), ..., ELN(NNEMAX+1).

### NEU.2.E(8E9.0) Tabulation Cosines

Omit this card if NAAMAX=0. Supply NAAMAX values of the cosine of the center-of-mass scattering angle in order of increasing cosine.

### NEU.4.I(24I3) Element Options

Supply cards NEU.4, etc. in sets, one set per element in the order associated with the MATerial compositions.

1. LMAX, number of different models to be used in generating the nonelastic transfer matrix. See card NEU.9 for more details.
2. NDSM, number of energy group boundaries with a nonzero, nonelastic scattering cross section.
3. KMAX, number of energy groups for which elastic scattering is anisotropic in the center-of-mass.  
KMAX=0, all elastic scattering is isotropic in the center-of-mass scattering system.
4. KMX(1)  
KMX(J)<0, the anisotropic angular distribution for energy group J is the same as for group K = -KMX(J) where K<J.

KMX(J)>0, the anisotropic angular distribution is input as tabulated data on card NEU.7 at the center-of-mass cosines listed on card NEU.3.

KMX(J)>100, the anisotropic angular distribution is input on card NEU.7 via Legendre expansion coefficients to order  $L = KMX(J) - 101$ , i.e., KMX(J) - 100 coefficients are input (including the  $P_0$  coefficient).

•

•

KMX(KMAX)

#### NEU.5.E(8E9.0) Total Cross Section

The microscopic cross section is input for the energy group boundaries listed on card NEU.2, NNEMAX+1 pieces of data.

#### NEU.6.E(8E9.0) Elastic Scattering Cross Section

Omit this card for hydrogen. The microscopic elastic scattering cross section is input for the energy group boundaries listed on card NEU.2.

#### NEU.7.E(8E9.0) Anisotropic Distribution

Omit this card for hydrogen or if KMAX=0. Start a new card for each energy group J for which KMX(J)>0. Supply these cards in ascending order of energy group indices. The data consists of either values of the distribution at the cosines listed on card NEU.3 (if KMX(J)<100) or Legendre expansion coefficients (if KMX(J)>100). Neither type of data needs to be normalized -- this is done by the program.

#### NEU.8.E(8E9.0) Nonelastic Scattering Cross Sections

Omit this card for hydrogen or if NDSM\*LMAX=0. Supply the nonelastic cross section for the first NDSM energy points listed on card NEU.2.

NEU.9.S/E(3I3,7E9.0/(8E9.0)) Nonelastic Scattering Models

Omit this card for hydrogen or if NDSM\*LMAX=0. Supply LMAX sets of this card containing the following data:

1. NGT=1, evaporation model, distribution of secondary neutron energies is calculated from  $\rho(E') = E' \exp [-E' \sqrt{\alpha/E}]$  (properly normalized, of course).

NGT=2, discrete level model, distribution of secondary neutron energies is calculated from  $\rho(E') = \delta(E-\alpha)$  where  $\alpha$  is the energy level in Mev.

NGT=3, uniform model, distribution of secondary neutron energies is calculated from  $\rho(E') = \frac{1}{E-\alpha}$ ,  $E' \leq E-\alpha$

2. MIN, first primary neutron energy group for which this model is used (any or all models can apply to any or all primary energy groups).
3. MAX, last primary neutron energy group for which this model is used.
4. ALPHA, the numerical value of  $\alpha$  for the selected models.
5. PNE(MIN)  
•  
•  
PNE(J), fraction of nonelastic scattered primary neutrons in energy group J which interact according to the selected models.  
•  
•  
PNE(MAX)

## SEcondary Production Cross Sections

This section provides microscopic cross sections for the production of secondary gamma rays from neutron interactions or secondary neutrons from high-energy gamma ray interactions.

### SEC.O.H(24A3) Header Card

Contains SEC in columns 1-3.

### SEC.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-5 from this card.
2. IN2, (0,>0)=(no,yes) card SEC.2 or SEC.3 is being input.
3. NPEMAX, number of primary energy groups which can initiate secondary production. These are assumed to be the NPEMAX highest energy groups.
4. NSEMAX, number of secondary energy groups in which secondary particles are produced. These are the NSEMAX highest energy groups.
5. NUNITX, (0,1)=(barns/atom,cm<sup>2</sup>/gm) cross section units option..
6. IN6, (0,>0)=(SEC.2,SEC.3) cross section input format.
- 7.-24. Input but not used.

### SEC.2.E(8E9.0) Cross Sections

If IN6=0 input these cross sections in sets, one set for each element in the order associated with the MATerial compositions. The set for each element contains the following data:

New card: for primary group 1, secondary production cross section times the number of secondaries produced in each secondary energy group, NSEMAX pieces of data.

•  
•  
New card: for primary group NPemax, secondary production cross section times the number of secondaries produced in each secondary energy group, NSEMAX pieces of data.

SEC.3.F(6(I2,A1,E9.0)) Cross Sections-DTF Format

If IN6>0, input the cross sections in the DTF-ANISN format in the same order as indicated for card SEC.2. This is the same order produced on punched cards by P0P0P4.

### ADDress Modification

This input section permits a modification of the input data indices on which sources, surfaces, regions, and detectors are entered. Its purpose is to provide a fairly simple means for combining the geometric descriptions of several independent problems into one problem. The use of the ROTate input section may also be required to move portions of the geometry.

#### ADD.1.H(24A3) Header Card

Has ADD in columns 1-3.

#### ADD.2.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-6 from this card.
2. IN2, not used.
3. IAD1, index modifier for any source indices input in the SOURCE or REGION input sections.
4. IAD2, index modifier for any surface indices input in the SURFACE, HELIX, REGION, or DETECTOR input sections.
5. IAD3, region index modifier for any region indices input in the REGION and DETECTOR input sections.
6. IAD4, detector index modifier for any detector indices input in the DETECTOR input section.
7. IAD5, composition index modifier for any non-zero composition indices input in the REGION input section.
- 8.-24. Input but not used.

## SØUrce Distributions

This section defines the spatial, angular and energy distributions of independent radiation sources. The radiation type is determined by the last cross section header card processed.

### SØU.O.H(24A3) Header Card

Must have SØU in columns 1-3.

### SØU.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2>0, number of sources being described via cards SØU.2, etc.

IN2=0, no sources are being input.

3. NVMAX, total number of independent sources.
4. NXMAX, maximum number of points required to tabulate a spatial or angular distribution. A minimum of two points is required for any continuous distribution such as equi-probable azimuthal angles.

5-24. Input but not used.

### SØU.2.R(12I3,4E9.0) Fixed Source Constants

Card SØU.2 is input for IN2 different sources. This card indicates whether cards SØU.3 and SØU.4 are required. If they are required, they are placed immediately behind card SØU.2.

- I, index of source being described,  $1 \leq I \leq NVMAX$ .

The next six variables depend on the source geometry.

	rectangular	cylindrical	spherical
2. NSG(I)	0	1	2
3. NPC(1,I)	x(cm)	r(cm)	$\rho$ (cm)
4. NPC(2,I)	y(cm)	$\theta$ (radians)	$\theta$ (radians)
5. NPC(3,I)	z(cm)	z(cm)	$\mu$
6. NPC(4,I)	$\theta'$ (radians)	$\theta'$ (radians)	$\theta'$ (radians)
7. NPC(5,I)	$\mu'$	$\mu'$	$\mu'$

number of  
tabulation  
points for  
(1 for delta  
function, 2 or  
more for con-  
tinuous, e.g.  
NPC(4,I)=  
NPC(5,I)=2  
for isotropic  
sources)

See Figure SØU.1 for the relationships of the variables.

- MAX, number of energy points or energy groups required to describe the input spectrum. The input spectrum will be regrouped internally to conform to the particle group structure.

- NØRM, spectrum normalization option (the total source strength is carried in the spectrum).

NØRM=0, normalize to total source in particles.

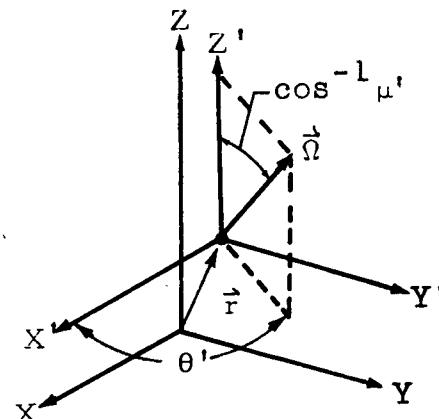
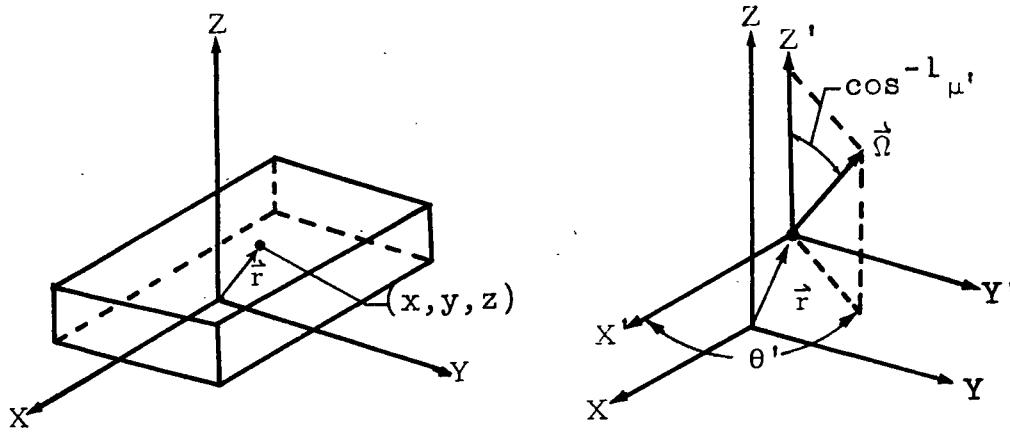
NØRM=1, normalize to total source in Mev.

NØRM=2, multiply spectrum by constant.

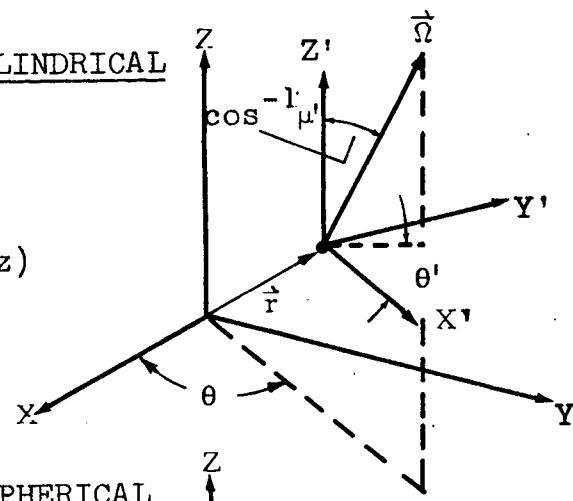
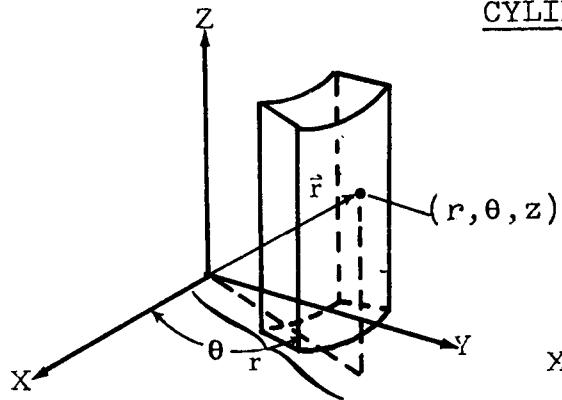
- ISP, input spectrum units option.

ISP=0, differential number spectrum at energy points.

RECTANGULAR



CYLINDRICAL



SPHERICAL

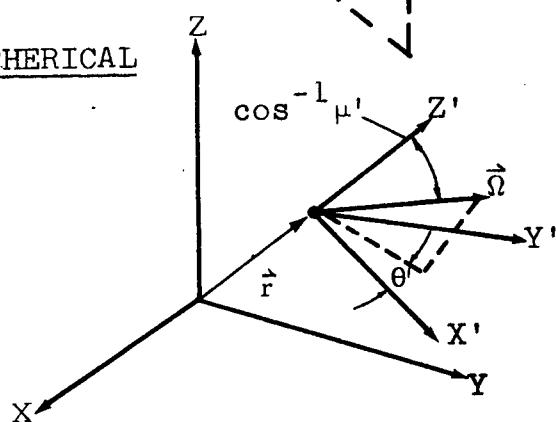
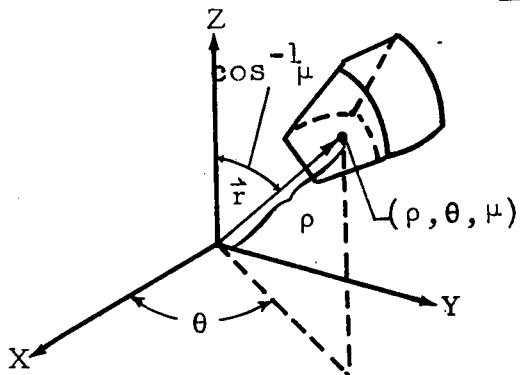


FIGURE SØU-1. SOURCE DISTRIBUTION VARIABLES

- ISP=1, differential energy spectrum at energy points.  
ISP=2, groupwise number spectrum (particles in group).  
ISP=3, groupwise energy spectrum (energy in group).
11. JAL, spectrum format option.
- JAL=0, alternating values of energy points and spectrum.  
JAL=1, spectrum input only using energy previously input  
for this case.  
JAL=2, energy point input (or calculation) followed by  
spectrum input on separate card (or calculation).
12. IDM, internal spectrum generation option.
- IDM=0, no effect.  
IDM=1, calculate energy points and neutron fission spectrum.  
IDM=2, calculate energy points and black body photon  
spectrum.  
IDM=3, calculate energy points and gamma ray fission  
spectrum.
13. T<sub>0</sub>T, source normalization constant, particles if  
NORM=0, Mev if NORM = 1, multiplying constant if  
NORM=2.
14. XTR(1,I), x component of the translation of the source  
coordinate system origin from the geometry coordinate  
system origin (cm).
15. XTR(2,I), y component of the source translation (cm).
16. XTR(3,I), z component of the source translation (cm).

### SØU.3.EE(4(2E9.0)) Source Variable Distributions

A distribution function is input for each of the three spatial,  $J = 1, 2$ , and  $3$ , and the two angular source variables,  $J = 4$ , and  $5$ . The distributions are input in the order indicated on card SØU.2. A new card is started for each variable. Each card contains alternating values of the variable and the relative distribution at the variable, a total of  $NPC(J,I)$  pairs. The first and last values of each variable must be the end points of the range of that variable. The distribution data is normalized internally. To avoid numerical difficulties it is sometimes necessary to decrement the minimum value of a variable and increment the maximum value. In particular, for azimuthal distributions use  $3.1416$  for  $\pi$  rather than  $3.14159$ . A delta function distribution would have one input pair.

In describing multiple sources, several distribution functions may be identical. If this occurs for the  $J^{th}$  source variable simply place the index of the source having the same distribution for its  $J^{th}$  variable in  $NPC(J,I)$  (card SØU.2) and affix a minus sign in front of it. Then omit card SØU.3 for that variable.

### SØU.4.E(8E9.0) Source Spectrum

If  $ISP=0,1$ , the differential spectrum is tabulated at discrete energy points where

$E(1)$  is the maximum spectrum energy (Mev).

⋮

$E(MAX)$  is the minimum spectrum energy.

$EN(K)$  is the differential spectrum corresponding to the  $K^{th}$  energy point  $E(K)$ . The units of  $EN(K)$  are particles/Mev if  $ISP=0$  or Mev/Mev if  $ISP=1$ .

JAL=0, the input on card SØU.4 consists of alternating values of energy and spectrum

E(1), EN(1), E(2), EN(2), ..., E(MAX), EN(MAX).

JAL=1, the energy points are already defined by prior input on card SØU.4 for this case (they will not be available from a previous case). The input consists of the relative spectrum at these points

EN(1), EN(2), ..., EN(MAX).

JAL=2, the energy points are defined first

E(1), E(2), ..., E(MAX).

and then followed by another card with the corresponding spectrum

EN(1), EN(2), ..., EN(MAX).

If ISP=2,3, a groupwise integrated spectrum is tabulated by group where

EBG(1) is the upper energy boundary of group 1.

⋮  
⋮

EBG(MAX+1) is the lower energy boundary of the last spectrum group.

ENG(K) is the integral spectrum for the Kth group with units of particles in group K if ISP=2, or Mev in group K if ISP=3.

JAL=0, the input on card SØU.4 consists of alternating values of energy group boundaries and group spectrum

EBG(1), ENG(1), EBG(2), ENG(2), ..., EBG(MAX),  
ENG(MAX), EBG(MAX+1).

JAL=1, the energy group boundaries are already defined and the groupwise spectrum is supplied on card SØU.4.

ENG(1), ENG(2), ..., ENG(MAX).

JAL=2, the energy group boundaries are defined first

EBG(1), EBG(2), ..., EBG(MAX+1).

and then followed by another card with the groupwise spectrum

ENG(1), ENG(2), ..., ENG(MAX).

The description of multiple sources may involve several sources which have the same relative spectrum. If this source has the same relative spectrum as a previously described source, place the index of that prior source in MAX, affix a minus sign, and omit card SØU.4. If this option is used in conjunction with NØRM=2, remember that the input spectrum of the prior source has already been normalized.

If ISP=0, JAL=2, and IDM>0, the energy points and spectrum are computed internally. If, in this situation, IDM=2, or IDM=3, card SØU.4 is input with one piece of data,  $\alpha$ . The energy points are calculated by subdividing each cross section group so that the total number of energy points is less than or equal to the value of MAX on card SØU.2. The relative spectrum is then calculated at these points as:

IDM=1,  $n(E) = \exp [-E/0.965] \sinh (2.29E)$

IDM=2,  $n(E) = \frac{E^3}{\exp [E/\alpha] - 1.0}$

IDM=3,  $n(E) = \exp [-\alpha E]$

where  $\alpha$  is the black body temperature if IDM=2.

NOTES:

The program assumes the source emits particles at a constant rate per second equal to the total source strength. This assumption is modified in time-dependent versions of the program by time profiles supplied via the PRØfile input section.

## PRØfiles of Source Time-Dependence

This section provides the input description of the time-dependence of the independent sources. The source time profiles are input as histogram distribution functions to simplify the folding of the profiles with the time-dependent fluxes which are calculated assuming a delta function source time-dependence. The distributions are normalized internally.

### PRØ.0.H(24A3) Header Card

Contains PRØ in columns 1-3.

### PRØ.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2, (0,>0)=(no,yes) profiles are input on cards PRØ.2.
3. NPFMAX, total number of time profiles.
4. NPTMAX, number of sections in the time profiles.
- 5.-24. Input but not used.

### PRØ.2.EE(4(2E9.0)) Source Time Profiles

The source time profiles are input as histogram distribution functions. The distributions are normalized internally. A new card is started for each profile I = 1, 2, ..., NPFMAX. The data for each profile consists of alternating values of time (seconds) and the relative distribution (arbitrary units) for a total of NPTMAX time points -- each profile has the

same number of points. Time points can coincide and can be repeated several times to provide the NPTMAX tabulation points. All profiles are assumed to start at time zero. The relative form of the data is:

$$t_1, h_1, t_2, h_2, \dots, t_{NPTMAX}, h_{NPTMAX}$$

where

$$\begin{aligned} f(t) &= h_1 & 0 < t < t_1 \\ &= h_2 & t_1 < t < t_2 \\ &\bullet \\ &\bullet \\ &\bullet \end{aligned}$$

NOTES:

The program will generate a single Poisson time distribution for use in time-dependent problems where  $p(t) = \tau^{N-1} \exp(-\tau)$ , where  $\tau = t/a$  and  $t$  is the real time in seconds. On data card PRØ.1

3. NPFMAX = 0
4. NPTMAX = 0
5. MAJØR, number of major time steps.
6. MINØR, number of small time steps at the start of each large time step.
7. N, exponent of  $\tau$  in the Poisson distribution.

Then if MAJØR>0, omit PRØ.2 and supply

PRØ.3.E(8E9.0) Poisson Parameters

Omit this card if MAJØR = 0.

1. ALPHA,  $\alpha$  ( seconds ) in the Poisson distribution.
2. TMAX (seconds), major time step length.
3. TMIN (seconds), minor time step length.
4. TZER (seconds), start time for the first major time step.

## SURfaces

This section provides input for describing quadric surfaces which form the boundaries of material regions.

### SUR.O.H(24A3) Header Card

Contains SUR in columns 1-3.

### SUR.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2>0, number of surfaces being input on card SUR.2. IN2=0, no surfaces are being input.
3. NSMAX, total number of surfaces.
4. NAMAX, maximum number of coefficients in any surface equation. NAMAX=3 if all the surfaces are planes, NAMAX=6 if there are any regular curved surfaces, and NAMAX=9 if there are any rotated surfaces.
- 5.-24. Input but not used.

### SUR.2.S(3I3,7E9.0) Surface Equations

Supply this card for IN2 surfaces.

1. I, index of the surface being described.
2. NTP(I), index (j) of the last nonzero coefficient if the surface is in the expanded form; calculated internally for all other surfaces.

3. NEX, form ( $n_x$ ) of the surface as input. 0, already in expanded form.  $1 \leq NEX \leq 13$ , special form as indicated in Figures SUR.1, SUR.2 and SUR.3 and Table SUR.1.
4. AA(1), first parameter defining the surface.
5. AA(2), second parameter defining the surface.  
⋮
10. AA(7), seventh parameter defining the surface.

The requisite parameters are listed in the last column of Table SUR.1 and are input in the order shown. If the surface is in the expanded form and rotational terms are involved, supply these on the continuation card SUR.4 before supplying card SUR.3 for the next input surface.

#### SUR.3.E(8E9.0) Rotated Surface Equation Terms

Supply this card as required to finish the description of a surface, omit otherwise.

1. A(7,I), coefficient of xy in the general surface equation.
2. A(8,I), coefficient of yz in the general surface equation.
3. A(9,I), coefficient of zx in the general surface equation.

SUR-3

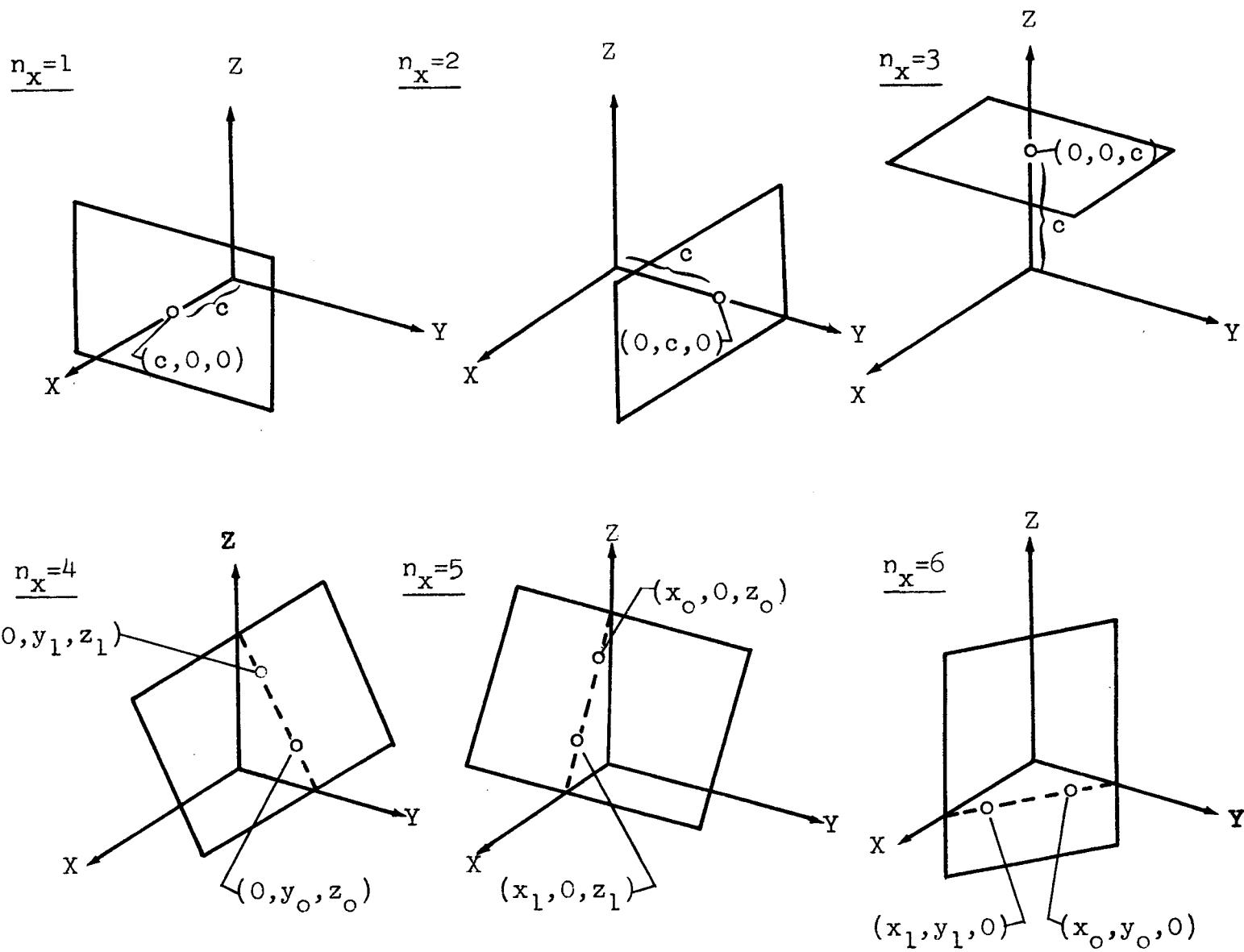


FIGURE SUR.1 PLANE SURFACES

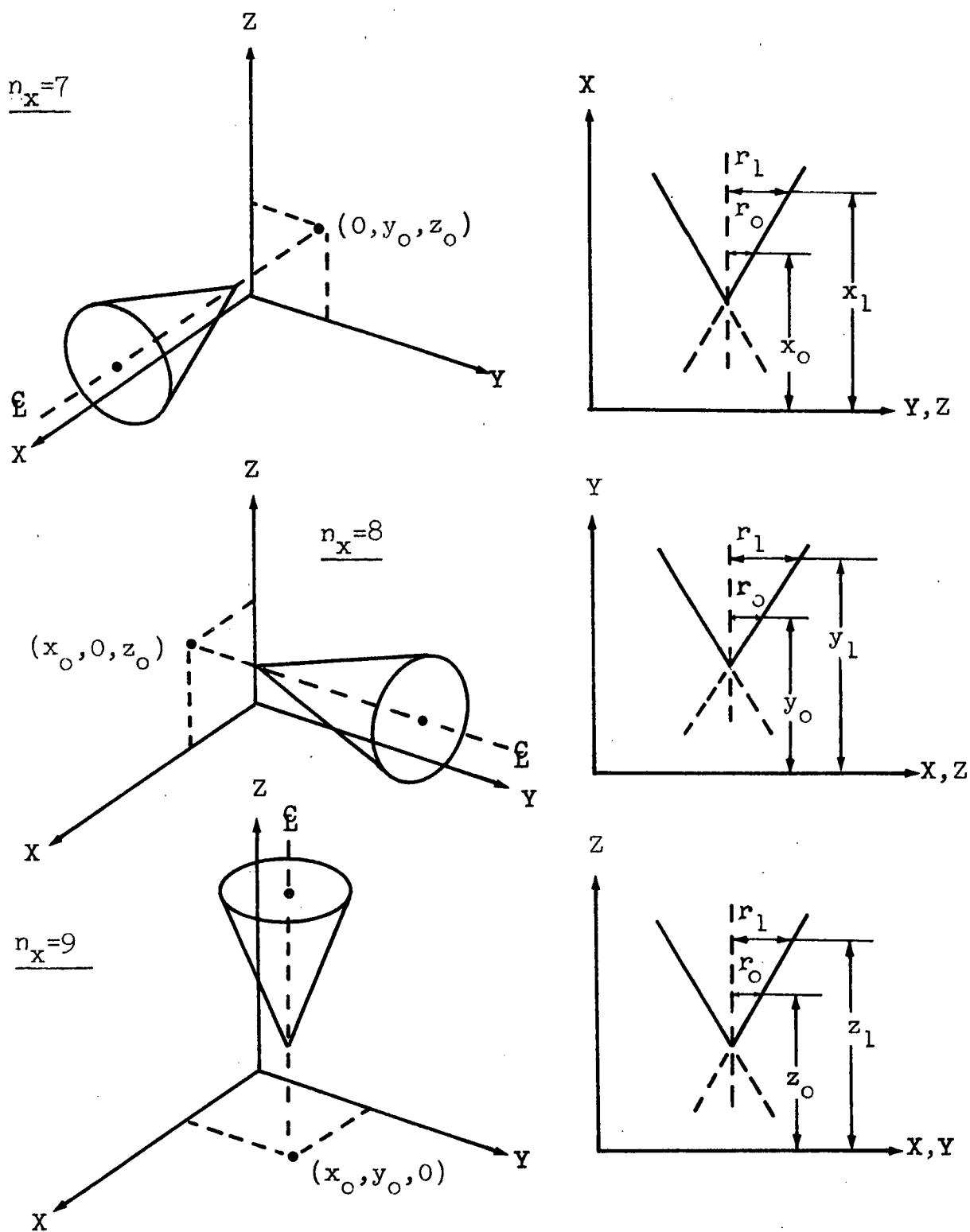


FIGURE SUR.2 CONICAL SURFACES

SUR-5

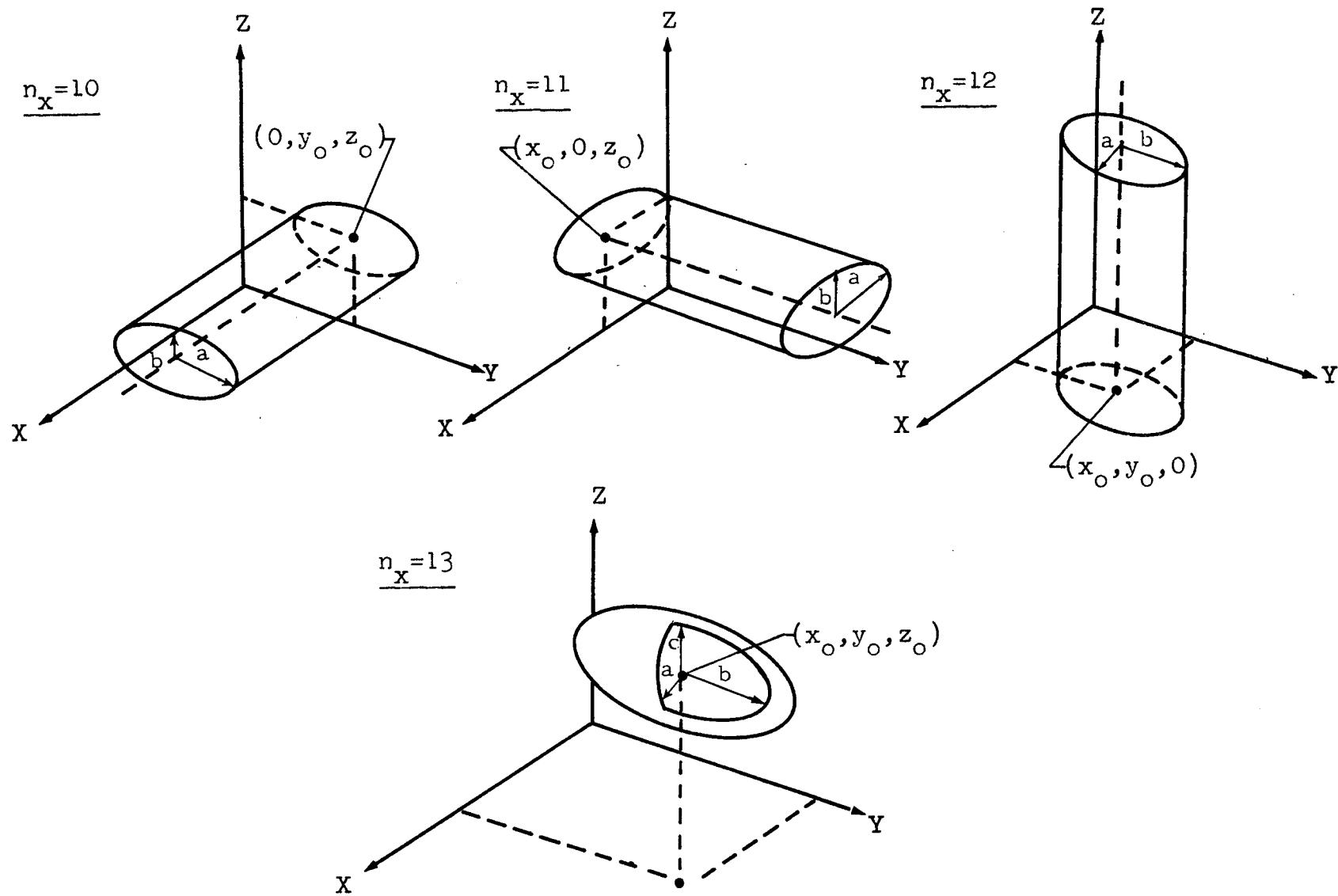


FIGURE SUR.3 ELLIPTICAL CYLINDERS AND ELLIPSOIDS

TABLE SUR.1

## SPECIAL SURFACE EQUATIONS

Surface type	Surface equation	Last term	Type $n_x$	Input
Quadric	$a_0 + a_1x + a_2y + a_3z + a_4x^2 + a_5y^2 + a_6z^2 + a_7xy + a_8yz + a_9zx = 0$	j	0	$a_0, a_1, \dots, a_j$
Plane $\perp$ x-axis	$x = c$	1	1	c
Plane $\perp$ y-axis	$y = c$	2	2	c
Plane $\perp$ z-axis	$z = c$	3	3	c
Plane $\parallel$ x-axis	$(y - y_o)/(z - z_o) = (y_1 - y_o)/(z_1 - z_o)$	3	4	$y_o, z_o, y_1, z_1$
Plane $\parallel$ y-axis	$(x - x_o)/(z - z_o) = (x_1 - x_o)/(z_1 - z_o)$	3	5	$x_o, z_o, x_1, z_1$
Plane $\parallel$ z-axis	$(x - x_o)/(y - y_o) = (x_1 - x_o)/(y_1 - y_o)$	2	6	$x_o, y_o, x_1, y_1$
Cone $\parallel$ x-axis	$\left( [(y - y_o)^2 + (z - z_o)^2]^{\frac{1}{2}} - r_o \right) / (x - x_o) = (r_1 - r_o) / (x_1 - x_o)$	6	7	$y_o, z_o, r_o, x_o, r_1, x_1$
Cone $\parallel$ y-axis	$\left( [(x - x_o)^2 + (z - z_o)^2]^{\frac{1}{2}} - r_o \right) / (y - y_o) = (r_1 - r_o) / (y_1 - y_o)$	6	8	$x_o, z_o, r_o, y_o, r_1, y_1$
Cone $\parallel$ z-axis	$\left( [(x - x_o)^2 + (y - y_o)^2]^{\frac{1}{2}} - r_o \right) / (z - z_o) = (r_1 - r_o) / (z_1 - z_o)$	6	9	$x_o, y_o, r_o, z_o, r_1, z_1$
Cylinder $\parallel$ x-axis	$(y - y_o)^2/a^2 + (z - z_o)^2/b^2 = 1$	6	10	$y_o, a, z_o, b$
Cylinder $\parallel$ y-axis	$(x - x_o)^2/a^2 + (z - z_o)^2/b^2 = 1$	6	11	$x_o, a, z_o, b$
Cylinder $\parallel$ z-axis	$(x - x_o)^2/a^2 + (y - y_o)^2/b^2 = 1$	5	12	$x_o, a, y_o, b$
Ellipsoid	$(x - x_o)^2/a^2 + (y - y_o)^2/b^2 + (z - z_o)^2/c^2 = 1$	6	13	$x_o, a, y_o, b, z_o, c$

## HELical Surfaces

This input section provides input for describing helical (or toroidal) surfaces. This section is actually an alternate to the SURface input section and represents an extension of that section. Since intersections are calculated by an iterative procedure, regions bounded by these surfaces should be defined so that the helix makes only a fraction of a turn for each region, e.g., 45° turn per region.

### HEL.O.H(24A3) Header Card

Has HEL in columns 1-3.

### HEL.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2>0, number of helical and quadric surfaces being input.  
IN2=0, no surface input.
3. NSMAX, total number of surfaces of all types.
4. NAMAX, maximum number of coefficients in any surface equation, 3 if all surfaces are planes, 6 if there are any helical or quadratic surfaces, and 9 if there are any rotated or quadric surfaces.
- 5.-24. Input but not used.

### HEL.2.S(3I3,7E9.0) Surface

1. I, index of surface.

2. NTP, not used.
3. NEX, 16 if the helix turns around the x axis.  
           17 if the helix turns around the y axis.  
           18 if the helix turns around the z axis.
4. AA(1),  $x_1^o$       } the origin of the helical surface where  

5. AA(2),  $x_2^o$       }  $x_1, x_2, x_3, = (x, y, z)$  if NEX = 16.  
                                = (y, z, x) if NEX = 17.  

6. AA(3),  $x_3^o$       }  $= (z, x, y)$  if NEX = 18.

7. AA(4), L(cm) the period of the helix. If zero, a torus results.

8. AA(5), R(cm) the distance of the helix centerline from the axis about which the helix turns.

9. AA(6), a(cm) the radius of the circular cross section of the helix.

10. Input but not used.

where the helical surface equation is

$$\phi(r) = \left\{ \left[ (x_j - x_j^o)^2 + (x_k - x_k^o)^2 \right]^{\frac{1}{2}} - R \right\}^2 + \frac{1}{1 + \left( \frac{L}{2\pi R} \right)^2} \left[ \frac{L}{2\pi} \tan^{-1} \left( \frac{x_k - x_k^o}{x_j - x_j^o} \right)^2 - (x_i - x_i^o) \right]^2 - a^2$$

i = NEX-15

j = i+1 modulo 3

k = j+1 modulo 3

## REGions

This section describes the material regions comprising the geometry. Care must be taken in describing these regions to avoid ambiguities. After all data has been input for a problem, the program checks for some of these ambiguities. If any errors are detected, the following message is written:

NØGØ\*THE PØINT IN REGION I IS ALSØ IN REGION J\*NØGØ

This error is usually the result of defining regions which overlap.

### REG.O.H(2<sup>4</sup>A3) Header Card

Contains REG in columns 1-3.

### REG.1.I(2<sup>4</sup>I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2>0, number of regions being input.  
IN2=0, no regions are being input.
3. NRMAX, total number of regions.
4. NBMAX, maximum number of boundaries per region.
- 5.-24. Input but not used.

### REG.2.R(12I3,4E9.0) Regions

Supply card REG.2 (and REG.3 as required) for IN2 regions.

1. I, index of the region being described.
2. ISV(I), index of the volume source superimposed over this region. 0, indicates none.
3. MTL(I)>0, index of the composition for the region.  
MTL(I)=0, the region is void.
4. NS(1,I), first boundary surface index.
5. NS(2,I), second boundary surface index. 0 or blank if all boundaries have been listed.  
•  
•  
NS(J,I), Jth boundary surface index. 0 or blank if all boundaries have been listed.  
•  
•
12. NS(9,I), >0, ninth boundary surface index if the region has exactly nine boundaries. 0, or blank if all boundaries have been listed (less than nine boundaries). -1, if the region has more than nine boundaries; the ninth and remaining boundaries are listed on card REG.4.
13. RHØ(I), density scale factor for the region.
14. XR(1,I), x-coordinate of any point in the region (cm).
15. XR(2,I), y-coordinate of the point in the region (cm).
16. XR(3,I), z-coordinate of the point in the region (cm).

### REG.3.I(24I3) Additional Region Boundaries

Supply this card(s) for each region having more than nine boundaries, immediately behind card REG.2 for the region; omit otherwise. This card contains data up to and including the maximum number of boundaries (more than 1 physical card if NBMAX>32).

1. NS(9,I), ninth boundary surface index.
2. NS(10,I), tenth boundary surface index.
3. NS(11,I), eleventh boundary surface index. 0 or blank if all boundaries are listed.  
⋮  
NS(NBMAX,1), last boundary surface index. 0 or blank if all boundaries are listed.

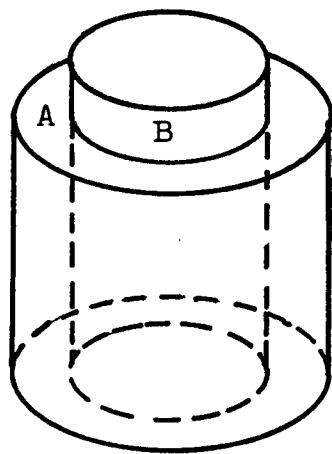
#### NOTES:

Restrictions must be imposed on possible region shapes to ensure that all points in a region are always on the same side of each region boundary. For example, the single region indicated in Figure REG.1a is unacceptable since there are points in the region which are both inside and outside boundaries A and B. The obvious solution is to use two regions to describe such geometric shapes.

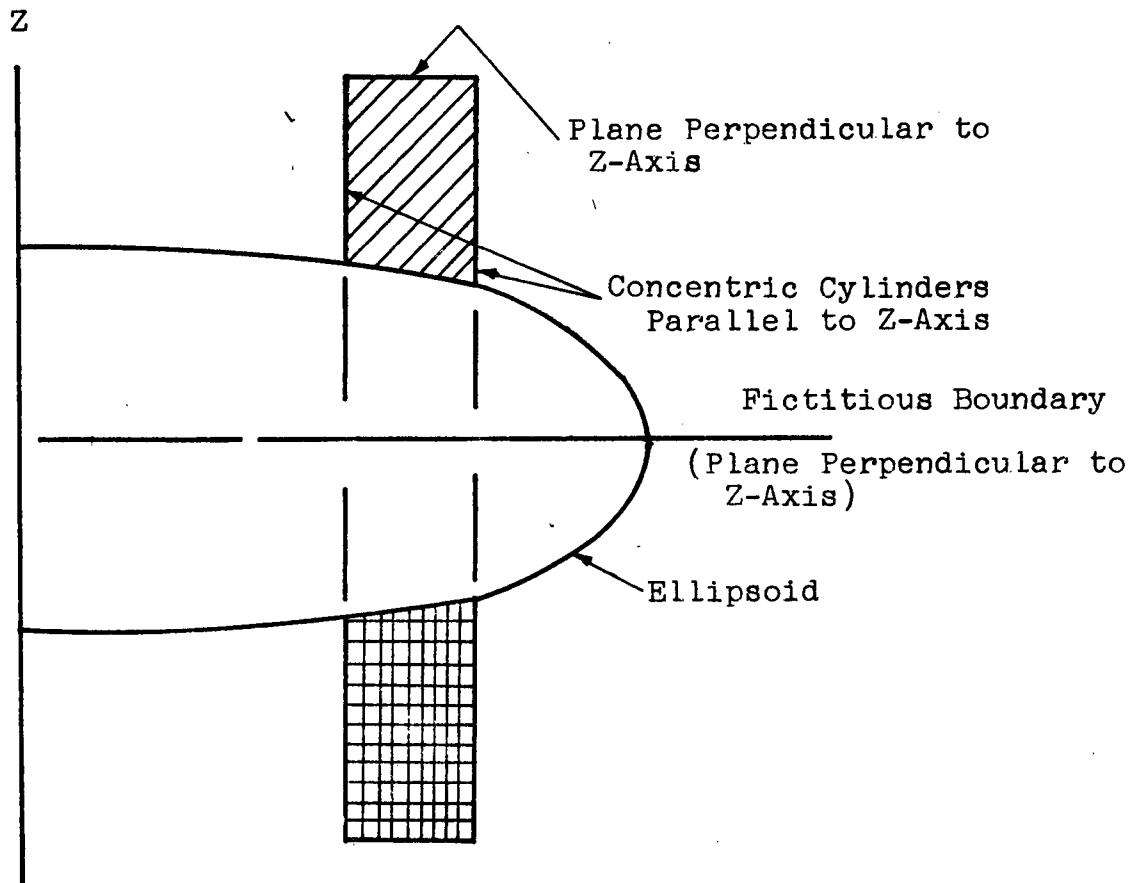
It is sometimes necessary to introduce fictitious boundaries. Figure REG.1b shows a typical situation requiring these boundaries. Examination of the hatched and cross hatched regions reveals that they form two sections of a single region since ambiguity indices of the boundaries have the same values for both sections. This condition can cause trouble if only

one section of the region is desired, even if other regions occupy the second section. The specification of the fictitious boundary eliminates the problem without otherwise affecting the geometric calculations. These fictitious boundaries must be included in the initial surface descriptions.

The final page of printout of each problem is sometimes helpful in correcting geometric errors. It contains a listing, by region, of the bounding surfaces (with the sign of ambiguity index affixed) and the region entered the last time a ray crossed these boundaries (most probable-next-regions). Most-probable-next-region indices less than zero indicate that there was no next region and should correspond to the outer boundaries of the problem. A zero indicates the boundary was never crossed.



a. Ambiguous Region Boundaries



b. Disjoint Regions

FIGURE REG.1 PROBLEMS IN REGION DESCRIPTIONS

## CYLindrical Geometry

This input section permits a simplified input of a symmetric cylindrical geometry.

### CYL.O.H(24A3) Header Card

Contains CYL in columns 1-3.

### CYL.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-6 from this card.
2. IN2, (0,>0)=(no,yes) cards CYL.2 and CYL.3 are being input.
3. NRRMAX, number of radial subdivisions.
4. NZZMAX, number of axial subdivisions.
5. ISV, index of the volume source superimposed over the regions. ISV=0 denotes none.
6. MTL, index of the material contained in the regions.  
The relative density is set at 1.0 unless MTL=0 (void).
- 7.-24. Input but not used.

### CYL.2.E(8E9.0) Radial Boundaries

This card contains the radial boundaries (cm) in increasing order. A radius of 0.0 must be the first entry on this card so that a total of NRRMAX+1 entries are required.

CYL.3.E(8E9.0) Axial Boundaries

This card contains the boundaries (cm) of the axial subdivisions, a total of NZZMAX+1 entries.

NOTES:

The program responds to the above input by generating NRRMAX cylindrical surfaces, concentric with the z-axis and numbered 1 through NRRMAX, and NZZMAX+1 plane surfaces, perpendicular to the z-axis and numbered NRRMAX+1 through NRRMAX+NZZMAX+1. The program then generates NRRMAX\*NZZMAX regions numbered outward radially for the first axial zone, then the second axial zone, etc.

## SPHerical Geometry

This input section provides for input description of concentric spherical regions.

### SPH.O.H(24A3) Header Card

Contains SPH in columns 1-3.

### SPH.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3.-5. from this card.
2. IN2, (0,>0)=(no,yes) the spherical region boundaries are being input on card SPH.2.
3. NSHELL, number of spherical regions to be described.
4. ISV, index of the volume source, if any, superimposed over the regions, 0 denotes none.
5. MTL, index of the material located in the regions.
- 6.-24. Input but not used.

### SPH.2.E(8E9.0) Sphere Boundaries

This card contains the outer boundaries (cm) of the spherical zones in order of increasing radius. The program generates NSHELL spherical surfaces numbered 1 through NSHELL. It then generates NSHELL regions also numbered 1 through NSHELL. Each region is given a density of 1.0 which will be replaced by a variable air density through the use of the AIR input section. Additional surfaces and regions can be added to this basic geometry using the SUR and REG input sections.

## AIR Density

This section provides for input of an exponential atmosphere to be used in conjunction with the SPH input section for air transport problems. The air density is exponentially interpolated to obtain the density at the boundaries of the spherical zones and is then linearly interpolated for particle transport.

### AIR.O.H(24A3) Header Card

Must have AIR in columns 1-3.

### AIR.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2<0, use the built-in air density variation (1959 ARDC) with altitude. The air composition given in the MATerials section should have a density of 1.0.  
IN2=0, previously defined air density variation holds.  
IN2>0, air density profile is input.
3. NAIRPT, number of points in the input tabulation of air density with altitude.
- 4.-24. Input but not used.

### AIR.2.EE(4(2E9.0)) Air Density

Supply this card if IN2>0 with NAIRPT pairs of data consisting of radius (cm) from the earth's center and the air density relative to the air composition given in the MATerials section.

## CHECK Ray Trace

This input section is utilized in the checkout of complex geometries. It provides information used by the program to ensure that ray traces terminate at the outer boundaries of the geometry rather than at the boundaries of undefined volumes within the geometry.

### CHE.O.H(24I3) Header Card

Has CHE in columns 1-3.

### CHE.1.I(24I3) Option Card

1. IN1, (0, > 0)=(no,yes) interpret data words 3-5 from this card.
2. IN2, (0, > 0)=(no,yes) card CHE.2 is being input.
3. NCHECK, total number of region-surface combinations forming the outer boundary of the geometry.
4. LCHECK=0, no effect.  
LCHECK>0, terminate the problem if this number of ray traces doesn't terminate at the region-surface combinations tabulated on card CHE.2.
- 5.-24. Input but not used.

### CHE.2II(12(2I3)) Outer Boundaries

The outer boundary of the geometry is defined by listing NCHECK pairs of indices of the region and surface forming the outer boundary.

NOTES:

If, during a ray trace, a region-surface combination at the apparent outer boundary of the geometry does not match with one of the listed pairs, the following message is printed

\*\*\*RAY TERMINATES AT SURFACE I WHERE IT BOUNDS REGION J\*\*\*

If LCHECK>0, the following information is also printed:  
the values of x (the ray origin) including the square and cross products, the values of c (the ray direction cosine) including the direct and cross products with x, the square and cross products of c, the quantities used in calculating the intersection of the ray with the surfaces, and the region, surface crossed, and partial path lengths along the ray.  
If LCHECK>0 and the number of errors equals LCHECK, the problem is terminated with the following message:

\*\*\*TERMINATING RUN DUE TO RAY TRACE ERRORS\*\*\*

The termination is not immediate. Internal counters are set so that the problem will hopefully make it to the output routines to give a somewhat normal print of results with possibly incorrect labeling on the detector index and the number of histories run.

## CØRrelated Calculations

This section provides for the simultaneous solution of multiple problems which have small differences in either the source description or the material composition of regions.

### CØR.O.H(24A3) Header Card

Has CØR in columns 1-3.

### CØR.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3.-5. from this card.
2. IN2>0, number of correlated sources and/or regions being input on card CØR.2.
3. NCCMAX, number of correlated problems.
4. NCSMAX, number of sources which are different from the base problem.
5. NCRMAX, number of regions which differ in composition from the base problem.
- 6.-24. Input but not used.

### CØR.3.I(24I3) Correlation Sets

Supply IN2 sets of this card.

1. I>0, index of the count on correlated sources.  
I<0, index of the count on correlated regions.

2. ICS(I), index of the base case source if I>0.

or

ICR(-I), index of the base case region if I<0.

3. JCS(1,I) if I>0.

JCR(1,-I) if I<0.

⋮

JCS(J,I), index of the source to be used in place of source ICS(I) in the J<sup>th</sup> correlated calculation, if I>0.

JCR(J,-I), index of the material in region ICR(-I) to be used in the J<sup>th</sup> correlated calculation if I<0.

⋮

JCS(NCCMAX,I) if I>0.

JCR(NCCMAX,-I) if I<0.

## DETectors

This section provides for the description of point, surface, and/or volume detectors. The transport calculation yields, as basic output, the differential number flux at each of these detectors. Other optional outputs can be invoked through other input sections.

### DET.O.H(24A3) Header Card

Columns 1-3 contain DET.

### DET.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2>0, number of detectors being described via card DET.2.  
IN2=0, no detectors are being input.
3. NDMAX, total number of detectors.
- 4.-24. Input but not used.

### DET.2.S(3I3,7E9.0) Detectors

1. I, index of the detector being described.
2. IDR(I)=0, for point detector.  
IDR(I)>0, region index for a surface or volume detector.
3. IDS(I)=0, for a point detector.  
IDS(I)=0, for a volume detector.  
IDS(I)>0, surface index for a surface detector (the detector is that part of surface IDS(I) which bounds region IDR(I)).

4.  $V\phi L(I)$ , scale factor for point detector (i.e., multiplies output by this number); region volume ( $\text{cm}^3$ ) for volume detector; detector area ( $\text{cm}^2$ ) for surface detector (1.0 yields surface-or volume-integrated fluxes).
5.  $CDT(1,I)$ , relative direction cosine with respect to the x-axis of the unit direction vector used in obtaining angular fluxes, e.g., Legendre moments (not used for surface detectors, angular moments are obtained with respect to the surface normal).
6.  $CDT(2,I)$ , relative direction cosine with respect to the y-axis.
7.  $CDT(3,I)$ , relative direction cosine with respect to the z-axis; the 3 direction cosines are normalized by the program.
8.  $XDT(1,I)$ , x coordinate if a point detector ( $\text{cm}$ ).
9.  $XDT(2,I)$ , y coordinate if a point detector ( $\text{cm}$ ).
10.  $XDT(3,I)$ , z coordinate if a point detector ( $\text{cm}$ ).

NOTES:

After processing all the input data, the program then generates particle histories and finally prints the fluxes for each detector. The output for each detector starts a new printout page and is headed by the line

\*\*\*FLUXES FOR DETECTOR I AFTER J PACKETS\*\*\*

where I is the detector index and J is the number of histories which were processed. Immediately below this line are column

headings followed by a printout line for each energy group.

The appropriately titled columns consist of groupwise values for the coefficient of variation (fractional standard deviation) of the number flux by group, the average energy for each group (Mev), the differential number flux for the group (particles/cm<sup>2</sup>/sec/Mev), the differential energy flux for the group (Mev/cm<sup>2</sup>/sec/Mev), the integrated number flux in each group (particles/cm<sup>2</sup>/sec), the integrated number flux down through the current group (particles/cm<sup>2</sup>/sec), and finally the integrated energy flux down through the current group (Mev/cm<sup>2</sup>/sec).

A second set of output is then printed for the detector and is headed by the line:

\*\*\*NUMBER FLUX RESPONSES FOR DETECTOR I AFTER J PACKETS\*\*\*

The first two columns NUMBER FLUX and ENERGY FLUX, in this set of output are always obtained and are essentially repeats of the group-integrated fluxes obtained in the first output set. Other columns are also printed, with appropriate title, of any response functions input using the RESPONSE input section. The lines of output for each energy group are the integrated response for that group. After all the group lines are printed, four additional lines are printed, TOTALS consisting of the total response for all energy groups, MIN ERROR the coefficient of variation in the total response if the response for each energy is independent, MOD ERROR the coefficient of variation using the usual equation for the variance, and MAX ERROR the coefficient of variation if the responses for the groups are strictly dependent.

A final set of output is then printed for each detector and is labeled

\*\*\*NUMBER FLUX MØMENTS FØR DETECTOR I AFTER J PACKETS\*\*\*

and gives various breakdowns on the differential number fluxes by energy group. The first column in this set of output is always obtained. It is labeled ITERANT K and consists of the average flux for the histories run between the  $(K-1)^{\text{th}}$  and  $K^{\text{th}}$  print cycles for the problem. Other columns are added depending on requested output options such as flux by order-of-scatter ( $\phi$ RD input section), etc. After the group lines are printed for this output set, the various response functions are then evaluated by integrating over each column, and are then printed with appropriate line titles.

The printout would continue in this manner for each detector. If the problem involved multiple printouts during the calculation, the printout for the next group of histories would appear farther downstream. The order of printing is reversed when only point detectors are run. The multiple prints for detector one are followed by the multiple prints for detector two, etc.

The input of point detector coordinates for air transport problems can be accommodated in terms of more convenient parameters. The detector index is flagged with a minus sign. Then the following interpretations are made:

XDT(1,I) = the distance of the detector from the earth's center (cm) -- earth radius =  $6.356766 \times 10^8$  cm.

XDT(2,I) = the look angle (degrees) of the detector measured from the vertical.

XDT(3,I) = the azimuthal angle (degrees) of the detector measured from the x-axis.

## FLUX Groups

This section provides for the definition of flux groups which are different from the cross section groups.

### FLU.O.H(24A3) Header Card

Columns 1-3 contain FLU.

### FLU.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) flux group boundaries are being input on card FLU.2.
3. NGMAX, number of flux groups.
- 4.-24. Input but not used.

### FLU.2.E(8E9.0) Group Boundaries

Supply the flux group boundaries in order of decreasing energy (Mev), ELF(1), ELF(2), ..., ELF(NGMAX+1).

## RESpone Functions

This input section provides the data for response functions used to weight the basic number fluxes output for each detector. The program has two response functions built-in, number and energy flux, to provide for the calculation of the coefficients of variations on their totals.

### RES.O.H(24A3) Header Card

Must contain RES in columns 1-3.

### RES.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2>0, number of response functions being input on card RES.2 and RES.3.  
IN2=0, no responses are being input.
3. NFMAX, total number of response functions besides those built-in.
- 4.-24. Input but not used.

### RES.2.A(24A3) Response Titles

This card contains a title for each response function being input. Each title is allowed 12 columns, i.e., the first title is in columns 1-12, the second in columns 13-24, etc.

### RES.3.S(3I3,7E9.0) Response Function

Supply this card (and RES.4 as required) in sets, one set for each of the IN2 responses being input.

1. I, index of the response function being input.
2. NFT=0 if this is a number flux response, i.e., response per particle/cm<sup>2</sup>•sec.  
NFT=1 if this is an energy flux response, i.e., response per Mev/cm<sup>2</sup>•sec.
3. NTL>0, this is an energy absorption response function for material NTL, omit data words 5-10 on this card.  
NTL=0, this is an input-described response function.
4. SCA, scale factor to convert the response function from its present units to more desirable units. Do not input 0.0. The units of energy absorption responses, NTL>0, are Mev/cm per particle/cm<sup>2</sup>•sec, i.e., Mev/cm<sup>3</sup>•sec.
5. RSP(1,I), response function at the upper boundary of flux group 1.  
•  
•  
•
10. RSP(6,I), response function at the lower boundary of flux group 6.

RES.4.E(8E9.0) Response Continuation Card

Omit this card if NTL>0 or if there are less than six flux groups. This card contains the response function at the lower energy boundaries of flux groups six through NGMAX.

### BIRth Regions

This input section provides for the optional output of obtaining a breakdown on fluxes according to the geometric region in which the radiation was emitted from an independent or secondary source. The resulting output for each detector appears under the general heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTOR I AFTER J PACKETS\*\*\*

where I is the detector index and J is the number of histories run. The specific columns are headed SØURCE K where K denotes the region index. The entries in each column are the differential number flux (particles/cm<sup>2</sup>/Mev/sec) for each flux group followed by the contribution to each response function.

#### BIR.0.H(24A3) Header Card

BIR is entered in column 1-3.

#### BIR.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) card BIR.2 is being input.
3. NVMØD, number of regions for which this output is required.
- 4.-24. Input but not used.

#### BIR.2.I(24I3) Birth Region Indices

List the indices of the regions for which this output is required, NVMØD entries.

## ØRDer of Scatter

This input section provides for a breakdown of fluxes at each detector according to the number of collisions which the particles have before reaching the detector. The resulting output for each detector appears under the general heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTØR I AFTER J PACKETS\*\*\*

where I is the detector index and J is the number of histories run.

The specific columns are headed SCATTER K where K denotes the number of collisions. The entries in the column are the differential number flux (particles/cm<sup>2</sup>/Mev/sec) for each flux group followed by the contribution to each response function.

### ØRD.0.H(24A3) Header Card

Contains ØRD in  $\infty$  lumns 1-3.

### ØRD.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, not used.
3. NCMAX, maximum order of scatter up to which the breakdown is obtained, i.e., NCMAX columns of output are produced containing the uncollided flux, single scattered flux,..., (NCMAX-1)th scattered flux.
- 4.-24. Input but not used.

ØRD-1

## SCAttering Regions

This input section will yield a breakdown on the differential number flux by the region(s) in which the particles scatter. The resulting output for each detector will appear under the heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTØR I AFTER J PACKETS\*\*\*

where I and J denote the detector index and number of histories respectively. The columns containing this output will have headings of the form REGION K where K is a region index. The output in each column consists of the differential number flux (particles/cm<sup>2</sup>/sec/Mev) by energy group followed by the contribution to each of the response functions.

### SCA.O.H(24A3) Header Card

Must have SCA in columns 1-3.

### SCA.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
  2. IN2, (0,>0)=(no,yes) card SCA.2 is being input.
  3. NSRMAX, number of regions for which the breakdown is required.
- 4.-24. Input but not used.

### SCA.2.I(24I3) Region Indices

Supply this card with the indices of the scattering regions, NSRMAX entries.

### BØoundary Crossings

This input section provides a breakdown of the particle fluxes according to region boundaries crossed by the particle in reaching the detectors. The resulting output for each detector appears under the heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTOR I AFTER J PACKETS\*\*\*

where I and J denote the detector index and histories respectively. The columns containing this output have headings of the form CRØSSING K where K is the index of the crossing. The output in each column consists of the differential number flux (particles/cm<sup>2</sup>.sec.Mev) by energy group followed by the contribution to each of the response functions.

### BØU.O.H(24A3) Header Card

Contains BØU in columns 1-3.

### BØU.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) card BØU.2 is being input.
3. NBCMAX, number of different boundaries for which the breakdown is required.
- 4.-24. Input but not used.

### BØU.2.II(12(2I3)) Boundary Definitions

This card contains NBCMAX pairs of numbers. The first number in each pair is the index of a region. The second number of the pair is the index of a surface bounding that region.

The output is generated for particles which cross the surface  
(in either direction) only where it bounds the region.

## ANGular Fluxes

This input section provides for the calculation of angular fluxes. The output for each detector consists of azimuthally-averaged Legendre moments of the angular flux. The output appears under the general heading

\*\*\*NUMBER FLUX M<sub>0</sub>MENTS F<sub>0</sub>R DETECTOR I AFTER J PACKETS\*\*\*

where I and J denote the detector index and number of histories, respectively. The columns containing the output have headings of the form ANGULAR K where K denotes the Legendre moment index. The K=-1 moment is the backward hemisphere component of the P<sub>-1</sub> moment and the K=1 moment is the forward hemisphere component of the P<sub>1</sub> moment. For K>1, the column contains the P<sub>K</sub> Legendre moment. These moments are generated with respect to the fixed directions specified in the DETector input section except for surface detectors. For surface detectors, the moments are with respect to the surface normal.

The output in each column is the Legendre moment of the differential number flux (particles/cm<sup>2</sup>.sec.Mev) by energy group followed by moments of the response functions.

### ANG.O.H(24A3) Header Card

Contains ANG in columns 1-3.

### ANG.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2, not used.

3. NLMAX, number of Legendre moments requested. Output will include moments to order NLMAX-1.
  4. NAFMAX, number of discrete directions at which the Legendre series is to be evaluated.
- 5.-24. Input but not used.

NOTES:

If NAFMAX>0, additional output is generated on the last print cycle for each detector. This output appears after the regular outputs and has the general heading

\*\*\*ANGULAR FLUXES FOR DETECTOR I AFTER J PACKETS\*\*\*

where I and J are the detector index and number of histories, respectively. Individual columns have the headings C<sub>0</sub>S=+\_X.XXXX where \_X.XXXX is the cosine of the polar angle with respect to the direction associated with the detector. NAFMAX polar angle cosines are generated by the program, equally spaced between -1.0 and +1.0 including these points. The output in each column is the azimuthally-averaged differential angular number flux (particles/cm<sup>2</sup>.sec.Mev.steradian) by energy group followed by the contributions to the angular responses (response/steradian).

## SØLid Angle Fluxes

This input section will provide angular fluxes for each detector which are averaged over specified solid angle elements. The output for each detector appears under the heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTØR I AFTER J PACKETS\*\*\*

where I and J are the detector index and number of histories, respectively. The individual columns are headed by CØNE K where K is the index of a solid angle element. The output in each column consists of the average differential angular number flux (particles/cm<sup>2</sup> sec.Mev·steradian) by energy group followed by the contribution to the response functions (response/steradian).

### SØL.O.H(24A3) Header Card

Contains SØL in columns 1-3.

### SØL.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3, from this card.
2. IN2, (0,>0)=(no,yes) card SØL.2 is being input.
3. NABMAX, number of solid angle elements.
- 4.-24. Input but not used.

### SØL.2.E(8E9.0) Solid Angle Boundaries

This card contains four pieces of data for each solid angle element--two elements per card. The data for each element in the order of input, are the lower and upper limits on

the azimuthal angle ( $-\pi \leq \theta \leq \pi$ ) and the lower and upper limits on the cosine of the polar angle. The azimuthal and polar angles are measured in a rotated coordinate system whose z axis is along the direction associated with each detector.

### TRAnslation Time

This input section provides for the translation of the time scale at each detector to make the physical numbers more manageable. The time input in this section for each detector is subtracted from the particle flight time before any time-dependent tallies are made for the detector.

#### TRA.O.H(24A3) Header Card

Has TRA in columns 1-3.

#### TRA.1.I(24I3) Option Card

1. IN1, not used.

2. IN2, ( $\leq 0, > 0$ )=(no,yes) card TRA.2 is being input.

IN2 = -1, the minimum time is computed internally as the time required to travel from the center of the closest source to the detector for particles in the most energetic energy group.

IN2 = -2, the minimum time is computed internally as the required time required for light to travel from the closest source to each detector.

#### TRA.2.E(8E9.0) Minimum Flight Time

This card contains the minimum time (sec) required for particles to travel from a source to each detector in the order of detector index, one entry for each detector described via the DETector input section. For secondary particle transport problems, this time includes the flight time of the primary particles.

## MØMents of Temporal Fluxes

This input section provides for the calculation of temporal moments of the particle fluxes. The output for each detector appears under the heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTØR I AFTER J PACKETS\*\*\*

where I and J denote the detector index and number of histories, respectively. The columns containing the output have the heading TEMPØRAL K where K is the index of the moment. The output in each column consists of the  $K^{\text{th}}$  moment of the differential number flux, i.e.,  $\int \phi(t) t^K dt$  (particles/cm<sup>2</sup>. sec<sup>1-K</sup>. Mev), by energy group followed by the moments of the response function.

### MØM.O.H(24A3) Header Card

This card has MØM in columns 1-3.

### MØM.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2, (0,>0)=(no,yes) card MØM.2 is being input.
3. NTMAX, number of temporal moments.
4. NTAMAX, number of times at which the time dependence is to be reconstructed from the moments.
- 5.-24. Input but not used.

MØM.2.E(8E9.0) Evaluation Times

This card contains NTAMAX times (sec) in ascending order at which the time dependence will be reconstructed from the temporal moments.

NOTES:

If NTAMAX>0, additional output is generated for each detector. This output is generated after all other output for the detector and is headed by the line

\*\*\*TEMPØRAL FLUXES FØR DETECTØR I AFTER J PACKETS FØR TIME PRØFILE K\*\*\*

where I denotes the detector index, J the number of histories, and K the source time profile. K=0 corresponds to a delta function source profile.

The columns under this heading are labeled by the times at which the time dependence is evaluated. The entries in the columns then consist of the differential number flux (particle/cm<sup>2</sup>/sec/Mev) by energy group followed by the time-dependent responses.

### TIMe Interval Fluxes

This input section provides for the calculation of time interval averaged temporal fluxes. The output for each detector appears under the heading

\*\*\*NUMBER FLUX MØMENTS FØR DETECTØR I AFTER J PACKETS\*\*\*

where I is the detector index and J is the number of histories. The columns containing the output have the more specific heading TIME BIN K where K is the index of the time interval. The output in each column consists of the differential number flux (particles/cm<sup>2</sup>.sec.Mev) by energy group averaged over the Kth time interval followed by the contribution to each response function and calculated as though all particles started at time t=0.

#### TIM.0.H(24A3) Header Card

This card must contain TIM in columns 1-3.

#### TIM.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) data card TIM.2 is being input.
3. NTBMAX, number of time intervals.
- 4.-24. Input but not used.

#### TIM.2.E(8E9.0) Time Interval Boundaries

This card contains the maximum time (sec) boundaries, in ascending order, for the time intervals, NTBMAX entries.

## GRØup Edit on Fluxes

This input section provides for an edit of fluxes at each detector by the energy group in which particles were emitted from the source.

### GRØ.O.H(24A3) Header Card

Has GRØ in columns 1-3.

### GRØ.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, not used.
3. NGRØUP, number of groups for which the edit is required.  
These will be the NGRØUP highest energy groups.
- 4.-24. Input but not used.

### NOTES:

The output generated for each detector appears under the heading

**\*\*\*NUMBER FLUX MØMENTS FØR DETECTØR I AFTER J PACKETS\*\*\***

The output appears under the columns headed GRØUP K where K is the index of the source group, K=1,2,...,NGRØUP. The entries in the column are the differential number flux (particles/cm<sup>2</sup>. sec·Mev) by energy group followed by the integrated response for each response function.

## NØRmal Derivatives

The section specifies the locations at which partial derivatives of the fluxes with respect to normal thicknesses of a region dimension are to be calculated.

### NØR.O.H(24A3) Header Card

Has NØR in columns 1-3.

### NØR.1.I(24I3) Option Card

1. IN1, (0, > 0) interpret data words 3 and 4 from this card.
  2. IN2, (0, > 0) cards NØR.2 and NØR.3 are being input.
  3. NØRMLD, number of locations at which normal derivatives are requested.
  4. NØRCØM, number of subsegments of the flux where each subsegment involves different combinations of the NØRMLD possible locations which particles can cross in arriving at a detector, i.e., one subsegment may consist of fluxes due to particles which cross all NØRMLD locations, another subsegment may consist of fluxes due to particles which do not cross any of the NØRMLD locations, etc.
- 5.-24. Input but not used.

### NØR.2.II(12(2I3)) Partial Derivative Locations

This card contains NØRMLD pairs of numbers giving the indices of the region and corresponding surface at which normal derivatives will be calculated.

### NØR.3.I(24I3) Normal Derivative Components Definition

This card defines the dependence of the NØRCØM components of the fluxes. NØRCØM cards are entered in sets for each detector in the problem, a total of NDMAX sets. Each of the cards in a set contains NØRMLD numbers giving the indices of the normal derivatives which each of the flux components sees. If one component involves all of the normal derivatives, the data card would contain the integers 1 through NØRMLD. If another component involves only the Ith normal derivative, the first piece of data on the card would be I followed by NØRMLD-1 zeros, etc..

#### NOTES:

The output resulting from this input appears after the optional flux edits and is headed by the line.

\*\*\*SHIELD DERIVATIVES FØR DETECTØR I AFTER J PACKETS\*\*\*

The columns under this heading consist of the energy group index, the total differential flux (particles/cm<sup>2</sup>. sec.Mev)-- labeled SEGMENT I where I is the index on the NØRCØM components, and the derivatives of the flux (particles/cm<sup>2</sup>. sec.Mev)/cm -- labeled NØRMAL J where J is the index on the NØRMLD possible derivatives. After the results are printed for each flux group, the response function weighted values are printed with the response title on the left side of the printout.

## MINimum Weight Shield

This input section will cause the program to calculate a minimum weight shield configuration using the derivatives resulting from the NOR input section.

### MIN.O.H(24A3) Header Card

Has MIN in columns 1-3.

### MIN.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-6 from this card.
  2. IN2, (0,>0)=(no,yes) cards MIN.2 and IN2 cards MIN.3 are being input.
  3. IPRESP, index of the response function to be used in defining the dose rate for the primary radiation type if this is a primary only problem. If this is a primary plus secondary problem, IPRESP is the response function index for the secondary problem.
  4. ISRESP, index of the response function for the primary particle if this is a primary and secondary problem.
  5. ITPRIN, number of iterations in the shield optimization between prints.
  6. ITERMX, maximum number of iterations in the shield optimization.
- 7-24. Input but not used.

MIN.2.E(8E9.0) Dose Rate Constraints

This card contains the dose rate constraint for each detector, NDMAX entries.

MIN.3.S(3I3,7E9.0) Shield Definitions

Input card MIN.3 IN2 times.

1. I, index of the shield based on its order of definition in the NØR input section.
2. IGS(I), (0,1,2)=(rectangular,cylindrical,spherical), shield geometry type.
3. IDF(I), index of the next shield lying at a larger radius than this shield. Not significant if all shields have rectangular geometry. A zero would be input for the outer shield of a series of concentric cylindrical or spherical shields.
4. TIN(I), initial thickness (cm) of this shield.
5. TMN(I), minimum thickness (cm) of this shield.
6. TMX(I), maximum thickness (cm) of this shield.
7. RIN(I), inner radius (cm) if this is the innermost shield of a set.
8. RSH(I), density ( $\text{gm}/\text{cm}^3$ ) of the shield material times any non-built-in geometric factors (area for rectangular, height for cylindrical).

9. DWN(I), maximum weight increment (gm) per iteration.

10. Input but not used.

NOTES:

The output generated from this input appears after the derivative information is printed. The output is preceded by the line

\*\*\*SHIELD OPTIMIZATION FOR DETECTOR I\*\*\*

Each print cycle is preceded by the lines

\*\*\*ITERATION\*\*\*WEIGHT(GM)\*\*\*DOSSE(1)\*\*\*DOSSE(2)\*\*\*DOSSE(TOT)\*\*UNSHIELDED\*\*\*

J	W	D <sub>1</sub>	D <sub>2</sub>	D <sub>t</sub>	D <sub>u</sub>
---	---	----------------	----------------	----------------	----------------

where J is the number of iterations during the shield optimization, W is the total shield system weight (grams), D<sub>1</sub> is the dose rate due to the last particle type, i.e., primary if only a one-particle type problem-secondary if a primary plus secondary problem, D<sub>2</sub> is the dose rate from primary particles in a primary plus secondary problem, D<sub>t</sub> is the total dose rate, and D<sub>u</sub> is the dose rate due to particles which did not cross any of the shields.

Following the above lines, are lines labeled DIMENSIONS, the thickness of each shield in cm; WEIGHT(GM), the weight of the individual shields; DWDT(GM/CM), the partial derivatives of the total shield weight with respect to thickness, DDDT( /CM) the partial derivatives of the dose rate with respect to thickness, and DDDW( /GM) the ratios of the dose and weight derivatives.

The last set of output during the optimization iterations is preceded by the line

\*\*\*TERMINATION=K(0/1/2/3)=(DIMENSION CONSTRAINTS/ITERATIONS/  
UNSHIELDED/DOSE CONSTRAINT) \*\*\*

and indicates the condition under which optimization terminated.

### DEPosition in Regions

This input section instructs the program to calculate the energy deposited in each region for problems which include one or more surface and/or volume detectors.

#### DEP.O.H(24A3) Header Card

This card must have DEP in columns 1-3.

#### DEP.I.1(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, not used.
3. NDEPØS, (0,>0)=(no,yes) calculate energy deposition.

#### NOTES:

The output from this option is printed preceding the output for the individual detectors. The output is headed by the line

\*\*\*ENERGY DEPØSITIØNS FØR CALCULATIØNAL SET K\*\*\*

where K is a sequential number of the base-line problem and any correlated problems described via the CØR input section. The output includes x,y, and z coordinates of a point in the region to simplify the region identification. The output also includes the coefficient of variation of total deposition (ERRØR), the total deposition (MEV/SEC), the deposition from particle histories terminated due to energy cutoff (E-CUTØFF),

the deposition from particle histories terminated at the collision cutoff (C-CUT $\backslash$ OFF), and finally the deposition due to weight cutoff (W-CUT $\backslash$ OFF).

### LEAkage of Energy

This input section instructs the program to calculate the energy leakage at the outer boundaries of the problem for those problems which contain surface and/or volume detectors.

#### LEA.O.H(24A3) Header Card

Has LEA in columns 1-3.

#### LEA.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, not used.
3. NLEAKS, number of different region-boundary combinations from which leakage can occur.
- 4.-24. Input but not used.

#### NOTES:

The output associated with this section appears just before the output for the individual detectors. The output is headed by the printout line

\*\*\*ENERGY LEAKAGES FØR CALCULATIONAL SET K\*\*\*

where K is a sequential numbering of the base-line problem and any correlated problems input via the CØR input section. The output includes the region and surface indices for the boundaries through which the leakage occurred, the leakage in Mev/sec and the computed coefficient of variation. The total leakage is also output.

## CHAnnel Detectors

This input section provides for the calculation of detector responses as a function of the energy deposited from a primary particle.

### CHA.O.H(24A3) Header Card

Has CHA in columns 1-3.

### CHA.1.I(24I3) Option Card

1. IN1 (0,>0)=(no,yes) interpret data words 3-5 from this card.
2. IN2>0, card CHA.2 and card CHA.3 for IN2 channels are input.  
IN2=0, cards CHA.2 and CHA.3 are not input.
3. NUMV $\emptyset$ L, number of channel detectors.
4. NUMREG, maximum number of regions to be included in the definition of a channel detector.
5. NCEMAX, number of energy channels.
- 6.-24. Input but not used.

### CHA.2.E(8E9.0) Channel Boundaries

This card contains the upper energy boundaries (Mev), in decreasing order, of the channels -- a total of NCEMAX entries.

CHA.3.I(24I3) Channel Detectors

This card describes the sensitive volume for each channel detector.

1. I, index of the detector.
2. MX, number of regions comprising the detector.
3. NUM(1,I)  
      :  
      :  
      NUM(MX,I) } indices of the regions comprising the detector.

## NØIse Functions

This input section provides the capability for analytically calculating the effect of electronic noise on the count rates of channel detectors.

### NØI.O.H(24A3) Header Card

Contains NØI in columns 1-3.

### NØI.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) card NØI.2 is being input.
3. NØISE, number of different noise functions.
- 4.-24. Input but not used.

### NØI.2.E(8E9.0) Gaussian Parameters

This card contains the noise parameters consisting of the full width at half maximum in Mev, a total of NØISE entries.

#### NOTES:

The output for each channel detector appears under the normal output and is headed by the line

\*\*\*CHANNEL AND THRESHOLD COUNT SPREAD DUE TO NOISE\*\*\*

The columns under this heading are the channel index, the upper and lower energy boundaries of the channel and then pairs of columns for each noise function. The first column of each pair contains the adjusted count rate for each channel. The second column is the threshold count rate for all channels down through the given channel.

## PLØt Output

This input section provides for the plotting and punching of calculated quantities.

### PLØ.O.H(24A3) Header Card

Columns 1-3 contain PLØ.

### PLØ.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, not used.
3. NPLØT, (0, 1, 2,3) = (neither,plot,punch,both) option for the differential number flux at each detector.
- 4.-24. Input but not used.

### QUICK Plot of Results

This input section provides a graphical printout of calculated results. The output is provided only on the last print cycle.

#### QUI.O.H(24A3) Header Card

Has QUI in columns 1-3.

#### QUI.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) card QUI.2 is being input.
3. NQUICK, number of different quick plots.
- 4.-24. Input but not used.

#### QUI.2.II(12(2I3)) Plot Requests

This card contains NQUICK pairs of integers. The first integer IQU(I) of each pair usually denotes the quantity (ordinate) being plotted. The second integer JQU(I) usually denotes the independent variable (abscissa).

#### NOTES:

The requested plots appear after the normal printout of the quantities being plotted. Present options include:

	IQU(I)	JQU(I)
1. DEPosition	0	versus region index
	1,2 or 3	versus region x,y, or z coordinates
	4,5 or 6	versus region radius 1 x,y, or z-axis
	7	versus region spherical radius
2 LEAkage output	0,1,...,7	versus outer region index, coordinate or radius as in DEP output.
3 CHannel output	0	counts in channel vs. channel index
	1	counts in channel vs. channel energy
	2	cumulative counts vs. channel index
	3	cumulative counts vs. channel energy
10 Total flux	1	differential number flux versus energy
11 Flux by source region	2	differential energy flux versus energy
12 Scattering region	3	cumulative number flux versus energy
13 Order of scatter	4	cumulative energy flux versus energy
14 Angular moment		
15 Temporal moment		
16 Boundary crossing		

IQU(I)	JQU(I)
17 Solid angle element	
18 Time interval	
19 Initial group	
21 Response by source region	>0 response function index
.	-1 total number flux
.	0 total energy flux
29 Response by initial group	
30 Shield optimization output	0 dose versus iteration 1 weight versus iteration 2 shield thicknesses versus iteration

## ØPTimum Importance Parameters

This input section tells the program to calculate, based on partial derivatives of the variance, better importance sampling parameters.

### ØPT.O.H(24A3) Header Card

Has ØPT in columns 1-3.

### ØPT.I.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, not used.
3. NØBIAS, (0,1)=(no,yes) calculate optimum importance.
- 4.-24. Input but not used.

### NOTES:

If the value of NØBIAS=1, additional output is generated for each response function. The output appears just below the total response and response error output and is preceded by the printout line

### **\*\*\*SUGGESTED CHANGES IN THE IMPORTANCE SAMPLING PARAMETERS\*\*\***

This line is followed by printout lines labeled SPA I. The numbers on this line are suggested changes in the spatial importance of region I for each response function. If these suggested changes are used for a particular response function they would be entered via the SPA input section. After all

the spatial importance parameters are printed, four lines labeled PRE I, I=1,2,3 and 4 are printed. These lines contain suggested values of AT, BT, AS, and BS which are entered via the PRE input section. The four PRE lines are followed by three lines labeled PSE I, I = 1,2 and 3 containing suggested changes for the values of ATA, ATB, and ATC entered in the PSE input section.

The next series of lines are labeled REL I where I is a source index and correspond to the relative source importances defined through the REL input section. The final set of lines are labeled RAT 10\*I+J where I is a source index and J=1,2,...,5 corresponding to the relative importance of source variables entered via the RAT input section.

If the problem was run for secondary particles a second set of similar output is generated and contains suggested importance parameter increments in the primary particle run to improve the secondary calculations.

Both the REL and RAT labeled output contain output for one more source than was specified in the SØU input section. The REL labeled output is of no consequence. The RAT labeled output for the additional source is important for the angular biasing of secondary sources.

## BIAsing Options

This input section provides for changing the probability density function models used in selecting source and scattering points.

### BIA.O.H(24A3) Header Card

Contains BIA in columns 1-3.

### BIA.I.I(24I3) Option Card

1. IN1=0, no effect.

IN1>0, interpret data words 3-6 from this card.

2. IN2≥0, no effect

IN2<0, set up the models according to the built-in criteria.

3. MØDEL P, option for selecting initial particle coordinates.

MØDEL P=0, select the source and then select the spatial source variables in the coordinate system for that source. This model must be used if there are one or more point sources, e.g., when running secondary source tapes.

This model uses built-in data which may be changed via the REL input section for selecting the source and built-in data which may be changed by the RAT input section for selecting the spatial variables.

MØDEL P=1, the spatial coordinates are selected using a spherical coordinate system centered at the "preferred point". The built-in preferred point can be changed via the PRE input section for surface and volume detector problems. For point detector problems where each detector

is run separately, the preferred point is the detector being run. To use this option all sources must be volumetric with each source volume completely covering one or more regions. To restrict the range of the solid angle part of the spherical coordinate selection process, a pseudo spherical source which completely contains all the volume sources is built-in but can be changed via the PSE input section.

The program built-in option is MØDEL<sub>P</sub>=1 unless one or more sources have discrete values for one or more of their spatial variables; in this event MØDEL<sub>P</sub>=0.

#### 4. MØDELQ, initial direction selection model.

MØDELQ=0, select the angular source variables in the source coordinate system. This model must be used if any sources have a discrete value for either or both of the angular source variables. The built-in data used to select the angular variables can be changed via the RAT input section.

MØDELQ=1, select the initial direction as though the initial source point were a scattering point, i.e., according to MØDELV below. The direction before scattering is defined as a unit vector from the center of the sphere containing all the sources to the selected source point. All the radiation sources must be angular or isotropic.

MØDELQ=2, like MØDELQ=0 except the angular source variables are defined in a rotated coordinate system with the z'-axis towards the preferred point.

The program built-in option is MØDELQ=1 unless one or more sources have discrete values for one or more of their angular variables; in this event MØDELQ=0.

5. MØDELU, distance to scattering point selection model.

MØDELU=0, use the exponential transformation.

MØDELU=1, use a curve fit of an approximation to the optimal pdf for the distance to collision.

MØDELU=2, for individual point detectors use the exponential transformation and the approximate optimal criterion for the decision on whether to work forward or backward in selecting the distance to collision.

MØDELU=3, for individual point detectors use the curve fit and the optimal criterion for the forward-backward decision. This is the model built into the program.

6. MØDELV, scattered direction selection model.

MØDELV=0, select the polar angle first measured from the direction before scattering. Then select the azimuthal angle measured from a unit vector directed towards the preferred point.

MØDELV=1, select the polar angle first, measured from the direction towards the preferred point. Then select the azimuthal angle measured from the direction before scattering.

MØDELV=2, very strong preference towards preferred point.  
Do not use this model.

MØDELV=4, the unit directions towards the preferred point and in the direction before scattering are weighted by approximate importance to give an overall preferred direction from which the polar angle is measured. Azimuthal angles are selected as being equiprobable.  
This is the model built into the program.

7. MØDELE, energy importance. The importance of particles in each energy group is proportional to  $\bar{E}^n$  where  $\bar{E}$  is the midpoint energy and n=MØDELE.
- MØDELE=1 is built in, i.e., the relative importance of equal weight particles is set equal to their energy.
8. MØDELM, (0,1)=(continuous,discrete) treatment of energy dependence. MØDELM=0 is built in. If MØDELM=1, the spectrum of energies spanned by a packet is sampled to produce a single mono-energetic packet equivalent to a discrete energy particle.
9. MØDELR, (0,1)=(yes,no) play Russian roulette with the packet based on its last contribution to the calculated results. This is a two step decision based on the contribution from the current collision of a history compared to contributions from all previous collisions of the same history and on the contribution from this history compared to the contribution from all the previous histories. MØDELR=0 is built in.
- 10.-24. Input but not used.

### PSEudo Spherical Sources

This input section defines the sphere enclosing all volume sources which is used to restrict the solid angle range for the M<sub>odelP</sub>=1 option.

#### PSE.O.H(24A3) Header Card

Has PSE in columns 1-3.

#### PSE.1.I(24I3) Option Card

1. IN1, not used.

2. IN2, (0,>0)=(no,yes) card PSE.2 is being input.

IN2<0, the built-in data is used, omit card PSE.2.

3.-24. Input but not used.

#### PSE.2.E(8E9.0) Spherical Source

1. RADIUS, radius (cm) of the smallest sphere which encloses all the sources.

2. XCT(1), x-coordinates (cm) of the center of the sphere.

3. XCT(2), y-coordinates (cm) of the center of the sphere.

4. XCT(3), z-coordinates (cm) of the center of the sphere.

5. ATA, spherical pseudo source sampling, polar angle importance adjustment.

ATA=1.0, all angles equally important. This is built in.

ATA>1.0, shifts importance towards small angle.

ATA<1.0, shifts importance towards large angle,  
numbers in the range  $1.0 \leq ATA \leq 10.0$  work fine. (This  
number must be greater than 0.0)

6. ATB, spherical pseudo source sampling, azimuthal angle importance adjustment.

ATB=1.0, all angles equally important.

ATB>1.0, shifts importance towards  $0^\circ$ .

ATB<1.0, shifts importance away from  $0^\circ$ .

This angle is measured in a rotated coordinate system  
and a little difficult to relate to the true coordinate  
system. The usual procedure is to use ATB=1.0 (this  
number must be greater than 0.0) -- the built-in value.

7. ATC, spherical pseudo source sampling, spatial importance adjustment. The built-in value is ATC=0.7.

ATC=1.0, uses built-in estimate of spatial importance.

ATC>1.0, shifts importance to lower source energies  
(source points closer to the detector).

ATC<1.0, shifts importance to higher source energies  
(source points further away).

General use of numbers  $0.7 < ATC < 1.3$  yield good results.

(The program can be tricked for leakage-type surface and  
volume detector calculations by putting the preferred  
point in the center of the source and using  $ATC \approx -1.0$ ).

8. ATD, flux contribution importance used in cutoff considerations; if all contributions to all detector groups on 2 successive inner iterations of a given outer iteration are less than ATD times the flux already obtained in this outer iteration, then the inner iterations are terminated. The built-in value is ATD = 0.001.

## RELative Source Importance

This input section provides the relative importance of each source to be used with MØDELP=0 in the selection of the source from which a particle starts.

### REL.O.H(24A3) Header Card.

This card has REL in columns 1-3.

### REL.1.I(24I3) Option Card

1. IN1, not used.

2. IN2, (0,>0)=(no,yes) card REL.2 is being input.

IN2<0, define the source importance internally and omit REL.2.

3.-24. Input but not used.

### REL.2.E(8E9.0) Source Importance

This card contains the relative importance of each source, a total of NVMAX entries. Any input source which should not be used for this problem should have an entry of 0.0. The built-in definition of these data uses the total source intensity in Mev/sec as the importance.

## RATios of Source Variable Importance

This input section gives the preferred value of each source variable and the relative importance of the preferred value expressed as a ratio.

### RAT.O.H(24A3) Header Card

Contains RAT in columns 1-3.

### RAT.I.1(24I3) Option Card

1. IN1, not used.

2. IN2, (0,>0)=(no,yes) card RAT.2 is being input.

IN2<0, use built-in definitions and omit card RAT.2.

3.-24. Input but not used.

### RAT.2.E(8E9.0) Source Variable Importance

This card is input as two physical cards per source with a set of cards for each source, NVMAX sets--2\*NVMAX cards. The first card of each set contains the preferred value of each of the 5 source variables (3 spatial - 2 angular) in the order defined on card SØU.2. This preferred value must be in the range of the variable given on card SØU.3 including the end points. The second card of each set gives the relative importance -- expressed as a ratio -- of the preferred value of the variable to the end point farthest away from it. The numbers on the second card of this set must be greater than zero since their logarithms are calculated.

The first three parameters on each card are used if MODELP=0.  
The last two are used if MODELQ=0.

If these data are computed internally, they are defined so that  
the sampling is equally probable over the range of each  
variable.

## PREFerred Point

This input section defines the preferred point for surfaces and/or volume detectors.

### PRE.O.H(24A3) Header Card

This card must contain PRE in columns 1-3.

### PRE.1.I(24I3) Option Card

1. IN1, not used.
2. IN2, ( $0,>0$ )=(no,yes) card PRE.2 is being input.  
IN2<0, the built-in data is used. Omit card PRE.2.
- 3.-24. Input but not used.

### PRE.2.E(8E9.0) Preferred Point

1. DELTA, radius (cm) of a sphere which covers the volume in space where fluxes are being calculated. The center of this sphere is the preferred point if NPINT=0.
2. BDC(1), x-coordinate (cm) of the center of the sphere.
3. BDC(2), y-coordinate (cm) of the center of the sphere.
4. BDC(3), z-coordinate (cm) of the center of the sphere.
5. AT, scaling factor for the spatial importance on the first leg of the scattering triangle.  
AT=1.0, uses built-in parameters.  
AT<1.0, shifts importance to higher energies.

AT>1.0, shifts importance to lower energies.

General use of numbers  $0.6 < AT < 1.2$  yields good results (must be greater than 0.0). AT = 0.9 is built-in.

6. BT, scaling factor for the spatial importance on the second leg of the scattering triangle; should approximate higher order scattering effects, so it is generally less than AT. BT=0.7 for photons and BT=0.5 for neutrons are built-in.  
If MODELU=0, it must be less than AT in absolute magnitude, i.e., BT<AT.

Numbers on the order of  $0.4 < BT < 0.9$  yield good results.

If the trick mentioned in discussing ATC is used, it should also be used here; i.e.,  $-0.9 < BT < -0.4$ . This number cannot = 0.0.

7. AS, scaling factor for preferred direction (towards detector) importance.

AS=1.0, uses built-in parameter.

AS>1.0, forces even more.

AS<1.0, forces less.

AS=0.0, yields no effect.

AS<0.0, forces away and should be used when ATC and BT are < 0.0.

Use of 1.0 yields good results for point detectors (built-in value).

8. BS, scaling factor for scattered direction importance.

BS=1.0, uses group-averaged parameter.

BS>1.0, forces even more.

BS<1.0, forces less.

BS=0.0, no effect from scattered direction.

Use of 1.0 yields good results (built-in value).

## SPAtial Importance

This input section provides for an artificial increase in the importance of scattering in selected regions, particularly useful in generating secondary sources.

### SPA.O.H(24A3) Header Card

Must have SPA in columns 1-3.

### SPA.l.I(24I3) Option Card

1. IN1, not used.

2. IN2, (0,>0)=(no,yes) card SPA.2 is being input.

IN2<0, built-in definition is used and card SPA.2 is omitted.

3.-24. Input but not used.

### SPA.2.E(8E9.0) Importance Factors

This card contains the relative importance of scattering in each geometric region, a total of NRMAX entries.

### CAPture Importance

This input section will eliminate the strong forward bias used in calculating fast neutron dose and substitute a more analog bias consistent with calculating good capture source distributions. The decision is made at random on each neutron collision.

### CAP.0.H(24A3) Header Card

Contains CAP in columns 1-3.

### CAP.1.I(24I3) Option Card

1. IN1, not used.
2. IN2, (0,>0)=(no,yes) card CAP.2 is being input.
- 3.-24. Input but not used.

### CAP.2.E(8E9.0) Capture Model Probabilities

This card contains an entry for every region, NRMAX total entries. Each entry is the probability, given that a collision occurs in the region, that the packet will be followed by an "analog" rather than a strongly biased technique.

## SHØrt Circuit

This section provides for the definition of a sphere of influence such that if a particle and point detector are on opposite sides, the plane defining the half spaces used in the selection of the next scattering point subdivides the line between the particle and detector at the intersection of the line with the sphere rather than at the line midpoint.

### SHØ.0.H(24A3) Header Card

Contains SHØ in columns 1-3.

### SHØ.1.I(24I3) Option Card

1. IN1, not used.

2. IN2, (0,>0)=(no,yes) card SHØ.2 is being input.

IN2<0, use built-in definition and omit card SHØ.2.

3.-24. Input but not used.

### SHØ.2.E(8E9.0) Sphere

1. DIM, radius (cm) of sphere.

2. CØR(1), x-coordinate (cm) of sphere.

3. CØR(2), y-coordinate (cm) of sphere.

4. COR(3), z-coordinate (cm) of sphere.

- 5. PTH(1), detector out, particle out of sphere } , minimum probability
- 6. PTH(2), detector out, particle in sphere } with which the scattering point
- 7. PTH(3), detector in, particle out of sphere } is selected by working back-
- 8. PTH(4), detector in, particle in sphere } ward from the detector

## ROTate and Translate

This input section provides for the rotation and/or translation of surfaces, points in region, detector points, pseudo source center, preferred point, and sources.

### ROT.O.H(24A3) Header Card

Columns 1-3 contain ROT.

### ROT.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data word 3 from this card.
2. IN2, (0,>0)=(no,yes) card ROT.2 is being input.
3. NRTRA, total number of rotations and/or translations.
- 4.-24. Input but not used.

### ROT.R(12I3,4E9.0) Rotation Parameters

Input this card NRTRA times.

1. NAXIS, (1,2,3) = rotate (x into y, y into z, z into x).  
NAXIS=0, translation only.
2. MINS, index of first surface. MINS=0, no surface operations.
3. MAXS, index of last surface.
4. MINR, index of first region. MINR=0, no region operations.
5. MAXR, index of last region.

6. MIND, index of first detector. MIND=0, no detector operations.
  7. MAXD, index of last detector.
  8. IDM(8), (0,>0)=(no,yes) operate on pseudo source center.
  9. IDM(9), (0,>0)=(no,yes) operate on preferred point.
  10. IDM(10), index of first source to be rotated or translated.
  11. IDM(11), index of last source to be rotated or translated.
  12. Input but not used.
  13. THETA $\neq$ 0.0, rotation in degrees.  
THETA=0.0, translation.
  14. XTR(1)
  15. XTR(2)
  16. XTR(3)
- },
- origin for rotation if NAXIS>0,  
translation vector (cm) if NAXIS=0.

## ARRay Direct Input

This section can be used for direct input of the elements in a data array. The use of this section can simplify the data input for some problems. However, an intimate knowledge of the program is recommended before using this input section. The array names are given in Appendix C.

### ARR.O.H(24A3) Header Card

Columns 1-3 must contain ARR.

The name of the array is extracted from the first set of 3 nonblank columns starting with column 7 or 10, or 13, ..., or 70.

### ARR.1.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-12 (as required) from this card.
2. IN2, (0,>0)=(no,yes), card ARR.2 or ARR.3 is being input.
3. IFT=1, the elements of the array are being input between specified limits on I,J, and K (all arrays are assumed 3-dimensional).  
IFT=2, the index of each element (as a one-dimensional array) is read and then the element is read -- logical pair input. This option is not available for BCD arrays.  
IFT=3, the entire array is being input.
4. MNK = number of logical pairs being input if IFT=2.

5. MXK  
6. MDK  
7. MNJ  
8. MXJ    used only if IFT=1;  
9. MDJ    see ARR.2 below  
10. MNI  
11. MXI  
12. MDI

13.-24. Input but not used.

ARR.2.  $\left\{ \begin{array}{l} I(24I3) \\ E(8E9.0) \\ A(24A3) \end{array} \right\}$  Array Elements

Input all array elements on this card if IFT=3.  
If IFT=1, input the following elements:

(( (ARR(K,J,I), K=MNK, MXK, MDK), J=MNJ, MXJ, MDJ ), I=MNI, MXI, MDI )

ARR.3.  $\left\{ \begin{array}{l} IS(12(2I3)) \\ ES(6(I3,E9)) \end{array} \right\}$  Index and Array Elements

If IFT=2, input MNK pairs of data consisting of the index of an array element followed by the element itself.

## DUMp Requests

This section provides for the dumping of specified named common blocks and arrays at selected points in most subprograms. See Appendix C for the common blocks and arrays.

### DUM.O.H(24A3) Header Card

This card has DUM in columns 1-3.

### DUM.1.I(24I3) Option Card

1. IN1, (0, >0)=(no,yes) interpret data words 3 and 4 from this card.
2. IN2, (0, >0)=(no, number of dump requests) input on cards DUM.2 and DUM.3.
3. NDUMPS, number of dump points.
4. NVAMAX, maximum number of arrays to be dumped at a dump point.
5. NCBMAX, maximum number of named common blocks.
- 6.-24. Input but not used.

Input cards DUM.2 and DUM.3 in sets, a total of IN2 sets.

### DUM.2.I(24I3) Dump Limits

1. I, index of the dump request,  $1 \leq I \leq NDUMPS$ .
2. NVA(I) , number of arrays in this dump request.

- NVA(I)<0, use array list for dump request J = -NVA(I).  
NVA(I)≥500, dump all arrays.
3. IFN(I), dump point, e.g., 1 = subroutine entrance point,  
9 = exit point.
  4. NDN(I), index of the first pass through the routine on  
which the dump will be given.
  5. NDX(I), index of the last pass on which the dump will  
be made.
  6. MXC, number of common blocks to be dumped.  
MSC≥100, dump all common blocks.
  7. Indices of named common blocks, e.g., 41 for named common
  8. C41; omit if MSC≥100.
  - ⋮

#### DUM.3.A(24A3) Subroutine and Array Names

- 1.-2. name of the subroutine in which the dump will be made.
- 3.,4,..., names of arrays to be dumped or blanks. Omit if  
NVA(I) ≥ 500.

Blank A3 words on this card are ignored so that the input  
can be prepared in a more readable manner.

## PRIInt Suppression

This section permits suppression of printing of input card images with the exception of header cards and comment cards encountered while searching for a header card. This section also permits the resumption of printing card images following a prior suppression. The suppression does not carry over into succeeding cases.

### PRI.O.H(24A3) Header Card

Must contain PRI in columns 1-3.

### PRI.I.1(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret the third data word on this card.
2. IN2, not used.
3. LIN $\emptyset$ UT, (0,1)=(yes,no) print input card images.
- 4.-24. Input but not used.

NEXT Case

This control section tells the program to proceed to the next case without executing the problem data. The program responds by incrementing the case index and initializing the page and line count indices.

NEX.O.H(2<sup>4</sup>A3) Header Card

Must contain NEX in columns 1-3.

NEX.1.I(2<sup>4</sup>I3) Option Card

1.-24. Input but not used.

### EXEcute the Problem

This section tells the program that all the necessary inputs have been provided. The program then allocates storage for additional arrays used during the execution of the problem. A printout line is then written.

\*\*\*THIS CASE USES I LOCATIONS FOR INPUT, J LOCATIONS TO RUN\*\*\*

If any errors are detected during data input, the above line is followed by the line

\*\*\*PROCEEDING TO THE NEXT CASE\*\*\*

and the execution is not performed. If the input data is acceptable, the following line is printed

G0\*G0\*G0\*G0\*G0\*G0

and the problem is then executed.

### EXE.O.H(24A3) Header Card

Must have EXE in columns 1-3.

### EXE.I(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-6 from this card.
2. IN2, not used.
3. NP0INT=0, calculate fluxes for surface, volume and/or point detectors using only one set of particle histories. Any point detectors should not lie in a source volume

or scattering medium if a meaningful, finite variance, answer is desired.

NPQINT=1, calculate fluxes for point detectors using a different set of particle histories for each detector. Point detectors can be located anywhere since the history set generated for each detector ensures a finite variance flux calculation.

4. NPRINT > 0, number of printouts of calculated fluxes during the calculation. The intermediate prints permit partial salvage of the results for problems which terminate abnormally. Alternatively, if a nonzero restart unit is designated on card TAP.1, the problem data will be saved on the restart tape at the start of each print loop for possible use later; see the CQNTINUE input section.

NPRINT=0, the program performs all steps up to the actual execution of the problem and then proceeds to the next case even though the error indicator is not set.

5. NUNITS, number of histories to be generated between each printout.
6. KALIDE, maximum number of collisions per particle.
- 7.-24. Input but not used.

### CØNtinue a Previous Run

This input section tells the program to read the restart tape generated during a previous run and continue execution of the problem on that tape.

#### CØN.O.H(24A3) Header Card

Must contain CØN in columns 1-3.

#### CØN.I.(24I3) Option Card

1. IN1, (0,>0)=(no,yes) interpret data words 3-6 from this card.

2. IN2, not used.

3. NPØINT

4. NPRINT

5. NUNITS

6. KALIDE

} Same definitions (possibly different values) as the same variables in the EXECUTE input section

7.-24. Input but not used.

STØp Processing

This section permits termination of the computer run by a programmed stop rather than terminating the run by encountering an end of file while trying to read input data for a nonexistent problem.

STØ.O.H(24A3) Header Card

Must have STØ in columns 1-3.

STØ.1.I(24I3) Option Card

1.-24. Input but not used.

Appendix B  
SAMPLE PROBLEM PRINTOUT

This appendix contains the complete printout from a sample problem. The problem involved the calculations of dose rates at a specified point from primary neutrons and photons and from secondary photons for a spherical reactor-shield configuration. The dose rates and dose rate derivatives with respect to shield thickness were then used to calculate a minimum weight shield configuration. The complete problem description and results of full length runs are given in Volume I of this report.

The printout includes all the data card images -- with one exception -- so a separate listing of these data cards is not given. A part of the lengthy printout of microscopic cross section card images is not included. Numerous comment cards are included in the data deck to clarify the problem description.

THE FASTER-III PROGRAM \*\*\*\*\*CASE 1  
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\*\*\*\*\*  
CARD IMAGE \*\*\*.000.001.H C ZEROUT INPUT SECTION IS NOT INPUT SINCE CORE IS ZEROED BEFORE FIRST CASE  
CARD IMAGE \*\*\*.000.002.H C ZEROUT SECTION WOULD BE USED BETWEEN MULTIPLE INDEPENDENT PROBLEMS  
CARD IMAGE \*\*\*.000.003.H C ZEROUT DOES NOT ZEROUT TAPE LOGICAL DESIGNATIONS, EVERYTHING ELSE  
\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890

CARD IMAGE TAP.000.001.H TAP E UNITS  
CARD IMAGE TAP.001.001.I C IN1 = 1, TAPE UNITS ARE BEING SPECIFIED  
CARD IMAGE TAP.001.002.I C IN2 = 0, NOT USED  
CARD IMAGE TAP.001.003.I C M5 = 9, NEUTRON COLLISION PARAMETERS WILL GO ON THIS TAPE  
CARD IMAGE TAP.001.004.I 1 0 0 0 9 0 0 0  
\*\*\*\*\*  
\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890

CARD IMAGE LAB.000.001.H LAB EL FOR PRINTOUT  
CARD IMAGE LAB.001.001.I C IN1 = 1, NOT USED ANYWAY  
CARD IMAGE LAB.001.002.I C IN2 = 1, LABEL CARDS ARE BEING INPUT  
CARD IMAGE LAB.001.003.I C NO COMMENT CARDS CAN FOLLOW THE NEXT CARD SINCE AN A FORMAT IS USED FOR INPUT  
CARD IMAGE LAB.001.004.I 1 1  
CARD IMAGE LAB.002.001.A \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*  
CARD IMAGE LAB.002.002.A \*\*\*\*\*PRIMARY NEUTRONS\*\*\*\*\*  
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CARD IMAGE MAT.000.001.H MAT ERIAL COMPOSITIONS  
CARD IMAGE MAT.001.001.I C IN1 = 1, LIMITS AND OPTIONS ARE BEING INPUT  
CARD IMAGE MAT.001.002.I C IN2 = 1, COMPOSITIONS ARE BEING INPUT  
CARD IMAGE MAT.001.003.I C NIMAX = 9, NINE ELEMENTS IN COMPOSITION TABLE  
CARD IMAGE MAT.001.004.I C NMMAX = 7, SEVEN MATERIALS ARE BEING DEFINED  
CARD IMAGE MAT.001.005.I C NUNITD = 0(IMPLIED), COMPOSITIONS IN E+24 ATOMS/CC  
CARD IMAGE MAT.001.006.I ,1,1,9,7/  
CARD IMAGE MAT.002.001.E C HYDROGEN  
CARD IMAGE MAT.002.002.E ,1.0813,1.,0197,,,0451,.0516,.058,,0645/ H  
CARD IMAGE MAT.003.001.E C BERYLLIUM  
CARD IMAGE MAT.003.002.E ,9.013,4,0,.12/  
CARD IMAGE MAT.004.001.E C BORON  
CARD IMAGE MAT.004.002.E ,11,5,,,000671,.000766,.000862,.000958/ B  
CARD IMAGE MAT.005.001.E C OXYGEN  
CARD IMAGE MAT.005.002.E ,16,8,,01146,,,0235,.0268,.0302,.0337/ O  
CARD IMAGE MAT.006.001.E C ALUMINUM

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 CARD IMAGE MUL.006.065.F 0 +28600- 7 0 + 0+ 0 0 +58883- 5 0 +47410- 6 0 +69710- 6 0 +51690- 6 1  
 CARD IMAGE MUL.006.066.F 0 +39930- 6 0 +31850- 6 0 +26580- 6 0 +22390- 6 0 +20160- 6 0 +15250- 6 2  
 CARD IMAGE MUL.006.067.F 32R+ 0+ 0 3 2  
 CARD IMAGE MUL.006.068.F 0 +10900- 7 0 + 0+ 0 0 +67099- 5 0 +83410- 6 0 +11202- 5 0 +79270- 6 1  
 CARD IMAGE MUL.006.069.F 0 +61290- 6 0 +49130- 6 0 +40460- 6 0 +34580- 6 0 +30320- 6 0 +27080- 6 2  
 CARD IMAGE MUL.006.070.F 0 +20970- 631R+ 0+ 0 3  
 CARD IMAGE MUL.006.071.F 0 +19000- 8 0 + 0+ 0 0 +80022- 5 0 +15625- 5 0 +17848- 5 0 +11571- 5 1  
 CARD IMAGE MUL.006.072.F 0 +88060- 6 0 +71870- 6 0 +60180- 6 0 +51290- 6 0 +44920- 6 0 +40080- 6 2  
 CARD IMAGE MUL.006.073.F 0 +36260- 6 0 +28670- 6 0 +82487- 8 0 +17637- 8 0 +10863- 8 0 +62926- 9 3  
 CARD IMAGE MUL.006.074.F 0 +35717- 9 0 +20374- 9 0 +98099- 1023R+ 0+ 0 4  
 CARD IMAGE MUL.006.075.F 2R+ 0+ 0 0 +10470- 4 0 +45503- 5 0 +38472- 5 0 +23414- 5 0 +17849- 5 1  
 CARD IMAGE MUL.006.076.F 0 +14857- 5 0 +12819- 5 0 +11161- 5 0 +97780- 6 0 +87130- 6 0 +78650- 6 2  
 CARD IMAGE MUL.006.077.F 0 +71700- 6 0 +57320- 6 0 +15151- 7 0 +32394- 8 0 +19952- 8 0 +11558- 8 3  
 CARD IMAGE MUL.006.078.F 0 +65602- 9 0 +37422- 9 0 +18018- 922R+ 0+ 0 4  
 CARD IMAGE MUL.006.079.F 2R+ 0+ 0 0 +13683- 4 0 +49186- 5 0 +31630- 5 0 +16007- 5 0 +12015- 5 1  
 CARD IMAGE MUL.006.080.F 0 +97620- 6 0 +83030- 6 0 +72220- 6 0 +63020- 6 0 +55160- 6 0 +49030- 6 2  
 CARD IMAGE MUL.006.081.F 0 +44120- 6 0 +40110- 6 0 +31830- 628R+ 0+ 0 3  
 CARD IMAGE MUL.006.082.F 2R+ 0+ 0 0 +16185- 4 0 +86429- 5 0 +77941- 5 0 +27570- 5 0 +98990- 6 1  
 CARD IMAGE MUL.006.083.F 0 +53720- 6 0 +34740- 6 0 +25000- 6 0 +18960- 6 0 +14560- 6 0 +11300- 6 2  
 CARD IMAGE MUL.006.084.F 0 +90700- 7 0 +74800- 7 0 +63000- 7 0 +42300- 727R+ 0+ 0 3  
 CARD IMAGE MUL.006.085.F 2R+ 0+ 0 2R+19102- 4 0 +75420- 5 0 +97080- 638R+ 0+ 0 1  
 C P1  
 CARD IMAGE MUL.007.001.F  
 CARD IMAGE MUL.007.002.F 2R+ 0+ 0 0 +83738- 5 0 +16991- 440R+ 0+ 0 1  
 CARD IMAGE MUL.007.003.F 2R+ 0+ 0 0 +92835- 5 0 +17259- 4 0 +42476- 539R+ 0+ 0 1  
 CARD IMAGE MUL.007.004.F 2R+ 0+ 0 0 +10168- 4 0 +18192- 4 0 +44522- 5 0 -12122- 538R+ 0+ 0 1  
 CARD IMAGE MUL.007.005.F 2R+ 0+ 0 0 +11591- 4 0 +20010- 4 0 +34364- 5 0 -16356- 5 0 -83940- 7 1  
 CARD IMAGE MUL.007.006.F 37R+ 0+ 0 2  
 CARD IMAGE MUL.007.007.F 2R+ 0+ 0 0 +12526- 4 0 +18679- 4 0 +34575- 5 0 -11066- 538R+ 0+ 0 1  
 CARD IMAGE MUL.007.008.F 2R+ 0+ 0 0 +13300- 4 0 +18606- 4 0 +43694- 5 0 -22679- 538R+ 0+ 0 1  
 CARD IMAGE MUL.007.009.F 2R+ 0+ 0 0 +17588- 4 0 +23051- 4 0 +17771- 5 0 -32860- 5 0 -17879- 6 1  
 CARD IMAGE MUL.007.010.F 37R+ 0+ 0 2  
 CARD IMAGE MUL.007.011.F 2R+ 0+ 0 0 +23819- 4 0 +34306- 4 0 +55909- 5 0 -18140- 538R+ 0+ 0 2  
 CARD IMAGE MUL.007.012.F 2R+ 0+ 0 0 +17076- 4 0 +13326- 4 0 +82960- 5 0 -25136- 538R+ 0+ 0 1  
 CARD IMAGE MUL.007.013.F 2R+ 0+ 0 0 +14113- 4 0 +14017- 4 0 +90136- 5 0 -83871- 5 0 -42595- 5 1  
 CARD IMAGE MUL.007.014.F 37R+ 0+ 0 2

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CARD IMAGE MUL.044.049.F	0 -20620- 429R+ 0+ 0	3
CARD IMAGE MUL.044.050.F	3R+ 0+ 0 0 +18361- 3 0 -92816- 4 0 +39621- 4 0 +53386- 4 0 +48791- 4	1
CARD IMAGE MUL.044.051.F	0 +42595- 4 0 +36982- 4 0 +31782- 4 0 +27190- 4 0 +23589- 4 0 +20729- 4	2
CARD IMAGE MUL.044.052.F	0 +18422- 4 0 +13847- 428R+ 0+ 0	3
CARD IMAGE MUL.044.053.F	3R+ 0+ 0 0 +77956- 4 0 -42209- 4 0 +41704- 4 0 -62083- 5 0 -17340- 4	1
CARD IMAGE MUL.044.054.F	0 -17546- 4 0 -15784- 4 0 -13818- 4 0 -11846- 4 0 -10039- 4 0 -85970- 5	2
CARD IMAGE MUL.044.055.F	0 -74451- 5 0 -65167- 5 0 -46988- 527R+ 0+ 0	3
CARD IMAGE MUL.044.056.F	3R+ 0+ 0 0 +52635- 4 0 -14391- 5 0 -42309- 438R+ 0+ 0	1

\*\*\*\*\*C ADD RESS MODIFICATION IS NOT REQUIRED

\*\*\*\*\*1234567890123456789012345678901234567890123456789012345678901234567890

CARD IMAGE SOU.000.001.H	SOURCE
CARD IMAGE SOU.001.001.I	C IN1 = 1, LIMITS ARE BEING INPUT
CARD IMAGE SOU.001.002.I	C IN2 = 1, ONE SOURCE IS BEING INPUT
CARD IMAGE SOU.001.003.I	C NVMAX = 1, THIS PROBLEM HAS ONLY ONE SOURCE
CARD IMAGE SOU.001.004.I	C NXMAX = 2, THERE ARE A MAXIMUM OF TWO POINTS IN ANY SOURCE DISTRIBUTION
CARD IMAGE SOU.001.005.I	1 1 1 2
CARD IMAGE SOU.002.001.R	C SPHERICAL GEOMETRY EQUIPROBABLE SPATIAL AND ANGULAR DISTRIBUTIONS
CARD IMAGE SOU.002.002.R	C FISSION NEUTRON SPECTRUM GENERATED INTERNALLY
CARD IMAGE SOU.002.003.R	1 2 2 2 2 2 2 80 0 0 2 1 2.91+19
CARD IMAGE SOU.003.001.EE	C RADIAL DISTRIBUTION
CARD IMAGE SOU.003.002.EE	,0,1,87,1/
CARD IMAGE SOU.004.001.EE	C AZIMUTHAL DISTRIBUTION(SPATIAL)
CARD IMAGE SOU.004.002.EE	-3.1416 1.0 3.1416 1.0
CARD IMAGE SOU.005.001.EE	C POLAR DISTRIBUTION(SPATIAL)
CARD IMAGE SOU.005.002.EE	-1.0 1.0 1.0 1.0
CARD IMAGE SOU.006.001.EE	C AZIMUTHAL DISTRIBUTION(ANGULAR)
CARD IMAGE SOU.006.002.EE	-3.1416 1.0 3.1416 1.0
CARD IMAGE SOU.007.001.EE	C POLAR DISTRIBUTION(ANGULAR)
CARD IMAGE SOU.007.002.EE	-1.0 1.0 1.0 1.0
CARD IMAGE ***.000.001.H	C PRO FILES OF SOURCE TIME DEPENDENCE ARE NOT INPUT
CARD IMAGE SUR.000.001.H	SURFACES
CARD IMAGE SUR.001.001.I	C IN1 = 1, LIMITS ARE BEING INPUT

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CARD IMAGE SUR.001.002.I C IN2 = 8, EIGHT SURFACES ARE BEING INPUT  
CARD IMAGE SUR.001.003.I C NSMAX = 8, EIGHT SURFACES TOTAL FOR THIS PROBLEM  
CARD IMAGE SUR.001.004.I C NAMAX = 6, ALL SURFACES HAVE SIX COEFFICIENTS

CARD IMAGE SUR.001.005.I ,1,8,8,6/  
CARD IMAGE SUR.002.001.S C CORE BOUNDARY  
CARD IMAGE SUR.002.002.S ,1,,13,,87,,87,,87/  
CARD IMAGE SUR.003.001.S C REFLECTOR BOUNDARY  
CARD IMAGE SUR.003.002.S ,2,,13,,90,,90,,90/  
CARD IMAGE SUR.004.001.S C DEPLETED URANIUM SHIELD BOUNDARY  
CARD IMAGE SUR.004.002.S ,3,,13,,95,,95,,95/  
CARD IMAGE SUR.005.001.S C SHIELD MIX1 BOUNDARY  
CARD IMAGE SUR.005.002.S ,4,,13,,152,,152,,152/  
CARD IMAGE SUR.006.001.S C SHIELD MIX2 BOUNDARY  
CARD IMAGE SUR.006.002.S ,5,,13,,167,,167,,167/  
CARD IMAGE SUR.007.001.S C SHIELD MIX3 BOUNDARY  
CARD IMAGE SUR.007.002.S ,6,,13,,182,,182,,182/  
CARD IMAGE SUR.008.001.S C BORATED WATER SHIELD BOUNDARY  
CARD IMAGE SUR.008.002.S ,7,,13,,299,,299,,299/  
CARD IMAGE SUR.009.001.S C LARGE OUTER BOUNDARY TO ENCLOSE POINT DETECTOR  
CARD IMAGE SUR.009.002.S ,8,,13,,1000000,,1000000,,1000000/

\*\*\*\*\*C HELICAL SURFACES ARE NOT INVOLVED IN THE GEOMETRY  
\*\*\*\*\*1234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890

CARD IMAGE REG.000.001.H REGIONS  
CARD IMAGE REG.001.001.I C IN1 = 1, LIMITS ARE BEING INPUT  
CARD IMAGE REG.001.002.I C IN2 = 8, EIGHT REGIONS ARE BEING INPUT  
CARD IMAGE REG.001.003.I C NRMAX = 8, THERE ARE EIGHT REGIONS IN THIS PROBLEM  
CARD IMAGE REG.001.004.I C NBMAX = 2, THERE ARE A MAXIMUM OF TWO BOUNDARIES PER REGION  
CARD IMAGE REG.001.005.I ,1,8,8,2/  
CARD IMAGE REG.002.001.R C CORE  
   1 1 1 1               1.0     0.0  
CARD IMAGE REG.002.002.R C REFLECTOR  
   2 0 2 1 2            1.0     88.0  
CARD IMAGE REG.003.001.R C DEPLETED URANIUM SHIELD  
   3 0 3 2 3            1.0     92.0  
CARD IMAGE REG.004.001.R  
CARD IMAGE REG.004.002.R

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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE REG.005.001.R C MIX1 SHIELD  
CARD IMAGE REG.005.002.R 4 0 4 3 4 1.0 120.0  
CARD IMAGE REG.006.001.R C MIX2 SHIELD  
CARD IMAGE REG.006.002.R 5 0 5 4 5 1.0 160.0  
CARD IMAGE REG.007.001.R C MIX3 SHIELD  
CARD IMAGE REG.007.002.R 6 0 6 5 6 1.0 170.0  
CARD IMAGE REG.008.001.R C BORATED WATER SHIELD  
CARD IMAGE REG.008.002.R 7 0 7 6 7 1.0 200.0  
CARD IMAGE REG.009.001.R C VOID  
CARD IMAGE REG.009.002.R 8 0 0 7 8 0.0 400.0  
\*\*\*\*\*  
CARD IMAGE \*\*\*.000.001.H C CYLINDRICAL GEOMETRY IS NOT USED  
CARD IMAGE \*\*\*.000.002.H C SPHERICAL GEOMETRY COULD HAVE BEEN USED IN PART  
CARD IMAGE \*\*\*.000.003.H C AIR DENSITY IS USED ONLY FOR TRANSPORT IN THE UPPER ATMOSPHERE  
CARD IMAGE \*\*\*.000.004.H C CHECK RAY TRACE OPTION IS NOT USED FOR THIS SIMPLE GEOMETRY  
CARD IMAGE \*\*\*.000.005.H C COR RELATED CALCULATIONS ARE NOT PERFORMED  
\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE DET.000.001.H DETECTOR  
CARD IMAGE DET.001.001.I C IN1 = 1, LIMITS ARE BEING INPUT  
CARD IMAGE DET.001.002.I C IN2 = 1, ONE DETECTOR IS BEING INPUT  
CARD IMAGE DET.001.003.I C NDMAX = 1, THERE IS ONLY ONE DETECTOR FOR THIS PROBLEM  
CARD IMAGE DET.001.004.I 1 1 1  
CARD IMAGE DET.002.001.S C POINT DETECTOR AT 30 FEET FROM CORE CENTER  
CARD IMAGE DET.002.002.S ,1,0,0,1,0,0,1,0,0,914.14/  
\*\*\*\*\*  
CARD IMAGE \*\*\*.000.001.H C FLUX GROUPS ARE NOT INPUT, THE OUTPUT WILL BE IN THE CROSS SECTION GROUPS  
\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE RES.000.001.H RESPONSES  
CARD IMAGE RES.001.001.I C IN1 = 1, LIMITS ARE BEING INPUT  
CARD IMAGE RES.001.002.I C IN2 = 4, FOUR RESPONSES ARE BEING INPUT  
CARD IMAGE RES.001.003.I C NFMAX = 4, THERE ARE A TOTAL OF FOUR RESPONSE FUNCTIONS  
CARD IMAGE RES.001.004.I C COMMENT CARDS CANNOT FOLLOW THE NEXT CARD  
CARD IMAGE RES.001.005.I 1 4 4  
CARD IMAGE RES.002.001.A MEV/CC-H2O RADS/HOUR REM/HR(TMJ) REM/HR(GHA)  
CARD IMAGE RES.003.001.S C PICKUP ENERGY ABSORPTION FOR BORATED WATER = MATERIAL 7

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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE RES.003.002.S 1 0 7 7.69-5  
CARD IMAGE RES.004.001.S 2 0 0 1.0-5 2.05 2.05 2.05 1.84 1.76 1.66  
CARD IMAGE RES.005.001.E 1.51 1.37 1.15 1.12 1.08 0.94 0.83 0.72  
CARD IMAGE RES.005.002.E 0.65 0.54 0.17 0.032 0.0072 0.0013 0.00036 3.6-4  
CARD IMAGE RES.005.003.E 5.4-4 9.5-4 1.5-3 4.0-3 0.0  
CARD IMAGE RES.006.001.S 3 0 0 1.0-4 1.15 1.15 1.15 1.12 1.07 1.09  
CARD IMAGE RES.007.001.E 1.10 0.95 0.95 0.95 0.93 0.91 0.90 0.80  
CARD IMAGE RES.007.002.E 0.60 0.54 0.54 0.21 0.05 0.05 0.05 0.05  
CARD IMAGE RES.007.003.E 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05  
CARD IMAGE RES.008.001.S 4 0 0 1.0-4 1.51 1.51 1.51 1.48 1.44 1.37  
CARD IMAGE RES.009.001.E 1.30 1.26 1.24 1.22 1.26 1.28 1.31 1.25  
CARD IMAGE RES.009.002.E 0.85 0.69 0.32 0.06 0.06 0.06 0.06 0.06  
CARD IMAGE RES.009.003.E 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06

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CARD IMAGE BIR.000.001.H BIRTH  
CARD IMAGE BIR.001.001.I C IN1 = 1, LIMIT IS BEING INPUT  
CARD IMAGE BIR.001.002.I C IN2 = 1, INDICES OF BIRTH REGIONS ARE BEING INPUT  
CARD IMAGE BIR.001.003.I C NVMOD = 7, THE PROGRAM WILL PRINT THE FLUXES BY BIRTH REGION FOR SEVEN REGIONS  
CARD IMAGE BIR.001.004.I C LIST OF BIRTH REGIONS  
CARD IMAGE BIR.001.005.I ,1,1,7/,1,2,3,4,5,6,7/

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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE ORD.000.001.H ORDER  
CARD IMAGE ORD.001.001.I C IN1 = 1, INTERPRET LIMIT  
CARD IMAGE ORD.001.002.I C IN2 = 0, NOT USED  
CARD IMAGE ORD.001.003.I C NCMAX = 8, ORDER OF SCATTER FLUXES THROUGH SEVENTH SCATTER  
CARD IMAGE ORD.001.004.I 1 0 8

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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE SCA.000.001.H SCATTERING REGIONS  
CARD IMAGE SCA.001.001.I C IN1 = 1, INTERPRET LIMIT  
CARD IMAGE SCA.001.002.I C IN2 = 1, SCATTERING REGIONS ARE BEING DEFINED  
CARD IMAGE SCA.001.003.I C NSRMAX = 7, SEPARATE TALLY OF SCATTERED FLUX FROM ALL SEVEN NON-VOID REGIONS  
CARD IMAGE SCA.001.004.I 1 1 7

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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE SCA.002.001.I C SCATTERING REGION INDICES  
CARD IMAGE SCA.002.002.I 1 2 3 4 5 6 7  
\*\*\*\*\*  
CARD IMAGE \*\*\*.000.001.H C BOU NDARY CROSSING TALLY NOT REQUESTED  
CARD IMAGE \*\*\*.000.002.H C ANG ULAR FLUXES NOT REQUESTED  
CARD IMAGE \*\*\*.000.003.H C SOL ID ANGLE FLUXES ARE NOT REQUESTED  
CARD IMAGE \*\*\*.000.004.H C TRA NSLATION TIME IS USED ONLY FOR TIME DEPENDENT PROBLEMS  
CARD IMAGE \*\*\*.000.005.H C MOM ENT'S OF TEMPORAL FLUXES NOT REQUESTED  
CARD IMAGE \*\*\*.000.006.H C TIM E INTERVAL FLUXES ARE NOT REQUESTED  
CARD IMAGE \*\*\*.000.007.H C GRO UP EDIT ON FLUXES IS NOT REQUESTED  
\*\*\*\*\*1234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE NOR.000.001.H NORMAL  
CARD IMAGE NOR.001.001.I C IN1 = 1, LIMITS ARE BEING INPUT  
CARD IMAGE NOR.001.002.I C IN2 = 1, NORMAL DERIVATIVE LOCATIONS ARE BEING DEFINED BY INPUT  
CARD IMAGE NOR.001.003.I C NORMLD = 5, THERE ARE FIVE NORMAL DERIVATIVE LOCATIONS  
CARD IMAGE NOR.001.004.I C NORCOM = 2, TWO COMPONENTS ARE ALLOWED--THE SECOND SHOULD GET ALL ZERO  
C RESULTS SINCE ALL PARTICLES SHOULD SEE THE FIRST COMPONENT SHIELDS  
CARD IMAGE NOR.001.005.I ,1,1,5,2/  
CARD IMAGE NOR.002.001.II C DEFINITION OF BOUNDARY CROSSINGS AT WHICH DERIVATIVES WILL BE COMPUTED  
CARD IMAGE NOR.002.002.II ,3,3,4,4,5,5,6,6,7,7/  
CARD IMAGE NOR.003.001.I C DEFINITION OF FIRST COMPONENT  
CARD IMAGE NOR.003.002.I ,1,2,3,4,5/  
CARD IMAGE NOR.004.001.I C DEFINITION OF SECOND COMPONENT  
CARD IMAGE NOR.004.002.I ,0,0,0,0,0/  
\*\*\*\*\*1234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE MIN.000.001.H MINIMUM WEIGHT  
CARD IMAGE MIN.001.001.I C IN1 = 1, LIMITS AND OPTIONS ARE BEING INPUT  
CARD IMAGE MIN.001.002.I C IN2 = 5, DOSE RATE CONSTRAINT AND FIVE INITIAL CONDITION CARDS ARE INPUT  
CARD IMAGE MIN.001.003.I C IPRESP = 1, INDEX OF RESPONSE FOR SECONDARY  
CARD IMAGE MIN.001.004.I C ISRESP = 4, INDEX OF RESPONSE FOR PRIMARY(NEUTRON)  
CARD IMAGE MIN.001.005.I C ITPRIN = 10, PRINTOUT EVERY TEN ITERATIONS DURING SHIELD OPTIMIZATION  
CARD IMAGE MIN.001.006.I C ITERMX = 1000, MAXIMUM NUMBER OF ITERATIONS DURING OPTIMIZATION  
CARD IMAGE MIN.001.007.I ,1,5,1,4,10,1000/  
CARD IMAGE MIN.002.001.E C DOSE RATE CONSTRAINT

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*****1234567890123456789012345678901234567890123456789012345678901234567890
CARD IMAGE MIN.002.002.E ,1-6/ DOSE RATE CONSTRAINT SET LOW TO ENSURE ITERATIONS WITH FEW HISTORIES
CARD IMAGE MIN.003.001.S C SHIELD ONE, DEPLETED URANIUM OUTER BOUNDARY
CARD IMAGE MIN.003.002.S ,1,2,2,5,0,1000,90,19,2+6/
CARD IMAGE MIN.004.001.S C SHIELD TWO, MIX1 OUTER BOUNDARY
CARD IMAGE MIN.004.002.S ,2,2,3,57,0,1000,95,6,4,7+5/
CARD IMAGE MIN.005.001.S C SHIELD THREE, MIX2 OUTER BOUNDARY
CARD IMAGE MIN.005.002.S ,3,2,4,15,0,1000,152,4,6,4+5/
CARD IMAGE MIN.006.001.S C SHIELD FOUR, MIX3 OUTER BOUNDARY
CARD IMAGE MIN.006.002.S ,4,2,5,15,0,1000,167,2,8,2+5/
CARD IMAGE MIN.007.001.S C SHIELD FIVE, BORATED WATER OUTER BOUNDARY
CARD IMAGE MIN.007.002.S ,5,2,0,117,0,1000,182,1,1+5/
*****
CARD IMAGE ***.000.001.H C DEP OSITION IN REGIONS IS NOT REQUESTED(POINT DETECTOR ONLY)
CARD IMAGE ***.000.002.H C LEA KAGE OF ENERGY IS NOT REQUESTED(POINT DETECTOR ONLY)
CARD IMAGE ***.000.003.H C CHA NNEL DETECTORS ARE NOT DEFINED
CARD IMAGE ***.000.004.H C NOI SE FUNCTIONS ONLY APPLY TO CHA NNEL DETECTORS
CARD IMAGE ***.000.005.H C PLO T OUTPUT IS NOT REQUESTED(CALCOMP)
*****1234567890123456789012345678901234567890123456789012345678901234567890
CARD IMAGE QUI.000.001.H QUICK PLOT
CARD IMAGE QUI.001.001.I C IN1 = 1, INTERPRET LIMIT
CARD IMAGE QUI.001.002.I C IN2 = 1, REQUESTS ARE BEING INPUT
CARD IMAGE QUI.001.003.I C NQUICK = 8, EIGHT QUICK PLOTS
,C 1,1,8/
CARD IMAGE QUI.001.004.I C N(E) VERSUS E
CARD IMAGE QUI.002.001.II C INTEGRAL OF N(E) VERSUS E
CARD IMAGE QUI.002.002.II C TOTAL ENERGY FLUX VS SOURCE REGION
CARD IMAGE QUI.002.003.II C TOTAL ENERGY FLUX VS SCATTERING REGION
CARD IMAGE QUI.002.004.II C TOTAL ENERGY FLUX VS ORDER OF SCATTER
CARD IMAGE QUI.002.005.II C DOSE VS SHIELD OPTIMIZATION ITERATION
CARD IMAGE QUI.002.006.II C WEIGHT VS SHIELD OPTIMIZATION ITERATION
CARD IMAGE QUI.002.007.II C SHIELD THICKNESSES VERSUS SHIELD OPTIMIZATION ITERATION
CARD IMAGE QUI.002.008.II ,10,0,10,2,21,0,22,0,23,0,30,0,30,1,30,2/
CARD IMAGE QUI.002.009.II
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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE OPT.000.001.H OPTIMUM  
CARD IMAGE OPT.001.001.I C IN1 = 1, INTERPRET LIMIT-OPTION  
CARD IMAGE OPT.001.002.I C IN2 = 0, THIS SECTION HAS NO OTHER INPUT  
CARD IMAGE OPT.001.003.I C NOBIAS = 1, THE PROGRAM WILL CALCULATE OPTIMUM BIASING PARAMETERS  
CARD IMAGE OPT.001.004.I 1 0 1  
\*\*\*\*\*  
CARD IMAGE \*\*\*.000.001.H C BIASING OPTIONS ARE USED AS BUILT IN  
CARD IMAGE \*\*\*.000.002.H C PSEUDO SPHERICAL SOURCE IS USED AS BUILT IN  
CARD IMAGE \*\*\*.000.003.H C RELATIVE SOURCE IMPORTANCE IS USED AS BUILT IN  
CARD IMAGE \*\*\*.000.004.H C RATIOS OF SOURCE VARIABLE IMPORTANCE ARE USED AS BUILT IN(NOT USED)  
CARD IMAGE \*\*\*.000.005.H C PREFERRED POINT DATA IS USED AS INPUT  
CARD IMAGE \*\*\*.000.006.H C SPATIAL IMPORTANCE IS USED AS BUILT IN  
\*\*\*\*\*1234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE CAP.000.001.H CAPTURE  
CARD IMAGE CAP.001.001.I C IN1 = 0, NOT USED  
CARD IMAGE CAP.001.002.I C IN2 = 1, CAPTURE RATIOS ARE BEING INPUT  
CARD IMAGE CAP.001.003.I 0 1  
CARD IMAGE CAP.002.001.E C PROBABILITY OF GOING TO A ANALOG SLOWING DOWN CALCULATION = 1/4 PER COLLISION  
CARD IMAGE CAP.002.002.E ,10\*0.25/  
\*\*\*\*\*  
CARD IMAGE \*\*\*.000.001.H C SHORT CIRCUIT IS NOT REQUIRED FOR UNIT SHIELD PROBLEMS  
CARD IMAGE \*\*\*.000.002.H C ROTATE AND TRANSLATE OPTION IS NOT REQUIRED  
CARD IMAGE \*\*\*.000.003.H C ARRAY DIRECT INPUT IS NOT USED  
CARD IMAGE \*\*\*.000.004.H C DUMPS ARE NOT REQUESTED  
CARD IMAGE \*\*\*.000.005.H C PRINT SUPPRESSION COULD HAVE BEEN USED FOR THE MULTIGROUP CROSS SECTIONS  
CARD IMAGE \*\*\*.000.006.H C NEXT CASE INPUT HERE WOULD INCREMENT THE CASE NUMBER ONLY  
\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE EXE.000.001.H EXECUTE  
CARD IMAGE EXE.001.001.I C IN1 = 1, INTERPRET LIMITS  
CARD IMAGE EXE.001.002.I C IN2 = 0, NOT USED  
CARD IMAGE EXE.001.003.I C NPOINT = 1, RUN POINT DETECTORS INDIVIDUALLY  
CARD IMAGE EXE.001.004.I C NPRINT = 1, ONE PRINTOUT(FINAL) ONLY  
CARD IMAGE EXE.001.005.I C NUNITS = 16, GENERATE 16 HISTORIES  
CARD IMAGE EXE.001.006.I C KALIDE = 15, A MAXIMUM OF FIFTEEN COLLISIONS PER HISTORY  
CARD IMAGE EXE.001.007.I 1 0 1 1 16 15

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\*\*\*\*\*THIS CASE USES 10316 LOCATIONS FOR INPUT, 15276 LOCATIONS TO RUN\*\*\*\*\*  
G0\*G0

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DETECTOR...	1	0	0	1.0000+00	0.0000	0.0000	1.0000+00	0.0000	0.0000	9.1414+02
*****FLUXES FOR DETECTOR 1 AFTER 16 PACKETS*****										
CALCULATED AVERAGE NUMBER FLUX ENERGY FLUX NUMBER FLUX ENERGY FLUX NUMBER FLUX ENERGY FLUX										
	PRECISION	ENERGY-MEV	DERIVATIVE	DERIVATIVE	THIS GROUP	THIS GROUP	CUMULATIVE	CUMULATIVE		
GROUP 1...	3.2634-01	1.3222+01	6.2303-03	8.2374-02	1.6884-02	2.2323-01	1.6884-02	2.2323-01		
GROUP 2...	3.3976-01	1.0869+01	2.1231-02	2.3076-01	4.6920-02	5.0998-01	6.3804-02	7.3321-01		
GROUP 3...	3.6396-01	8.9050+00	2.7423-02	2.4420-01	4.9636-02	4.4201-01	1.1344-01	1.1752+00		
GROUP 4...	3.8336-01	6.8775+00	8.0240-03	5.5212-02	1.7019-02	1.1705-01	1.3046-01	1.2923+00		
GROUP 5...	5.9562-01	5.4121+00	3.3140-04	1.7936-03	3.6454-04	1.9730-03	1.3082-01	1.2942+00		
GROUP 6...	6.1128-01	4.4266+00	1.7982-05	7.9601-05	1.6184-05	7.1641-05	1.3084-01	1.2943+00		
GROUP 7...	8.5210-01	3.4703+00	5.3348-08	1.8513-07	5.6549-08	1.9624-07	1.3084-01	1.2943+00		
GROUP 8...	6.9655-01	2.7139+00	4.0605-07	1.1020-06	2.1927-07	5.9508-07	1.3084-01	1.2943+00		
GROUP 9...	6.2985-01	2.3786+00	1.4125-07	3.3597-07	3.3900-08	8.0633-08	1.3084-01	1.2943+00		
GROUP 10...	8.7180-01	2.0338+00	3.7038-09	7.5330-09	1.4815-09	3.0132-09	1.3084-01	1.2943+00		
GROUP 11...	9.3474-01	1.5175+00	6.3812-11	9.6833-11	3.0630-11	4.6480-11	1.3084-01	1.2943+00		
GROUP 12...	9.6678-01	1.2371+00	7.1528-13	8.8491-13	1.7167-13	2.1238-13	1.3084-01	1.2943+00		
GROUP 13...	9.6815-01	1.0062+00	1.1080-15	1.1148-15	2.2160-16	2.2297-16	1.3084-01	1.2943+00		
GROUP 14...	9.6821-01	6.5513-01	1.8001-13	1.1793-13	6.4805-14	4.2456-14	1.3084-01	1.2943+00		
GROUP 15...	9.6825-01	5.0924-01	7.3367-19	3.7362-19	1.0271-19	5.2306-20	1.3084-01	1.2943+00		
GROUP 16...	0.0000	2.7726-01	6.8930-23	1.9112-23	2.0679-23	5.7335-24	1.3084-01	1.2943+00		
GROUP 17...	0.0000	6.2500-02	7.8259-35	4.8912-36	7.4346-36	4.6466-37	1.3084-01	1.2943+00		
GROUP 18...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 19...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 20...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 21...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 22...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 23...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 24...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 25...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
GROUP 26...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.3084-01	1.2943+00		
*****NUMBER FLUX RESPONSES FOR DETECTOR 1 AFTER 16 PACKETS*****										
	NUMBER FLUX ENERGY FLUX MEV/CC-H <sub>2</sub> O	RADS/HOUR	REM/HR(TMJ)	REM/HR(GHA)						
GROUP 1...	1.6884-02	2.2323-01	1.4667-07	3.4612-07	1.9417-05	2.5495-06				
GROUP 2...	4.6920-02	5.0998-01	3.7696-07	9.6186-07	5.3958-06	7.0849-06				
GROUP 3...	4.9636-02	4.4201-01	3.9027-07	9.5448-07	5.6180-06	7.4049-06				
GROUP 4...	1.7019-02	1.1705-01	1.2735-07	3.0473-07	1.8535-06	2.4767-06				
GROUP 5...	3.6454-04	1.9730-03	2.5898-09	6.1979-09	3.9442-08	5.0968-08				

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GROUP	6...	1.6184-05	7.1641-05	1.1232-10	2.5400-10	1.7738-09	2.1488-09
GROUP	7...	5.6549-08	1.9624-07	3.5775-13	8.0910-13	5.7405-12	7.2234-12
GROUP	8...	2.1927-07	5.9508-07	1.2084-12	2.7395-12	2.0831-11	2.7388-11
GROUP	9...	3.3900-08	8.0633-08	1.7634-13	3.8597-13	3.2205-12	4.1777-12
GROUP	10...	1.4815-09	3.0132-09	7.5223-15	1.6303-14	1.3929-13	1.8365-13
GROUP	11...	3.0630-11	4.6480-11	1.3809-16	3.0288-16	2.8087-15	3.8992-15
GROUP	12...	1.7167-13	2.1238-13	7.1995-19	1.5249-18	1.5541-17	2.2216-17
GROUP	13...	2.2160-16	2.2297-16	8.7623-22	1.7127-21	1.8794-20	2.8339-20
GROUP	14...	6.4805-14	4.2456-14	1.9958-19	4.3448-19	4.2668-18	6.2654-18
GROUP	15...	1.0271-19	5.2306-20	2.8473-25	6.3475-25	5.9834-24	8.2522-24
GROUP	16...	2.0679-23	5.7335-24	4.2060-29	7.7813-29	1.1167-27	1.0883-27
GROUP	17...	7.4346-36	4.6466-37	0.0000	0.0000	0.0000	0.0000
GROUP	18...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	19...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	20...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	21...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	22...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	23...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	24...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	25...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	26...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
TOTALS.....		1.3084-01	1.2943+00	1.0439-06	2.5736-06	1.4850-05	1.9569-05
MIN ERROR...		1.9538-01	1.9427-01	1.9456-01	1.9579-01	1.9573-01	1.9561-01
MOD ERROR...		3.5096-01	3.4955-01	3.5052-01	3.5077-01	3.5084-01	3.5087-01
MAX ERROR...		3.5363-01	3.5006-01	3.5290-01	3.5274-01	3.5331-01	3.5338-01
*****SUGGESTED CHANGES IN THE IMPORTANCE SAMPLING PARAMETERS*****							
SPA	1...	8.1903-01	7.7411-01	8.1219-01	8.0737-01	8.1575-01	8.1650-01
SPA	2...	9.9491-01	9.9656-01	9.9488-01	9.9552-01	9.9501-01	9.9499-01
SPA	3...	8.5151-01	8.0997-01	8.4540-01	8.4099-01	8.4873-01	8.4933-01
SPA	4...	1.1818+00	1.2405+00	1.1910+00	1.1959+00	1.1859+00	1.1849+00
SPA	5...	9.8516-01	9.8318-01	9.8487-01	9.8457-01	9.8501-01	9.8504-01
SPA	6...	9.9363-01	9.9278-01	9.9350-01	9.9338-01	9.9356-01	9.9358-01
SPA	7...	9.9301-01	9.9201-01	9.9285-01	9.9271-01	9.9292-01	9.9294-01
SPA	8...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00
PRE	1...	1.2731+00	1.1597+00	1.2602+00	1.2497+00	1.2668+00	1.2684+00
PRE	2...	-3.4725-01	-4.0135-01	-3.5870-01	-3.6613-01	-3.5280-01	-3.5162-01
PRE	3...	1.4730+00	1.5309+00	1.4841+00	1.4885+00	1.4778+00	1.4766+00

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	PRE	4...	1.6542+00	1.6972+00	1.6627+00	1.6698+00	1.6591+00	1.6578+00		
	PSE	1...	1.0000+01	1.0000+01	1.0000+01	1.0000+01	1.0000+01	1.0000+01		
	PSE	2...	1.0107-01	4.7256-02	9.1232-02	8.2640-02	9.5897-02	9.7002-02		
	PSE	3...	1.0692+00	1.1996+00	1.0902+00	1.0996+00	1.0782+00	1.0761+00		
	REL	1...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	REL	2...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
	RAT	11...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
	RAT	12...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	13...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	14...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	15...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	21...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	22...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	23...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	24...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
	RAT	25...	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00	1.0000+00		
			*****NUMBER FLUX	MOMENTS FOR DETECTOR	1	AFTER	16	PACKETS*****		
			ITERANT	SOURCE 1	SOURCE 2	SOURCE 3	SOURCE 4	SOURCE 5	SOURCE 6	SOURCE 7
	GROUP	1...	6.2303-03	6.2303-03	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	2...	2.1231-02	2.1231-02	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	3...	2.7423-02	2.7423-02	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	4...	8.0280-03	8.0280-03	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	5...	3.3140-04	3.3140-04	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	6...	1.7982-05	1.7982-05	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	7...	5.3348-08	5.3348-08	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	8...	4.0605-07	4.0605-07	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	9...	1.4125-07	1.4125-07	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	10...	3.7038-09	3.7038-09	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	11...	6.3812-11	6.3812-11	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	12...	7.1528-13	7.1528-13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	13...	1.1080-15	1.1080-15	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	14...	1.8001-13	1.8001-13	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	15...	7.3367-19	7.3367-19	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	16...	6.8930-23	6.8930-23	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	17...	7.8259-35	7.8259-35	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	18...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	GROUP	19...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

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GROUP	20...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	21...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	22...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	23...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	24...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	25...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	26...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
NUMBER FLUX	1.3084-01	1.3084-01	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
ENERGY FLUX	1.2943+00	1.2943+00	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
MEV/CC-H2O	1.0439-06	1.0439-06	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
RADS/HOUR	2.5736-06	2.5736-06	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
REM/HR(TMJ)	1.4850-05	1.4850-05	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
REM/HR(GHA)	1.9569-05	1.9569-05	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
*****NUMBER FLUX MOMENTS FOR DETECTOR 1 AFTER 16 PACKETS*****									
	REGION 1	REGION 2	REGION 3	REGION 4	REGION 5	REGION 6	REGION 7	SCATTER 0	
GROUP	1...	2.7251-04	0.0000	8.6033-05	1.8109-03	3.4202-07	9.6627-09	9.4686-09	4.0605-03
GROUP	2...	1.0474-03	7.8132-06	2.3413-04	7.4497-03	4.5381-06	1.4583-07	2.2149-07	1.2487-02
GROUP	3...	1.3721-03	1.7357-05	2.3540-04	1.1048-02	1.3984-05	2.1343-06	9.6279-07	1.4733-02
GROUP	4...	3.6424-04	7.9133-06	4.0850-05	4.3953-03	2.8632-05	3.8467-06	3.8789-06	3.1833-03
GROUP	5...	1.0577-05	4.2962-07	8.0463-07	2.2568-04	2.0210-06	1.7287-07	5.2541-06	8.6459-05
GROUP	6...	3.0794-07	2.2786-08	1.5247-08	1.1492-05	6.5371-07	3.5551-07	2.8626-06	2.2725-06
GROUP	7...	2.4630-11	2.3958-12	5.0763-13	2.0786-09	9.9169-10	1.0190-09	4.9042-08	1.8956-10
GROUP	8...	1.1399-09	2.4493-10	2.2146-11	7.8034-08	1.9510-08	2.3946-08	2.7698-07	6.1822-09
GROUP	9...	1.1458-09	3.2508-10	1.9910-11	2.7950-08	1.8122-08	8.2501-10	8.7603-08	5.2579-09
GROUP	10...	6.3960-14	2.4410-14	6.8414-16	1.2033-11	1.1162-11	3.1508-12	3.6770-09	3.7907-13
GROUP	11...	3.3119-18	1.6109-18	1.9631-20	3.3964-15	1.2699-14	2.4211-14	6.3771-11	2.1449-17
GROUP	12...	4.0591-24	3.3527-24	1.1019-26	2.4246-20	3.3940-19	4.9929-18	7.1528-13	3.2446-23
GROUP	13...	0.0000	0.0000	0.0000	4.4459-26	1.3920-24	3.7504-25	1.1080-15	0.0000
GROUP	14...	0.0000	0.0000	0.0000	2.5287-23	3.8541-22	4.4710-22	1.8001-13	0.0000
GROUP	15...	0.0000	0.0000	0.0000	0.0000	1.0397-34	7.2215-33	7.3367-19	0.0000
GROUP	16...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	6.8930-23	0.0000
GROUP	17...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	7.8259-35	0.0000
GROUP	18...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	19...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	20...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	21...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP	22...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 1  
 T.M.JORDAN-A.R.T.RESEARCH\*\*\*\*\*PRIMARY NEUTRONS\*\*\*\*\*PAGE 76

GROUP 23...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP 24...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP 25...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
GROUP 26...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
NUMBER FLUX	6.3209-03	6.5953-05	1.2641-03	5.0946-02	9.9795-05	1.2891-05	1.9061-05	7.2112-02	
ENERGY FLUX	6.2414-02	5.8547-04	1.3101-02	4.8738-01	7.7880-04	9.6819-05	1.2106-04	7.2983-01	
MEV/CC-H2O	5.0402-08	5.1478-10	1.0187-08	4.0370-07	7.6182-10	9.7864-11	1.3960-10	5.7815-07	
RADS/HOUR	1.2438-07	1.2668-09	2.5146-08	9.9388-07	1.8454-09	2.3587-10	3.3287-10	1.4266-06	
REM/HR(TMJ)	7.1761-07	7.4220-09	1.4407-07	5.7639-06	1.1042-08	1.4224-09	2.0813-09	8.2027-06	
REM/HR(GHA)	9.4558-07	9.8044-09	1.8963-07	7.6025-06	1.4655-08	1.8865-09	2.7127-09	1.0802-05	
*****NUMBER FLUX	SCATTER 1	SCATTER 2	SCATTER 3	SCATTER 4	1 AFTER	16 PACKETS	*****	*****	*****
SCATTER 5	SCATTER 6	SCATTER 7							
GROUP 1...	1.6858-03	4.3508-04	3.2970-05	1.5183-05	7.1050-07	7.7727-08	1.0755-08		
GROUP 2...	5.3401-03	3.1956-03	1.3273-04	6.8073-05	6.4975-06	7.9635-07	1.9122-07		
GROUP 3...	6.5782-03	5.7482-03	2.3434-04	1.0807-04	1.7135-05	3.3964-06	4.2969-07		
GROUP 4...	1.7827-03	2.8094-03	1.2713-04	8.5465-05	3.0184-05	5.8620-06	2.8442-06		
GROUP 5...	7.4834-05	1.3653-04	1.2485-05	1.2880-05	2.3162-05	6.3381-07	1.2285-06		
GROUP 6...	3.8472-06	5.2341-06	1.2427-06	1.4556-06	6.3858-07	4.2800-07	2.8387-07		
GROUP 7...	3.3574-10	6.9749-10	3.9718-10	6.3206-10	9.3405-10	1.1161-09	6.9187-09		
GROUP 8...	1.3582-08	2.0619-08	2.5645-08	1.6367-08	1.8980-08	2.7489-08	6.3244-08		
GROUP 9...	3.9944-09	6.9812-09	4.8951-09	1.1657-08	1.8114-08	2.6978-09	6.7450-08		
GROUP 10...	1.0553-12	2.8627-12	3.8561-12	3.4676-12	9.2653-12	5.7142-12	4.3827-10		
GROUP 11...	9.2907-17	1.5959-16	5.5786-16	1.6126-15	9.4541-15	2.8242-14	3.6645-13		
GROUP 12...	3.4555-22	8.8750-22	6.7070-21	1.3370-20	2.9514-19	5.0346-18	2.6127-15		
GROUP 13...	0.0000	1.2875-29	6.7362-28	1.3882-26	3.3865-25	1.4455-24	1.2740-20		
GROUP 14...	4.9771-27	3.2426-26	3.6383-25	2.0606-23	1.0856-22	7.1647-22	2.5391-19		
GROUP 15...	0.0000	0.0000	0.0000	0.0000	1.0397-34	7.2215-33	2.1560-28		
GROUP 16...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	5.5705-34		
GROUP 17...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 18...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 19...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 20...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 21...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 22...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 23...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 24...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 25...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 1  
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GROUP 26...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
NUMBER FLUX	3.2142-02	2.4756-02	1.0912-03	5.8387-04	1.1443-04	2.1645-05	8.9239-06
ENERGY FLUX	3.2116-01	2.2679-01	1.0080-02	5.2496-03	9.1418-04	1.6765-04	6.1975-05
MEV/CC-H2O	2.5701-07	1.9445-07	8.5899-09	4.5696-09	8.7695-10	1.6502-10	6.6576-11
RADS/HOUR	6.3367-07	4.7828-07	2.1078-08	1.1195-08	2.1285-09	3.9923-10	1.5988-10
REM/HR(TMJ)	3.6511-06	2.7907-06	1.2298-07	6.5581-08	1.2692-08	2.3951-09	9.7640-10
REM/HR(GHA)	4.8101-06	3.6849-06	1.6235-07	8.6634-08	1.6833-08	3.1739-09	1.2918-09
*****SHIELD DERIVATIVES FOR DETECTOR 1 AFTER 16 PACKETS*****							
	SEGMENT 1	NORMAL 1	NORMAL 2	NORMAL 3	NORMAL 4	NORMAL 5	
GROUP 1...	6.2303-03	-1.2893-03	-7.8975-04	-7.0241-04	-6.1760-04	-5.2594-04	
GROUP 2...	2.1231-02	-4.2595-03	-2.7443-03	-2.4610-03	-2.1847-03	-1.8829-03	
GROUP 3...	2.7423-02	-5.3984-03	-3.6892-03	-3.3405-03	-2.9988-03	-2.6211-03	
GROUP 4...	8.0280-03	-1.6346-03	-1.1994-03	-1.0973-03	-9.9551-04	-8.7986-04	
GROUP 5...	3.3140-04	-5.9628-05	-5.5692-05	-5.2050-05	-4.8080-05	-4.3753-05	
GROUP 6...	1.7982-05	-3.5164-06	-3.0478-06	-2.9892-06	-2.8239-06	-2.7669-06	
GROUP 7...	5.3348-08	-8.4427-09	-5.9606-09	-8.1082-09	-7.1277-09	-1.1083-08	
GROUP 8...	4.0605-07	-8.4895-08	-5.5612-08	-6.7151-08	-6.3885-08	-7.6905-08	
GROUP 9...	1.4125-07	-4.4026-08	-1.8572-08	-1.9410-08	-1.9374-08	-2.7048-08	
GROUP 10...	3.7038-09	-5.7996-10	-4.4820-10	-6.4632-10	-5.7479-10	-9.1843-10	
GROUP 11...	6.3812-11	-8.7433-12	-6.9679-12	-1.0111-11	-8.6051-12	-1.9494-11	
GROUP 12...	7.1528-13	-9.0590-14	-7.1592-14	-1.0313-13	-8.5027-14	-2.7059-13	
GROUP 13...	1.1080-15	-1.3967-16	-1.1111-16	-1.5970-16	-1.3148-16	-5.3349-16	
GROUP 14...	1.8001-13	-2.2686-14	-1.8081-14	-2.5971-14	-2.1377-14	-7.8055-14	
GROUP 15...	7.3367-19	-9.2736-20	-7.6301-20	-1.1010-19	-9.0982-20	-4.6714-19	
GROUP 16...	6.8930-23	-8.9423-24	-8.7097-24	-1.3099-23	-1.1126-23	-5.2757-23	
GROUP 17...	7.8259-35	-1.0186-35	-9.9598-36	-1.5074-35	-1.2835-35	-9.0919-35	
GROUP 18...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 19...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 20...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 21...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 22...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 23...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 24...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 25...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
GROUP 26...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
NUMBER FLUX	1.3084-01	-2.6213-02	-1.7489-02	-1.5775-02	-1.4096-02	-1.2247-02	
ENERGY FLUX	1.2943+00	-2.5972-01	-1.7151-01	-1.5445-01	-1.3775-01	-1.1942-01	

THE FASTER-III PROGRAM \*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*CASE 1  
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MEV/CC-H20 1.0439-06 -2.0922-07 -1.3930-07 -1.2560-07 -1.1219-07 -9.7433-08  
RADS/HOUR 2.5736-06 -5.1571-07 -3.4322-07 -3.0945-07 -2.7639-07 -2.4001-07  
REM/HR(TMJ) 1.4850-05 -2.9751-06 -1.9832-06 -1.7885-06 -1.5979-06 -1.3881-06  
REM/HR(GHA) 1.9569-05 -3.9206-06 -2.6141-06 -2.3576-06 -2.1064-06 -1.8299-06

\*\*\*\*\*SHIELD DERIVATIVES FOR DETECTOR 1 AFTER 16 PACKETS\*\*\*\*\*  
SEGMENT 2

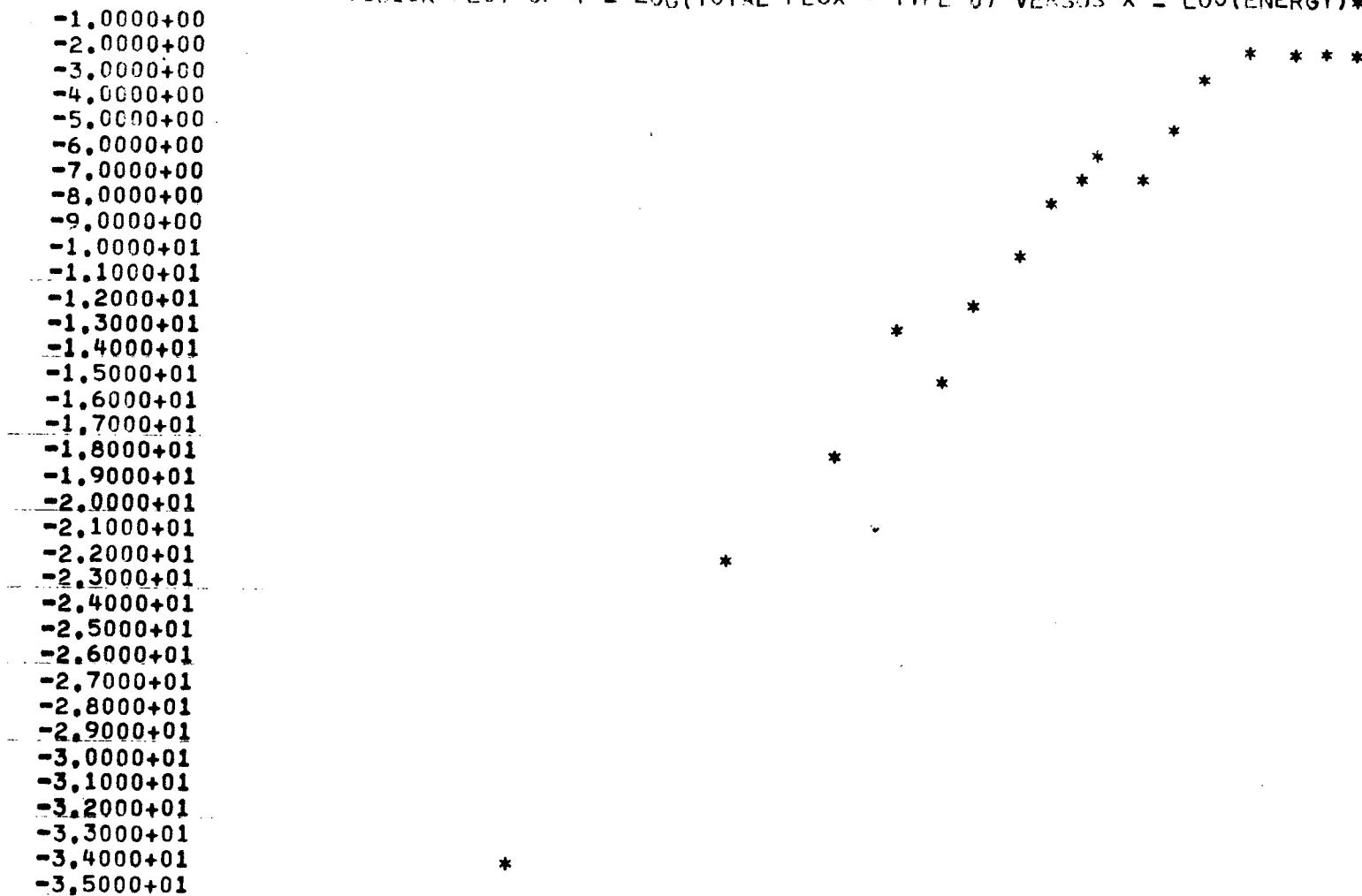
GROUP 1... 0.0000  
GROUP 2... 0.0000  
GROUP 3... 0.0000  
GROUP 4... 0.0000  
GROUP 5... 0.0000  
GROUP 6... 0.0000  
GROUP 7... 0.0000  
GROUP 8... 0.0000  
GROUP 9... 0.0000  
GROUP 10... 0.0000  
GROUP 11... 0.0000  
GROUP 12... 0.0000  
GROUP 13... 0.0000  
GROUP 14... 0.0000  
GROUP 15... 0.0000  
GROUP 16... 0.0000  
GROUP 17... 0.0000  
GROUP 18... 0.0000  
GROUP 19... 0.0000  
GROUP 20... 0.0000  
GROUP 21... 0.0000  
GROUP 22... 0.0000  
GROUP 23... 0.0000  
GROUP 24... 0.0000  
GROUP 25... 0.0000  
GROUP 26... 0.0000  
NUMBER FLUX 0.0000  
ENERGY FLUX 0.0000  
MEV/CC-H20 0.0000  
RADS/HOUR 0.0000  
REM/HR(TMJ) 0.0000

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 1  
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REM/HR(GHA) 0.0000

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\*\*\*\*\*QUICK PLOT OF Y = LOG(TOTAL FLUX - TYPE 0) VERSUS X = LOG(ENERGY)\*\*\*\*\*



X= -2.0000+00

2.0000+00=X

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 1  
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\*\*\*\*\*QUICK PLOT OF Y = LOG(TOTAL FLUX - TYPE 2) VERSUS X = LOG(ENERGY)\*\*\*\*\*

-1.0000+00  
-1.0588+00  
-1.1176+00  
-1.1765+00  
-1.2353+00  
-1.2941+00  
-1.3529+00  
-1.4118+00  
-1.4706+00  
-1.5294+00  
-1.5882+00  
-1.6471+00  
-1.7059+00  
-1.7647+00  
-1.8235+00  
-1.8824+00  
-1.9412+00  
-2.0000+00  
-2.0588+00  
-2.1176+00  
-2.1765+00  
-2.2353+00  
-2.2941+00  
-2.3529+00  
-2.4118+00  
-2.4706+00  
-2.5294+00  
-2.5882+00  
-2.6471+00  
-2.7059+00  
-2.7647+00  
-2.8235+00  
-2.8824+00  
-2.9412+00  
-3.0000+00

$$X = -7,000 + 00$$

$$2.0000+00=x$$

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\*\*\*\*\*QUICK PLOT OF Y = LOG( SOURCE ENERGY FLUX) VERSUS X = COMPONENT INDEX\*\*\*\*\*  
\*\*\*\*\*THE RANGE OF X AND/OR Y IS ZERO\*\*\*\*\*

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 1  
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\*\*\*\*\*QUICK PLOT OF Y = LOG( REGION ENERGY FLUX) VERSUS X = COMPONENT INDEX\*\*\*\*\*

0.0000  
-1.4706+01  
-2.9412+01  
-4.4118+01  
-5.8824+01  
-7.3529+01  
-8.8235+01  
-1.0294+00  
-1.1765+00 \*  
-1.3235+00  
-1.4706+00  
-1.6176+00  
-1.7647+00  
-1.9118+00  
-2.0588+00  
-2.2059+00  
-2.3529+00  
-2.5000+00  
-2.6471+00  
-2.7941+00  
-2.9412+00  
-3.0882+00  
-3.2353+00 \*  
-3.3824+00  
-3.5294+00  
-3.6765+00  
-3.8235+00  
-3.9706+00  
-4.1176+00  
-4.2647+00  
-4.4118+00  
-4.5588+00  
-4.7059+00  
-4.8529+00  
-5.0000+00

X= 1.0000+00

7.0000+00=X

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\*\*\*\*\*QUICK PLOT OF Y = LOG( SCATTER ENERGY FLUX) VERSUS X = COMPONENT INDEX\*\*\*\*\*

0.0000  
-1.4706-01 \*  
-2.9412-01  
-4.4118-01 \*  
-5.8624-01 \*  
-7.3529-01  
-8.8235-01  
-1.0294+00  
-1.1765+00  
-1.3235+00  
-1.4706+00  
-1.6176+00  
-1.7647+00  
-1.9118+00  
-2.0588+00  
-2.2059+00  
-2.3529+00 \*  
-2.5000+00  
-2.6471+00  
-2.7941+00  
-2.9412+00  
-3.0882+00  
-3.2353+00  
-3.3824+00  
-3.5294+00  
-3.6765+00  
-3.8235+00  
-3.9706+00  
-4.1176+00  
-4.2647+00  
-4.4118+00  
-4.5588+00  
-4.7059+00  
-4.8529+00  
-5.0000+00

X= 0.0000

7.0000+00=X

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 1  
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\*\*\*\*\*BOUNDARY SEARCH PARAMETERS, (SURFACE,MOST PROBABLE NEXT REGION)\*\*\*\*\*

REGION	1(	1,	2)		
REGION	2(	-1,	1)(	2,	3)
REGION	3(	-2,	2)(	3,	4)
REGION	4(	-3,	3)(	4,	5)
REGION	5(	-4,	4)(	5,	6)
REGION	6(	-5,	5)(	6,	7)
REGION	7(	-6,	6)(	7,	8)
REGION	8(	-7,	7)(	8,	-11)

THE FASTER-III PROGRAM \*\*\*\* SHIELD TEST PROFILE \*\*\*\* CASE 2  
T.M.JORDAN-A.R.T.RESEARCH \*\*\*\* PRIMARY NEUTRONS \*\*\*\* PAGE 1  
\*\*\*\*\*12345678901234567890123456789012345678901234567890  
CARD IMAGE TAP.000.001.H TAPES  
CARD IMAGE TAP.001.001.I C DEFINE SOURCE TAPE CONTAINING FLUXES FOR SECONDARY SOURCES  
CARD IMAGE TAP.001.002.I 1 0 1 0 2 9 0 0

THE FASTER-ITI PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 2  
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\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE LAB.000.001,H LABEL  
CARD IMAGE LAB.001.001,I 0 1  
CARD IMAGE LAB.002.001,A \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*  
CARD IMAGE LAB.002.002,A \*\*\*\*\*SECONDARY PHOTONS\*\*\*\*\*  
\*\*\*\*\*12345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE PHO.000.001,H PHOTON CROSS SECTIONS  
CARD IMAGE PHO.001.001,I 1 1 15 0 0  
CARD IMAGE PHO.002.001,E C ENERGY GROUPS  
CARD IMAGE PHO.002.002,E ,8,5,5,5,4,5,4,3,5,3,2,6,2,2,1,8,1,35,,9,,4,0,26,,15,,08/  
CARD IMAGE PHO.003.001,I C HYDROGEN  
CARD IMAGE PHO.003.002,I 0 0 14 0 0 0 14 14  
CARD IMAGE PHO.004.001,E C TAB ENERGIES  
CARD IMAGE PHO.004.002,E ,10,8,6,5,4,3,2,1,5,1,,6,,4,0,2,,15,,08/  
CARD IMAGE PHO.005.001,E C PAIR PRODUCTION  
CARD IMAGE PHO.005.002,E ,2.7-3,2.2-3,1.5-3,1,2-3,8,7-4,5,2-4,1.8,4,4,4-5/  
CARD IMAGE PHO.006.001,E C PHOTOELECTRIC  
CARD IMAGE PHO.006.002,E ,7\*0,1.8-9,5,2-9,2,1-8,6,6-8,4,5-7,1,0-6,6,0-6/  
CARD IMAGE PHO.007.001,I C BERYLLIUM  
CARD IMAGE PHO.007.002,I 0 0 14 0 0 0 14 14  
CARD IMAGE PHO.008.001,E C TAB ENERGIES  
CARD IMAGE PHO.008.002,E ,10,8,6,5,4,3,2,1,5,1,,6,,4,0,2,,15,,08/  
CARD IMAGE PHO.009.001,E C PAIR PRODUCTION  
CARD IMAGE PHO.009.002,E ,3.7-2,2.82-2,2.28-2,1.84-2,1.32-2,8,2-3,2.8-3,7,-4/  
CARD IMAGE PHO.010.001,E C PHOTOELECTRIC  
CARD IMAGE PHO.010.002,E ,7.2-8,9,3-8,1.3-7,1.6-7,2-7,3,7-7,9-7,1,7-6,4-6,1,6-5,5-5,3,5-4,8,2-4  
CARD IMAGE PHO.010.003,E ,5.2-3/  
CARD IMAGE PHO.011.001,I C BORON  
CARD IMAGE PHO.011.002,I 0 0 14 0 0 0 14 14  
CARD IMAGE PHO.012.001,E C TAB ENERGIES  
CARD IMAGE PHO.012.002,E ,10,8,6,5,4,3,2,1,5,1,,6,,4,0,2,,15,,08/  
CARD IMAGE PHO.013.001,E C PAIR PRODUCTION  
CARD IMAGE PHO.013.002,E ,5,9-2,4,8-2,3,7-2,3,0-2,2,2-2,1,3-2,4,5-2,1,1-3/  
CARD IMAGE PHO.014.001,E C PHOTOELECTRIC  
CARD IMAGE PHO.014.002,E ,2,2-7,2,9-7,4,1-7,5,2-7,7,1-6,2,5-6,4,6-6,1,2-5,5-5,1,6-4,1,1-3,2,4-3

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THE FASTER-ITI PROGRAM \*\*\*\*\* UNIT SHIELD TEST PROFILE \*\*\*\*\* CASE  
T.N.JORDAN-A.V.T.RESEARCHER \*\*\*\*\* SECONDARY PHOTOCOPY \*\*\*\*\* PAGE

THE FASTER-III PROGRAM \* \*\*\*\* \* UNIT SHIELD TEST PROBLEM \*\*\*\* \* CASE  
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\*\*\*\*\* THIS CASE USES 10972 LOCATIONS FOR INPUT, 15228 LOCATIONS TO RUN \*\*\*\*\*

THE FASTER-III ECOLOGY, \*\*\*\*\*UNIT SHIELD TEST PROFILE\*\*\*\*\*CASE 2  
 T.M.JORDAN-A.L.T.RESEARCH\*\*\*\*\*SECONDARY PHOTO \*\*\*\*\*PAGE 4

DETECTOR... 1 2 3 4 1.0000+00 0.0000 0.0000 1.0000+00 0.0000 0.0000 9.1414+02

\*\*\*\*\*FLUXES FOR DETECTOR: 1 AFTER 16 PACKETS\*\*\*\*\*

	CALCULATOR PRECISION	AVERAGE ENERGY-FLUX	CUMULATIVE ENERGY-FLUX	NUMBER FLUX	ENERGY FLUX	NUMBER FLUX	ENERGY FLUX	NUMBER FLUX	ENERGY FLUX
GROUP 1...	7.9446-01	6.7496+00	1.9223-01	1.2975+00	4.8059-01	3.2439+00	4.8059-01	3.2439+00	
GROUP 2...	8.4969-01	5.2500+00	9.7274-01	5.1069+00	4.8637-01	2.5534+00	9.6696-01	5.7973+00	
GROUP 3...	7.4457-01	4.7300+00	1.0280+00	8.8426+00	9.3296-01	4.4213+00	1.8999+00	1.0219+01	
GROUP 4...	8.8214-01	4.2510+00	2.1521+00	9.1718+00	1.0790+00	4.5059+00	2.9790+00	1.4804+01	
GROUP 5...	7.7055-01	3.7522+00	2.5190+00	9.4516+00	1.2595+00	4.7258+00	4.2384+00	1.9530+01	
GROUP 6...	7.0412-01	3.2352+00	2.1146+00	6.8413+00	1.0573+00	3.4207+00	5.2958+00	2.2951+01	
GROUP 7...	6.6495-01	2.7904+00	1.7944+00	5.0371+00	7.1775-01	2.0026+00	6.0135+00	2.4954+01	
GROUP 8...	6.1086-01	2.4028+00	4.3957-01	1.0562+00	1.7583-01	4.2248-01	6.1893+00	2.5376+01	
GROUP 9...	9.6811-01	2.1682+00	3.9207-02	8.5010-02	1.5683-02	3.4004-02	6.2050+00	2.5410+01	
GROUP 10...	9.6765-01	1.4232+00	2.8586-02	4.0827-02	1.2864-02	1.8372-02	6.2179+00	2.5429+01	
GROUP 11...	9.4247-01	9.5341-01	3.5139+00	3.3712+00	1.5812+00	1.5171+00	7.7991+00	2.6946+01	
GROUP 12...	5.6773-01	5.3910-01	1.0624-01	5.6317-02	5.3119-02	2.8158-02	7.8522+00	2.6974+01	
GROUP 13...	9.1194-01	3.7667-01	2.4253-03	9.1355-04	3.3954-04	1.2790-04	7.8526+00	2.6974+01	
GROUP 14...	9.5658-01	2.4698-01	3.7353-04	9.0915-05	4.1039-05	9.9016-06	7.8526+00	2.6974+01	
GROUP 15...	6.6802-01	1.0970-01	2.9864-09	3.2761-10	2.0905-10	2.2933-11	7.8526+00	2.6974+01	

\*\*\*\*\*NUMBER FLUX RESPONSES FOR DETECTOR 1 AFTER 16 PACKETS\*\*\*\*\*

	NUMBER FLUX	ENERGY FLUX	RESPONSES FOR DETECTOR
GROUP 1...	4.8059-01	3.2439+00	3.5670-06
GROUP 2...	4.8637-01	2.5534+00	3.0322-06
GROUP 3...	9.3296-01	4.4213+00	5.4177-06
GROUP 4...	1.0790+00	4.5059+00	5.7722-06
GROUP 5...	1.2595+00	4.7258+00	6.1564-06
GROUP 6...	1.0562+00	3.4207+00	4.6582-06
GROUP 7...	7.1775-01	2.0026+00	2.8078-06
GROUP 8...	1.7583-01	4.2248-01	6.1678-07
GROUP 9...	1.5683-02	3.4004-02	5.1772-08
GROUP 10...	1.2864-02	1.8372-02	7.1340-08
GROUP 11...	1.5612+00	1.5171+00	2.7967-06
GROUP 12...	5.3119-02	2.8158-02	5.3549-08
GROUP 13...	3.3954-04	1.2790-04	2.4652-10
GROUP 14...	4.1039-05	9.9016-06	1.8074-11
GROUP 15...	2.0905-10	2.2933-11	3.6954-17
TOTALS.....	7.8526+00	2.6974+01	3.4958-05

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 2  
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MIN ERROR... 3.0304-01 2.9073-01 2.8705-01  
 MOD ERROR... 7.8845-01 7.7893-01 7.7932-01  
 MAX ERROR... 8.0096-01 7.8670-01 7.8798-01

\*\*\*\*\*SUGGESTED CHANGES IN THE IMPORTANCE SAMPLING PARAMETERS\*\*\*\*\*

SPA	1...	1.0000+00	1.0000+00
SPA	2...	1.0000+00	1.0000+00
SPA	3...	1.0000+00	1.0000+00
SPA	4...	9.9994-01	1.0015+00
SPA	5...	1.0084+00	1.0089+00
SPA	6...	1.0094+00	1.0051+00
SPA	7...	9.8895-01	9.8661-01
SPA	8...	1.0000+00	1.0000+00
PRE	1...	9.1749-01	8.2401-01
PRE	2...	6.7972-01	7.7096-01
PRE	3...	1.0407+00	9.9796-01
PRE	4...	1.0665+00	9.5417-01
PSE	1...	1.0000+01	1.0000+01
PSE	2...	9.9938-01	9.9915-01
PSE	3...	6.9993-01	6.9991-01
REL	1...	1.0000+00	1.0000+00
REL	2...	0.0000	0.0000
RAT	11...	0.0000	0.0000
RAT	12...	1.0000+00	1.0000+00
RAT	13...	1.0000+00	1.0000+00
RAT	14...	1.0000+00	1.0000+00
RAT	15...	1.0000+00	1.0000+00
RAT	21...	1.0000+00	1.0000+00
RAT	22...	1.0000+00	1.0000+00
RAT	23...	1.0000+00	1.0000+00
RAT	24...	1.0000+00	1.0000+00
RAT	25...	1.0000+00	1.0000+00
SPA	1...	9.8254-01	9.7722-01
SPA	2...	1.0170+00	1.0201+00
SPA	3...	9.6371-01	9.5447-01
SPA	4...	9.9731-01	9.9492-01
SPA	5...	9.8903-01	9.8961-01
SPA	6...	9.9135-01	9.8795-01

THE FASTER-III PROGRAM \*\*\*\* UNIT SHIELD TEST PROBLEMS \*\*\*\* CASE 2  
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SPA	7...	9.9657-01	9.9811-01	9.9112-01
SFA	8...	1.0000+00	1.0000+00	1.0000+00
PRE	1...	2.7446-01	2.4158-01	2.9205-01
PRE	2...	8.3339-01	8.7960-01	8.6587-01
PRE	3...	1.0910+00	1.1168+00	1.1110+00
PRE	4...	1.2948+00	1.3250+00	1.3729+00
PSE	1...	1.0000+01	1.0000+01	1.0000+01
PSE	2...	7.6493-01	7.3285-01	7.4379-01
PSE	3...	6.4791-01	6.3762-01	6.4200-01
REL	1...	1.0000+00	1.0000+00	1.0000+00
REL	2...	0.0000	0.0000	0.0000
RAT	11...	0.0000	0.0000	0.0000
RAT	12...	1.0000+00	1.0000+00	1.0000+00
RAT	13...	1.0000+00	1.0000+00	1.0000+00
RAT	14...	1.0000+00	1.0000+00	1.0000+00
RAT	15...	1.0000+00	1.0000+00	1.0000+00
RAT	21...	1.0000+00	1.0000+00	1.0000+00
RAT	22...	1.0000+00	1.0000+00	1.0000+00
RAT	23...	1.0000+00	1.0000+00	1.0000+00
RAT	24...	1.0000+00	1.0000+00	1.0000+00
RAT	25...	1.0000+00	1.0000+00	1.0000+00

***** NUMBER FLUX MOMENTS FOR DETECTOR 1 AFTER 16 PACKETS *****							
	ITERANT	SOURCE 1	SOURCE 2	SOURCE 3	SOURCE 4	SOURCE 5	SOURCE 6
GROUP	1...	1.9223-01	8.1184-05	3.2565-07	1.1310-06	1.1751-01	6.2711-02
GROUP	2...	9.7274-01	3.6148-04	0.0000	1.1767-05	6.7483-01	2.8184-01
GROUP	3...	1.8659+00	5.7912-04	0.0000	1.9437-05	1.3772+00	4.7411-01
GROUP	4...	2.1581+00	7.9833-04	0.0000	2.4389-05	1.4527+00	6.8394-01
GROUP	5...	2.5190+00	9.3426-04	0.0000	2.2813-05	1.7356+00	7.5994-01
GROUP	6...	2.1146+00	7.7363-04	3.0164-07	1.3342-05	1.4470+00	6.3969-01
GROUP	7...	1.7944+00	6.1125-04	3.1644-08	7.5305-06	1.1906+00	5.8598-01
GROUP	8...	4.3957-01	5.7636-05	1.5790-09	5.1539-07	2.6909-01	1.6491-01
GROUP	9...	3.9207-02	1.1388-12	0.0000	9.0720-15	3.9206-02	1.5409-06
GROUP	10...	2.8586-02	6.8303-11	0.0000	1.5384-16	2.8569-02	1.3536-05
GROUP	11...	3.5139+00	4.7407-12	1.5503-18	2.3077-14	3.4328+00	7.9615-02
GROUP	12...	1.0624-01	5.7521-24	0.0000	0.0000	7.9325-02	2.5820-02
GROUP	13...	2.4253-03	0.0000	0.0000	0.0000	2.5274-27	1.0284-03
GROUP	14...	3.7353-04	0.0000	0.0000	0.0000	4.3366-32	3.2959-27
							4.8956-16
							3.7353-04

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 2  
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GROUP	15...	2.9864-09	0.0000	0.0000	0.0000	0.0000	0.0000	3.6117-34	2.9864-09
NUMBER FLUX		7.8526+00	2.1939-03	9.7832-07	5.1920-05	5.8343+00	1.9258+00	7.4468-02	1.5798-02
ENERGY FLUX		2.6974+01	9.1293-03	6.0202-06	2.2114-04	1.8845+01	7.6891+00	3.3905-01	9.1813-02
REM/HR		3.4958-05	1.1476-08	6.7591-12	2.7700-10	2.4689-05	9.7399-06	4.1319-07	1.0389-07
*****NUMBER FLUX MOMENTS FOR DETECTOR 1 AFTER 16 PACKETS*****									
	REGION 1	REGION 2	REGION 3	REGION 4	REGION 5	REGION 6	REGION 7	SCATTER 0	
GROUP 1...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	1.9223-01	
GROUP 2...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	9.7274-01	
GROUP 3...	0.0000	0.0000	0.0000	0.0000	2.9550-01	0.0000	0.0000	1.5704+00	
GROUP 4...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	2.1581+00	
GROUP 5...	0.0000	0.0000	0.0000	3.0989-01	0.0000	0.0000	3.3216-02	2.1759+00	
GROUP 6...	0.0000	0.0000	0.0000	2.9518-01	0.0000	0.0000	1.4756-01	1.6719+00	
GROUP 7...	0.0000	0.0000	0.0000	1.3609-01	0.0000	0.0000	3.3675-01	1.3215+00	
GROUP 8...	0.0000	0.0000	0.0000	1.3312-02	0.0000	2.6018-02	1.1203-01	2.8821-01	
GROUP 9...	0.0000	0.0000	4.0303-15	2.8306-06	0.0000	5.2456-07	3.9202-02	1.7024-06	
GROUP 10...	0.0000	0.0000	2.0831-12	1.8059-09	1.6442-08	1.3016-05	2.8572-02	8.0180-07	
GROUP 11...	0.0000	0.0000	2.5026-12	1.4747-04	1.3911-02	3.3859-01	3.1543+00	6.8933-03	
GROUP 12...	0.0000	0.0000	0.0000	7.9382-10	9.4002-05	5.4343-03	1.0060-01	1.0524-04	
GROUP 13...	0.0000	0.0000	0.0000	9.2782-28	6.4070-11	3.8028-08	2.4253-03	4.3794-09	
GROUP 14...	0.0000	0.0000	0.0000	0.0000	5.1593-30	7.6488-26	3.7353-04	4.7139-10	
GROUP 15...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	2.9060-09	8.0427-11	
NUMBER FLUX	0.0000	0.0000	2.0652-12	5.1012-01	6.3067-03	1.6549-01	1.7686+00	5.4021+00	
ENERGY FLUX	0.0000	0.0000	2.4228-12	1.9238+00	6.0306-03	1.7263-01	2.2256+00	2.2646+01	
REM/HR	0.0000	0.0000	4.2773-18	2.4976-06	1.1095-08	3.0817-07	3.7297-06	2.8411-05	
*****NUMBER FLUX MOMENTS FOR DETECTOR 1 AFTER 16 PACKETS*****									
	SCATTER 1	SCATTER 2	SCATTER 3	SCATTER 4	SCATTER 5	SCATTER 6	SCATTER 7		
GROUP 1...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 2...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 3...	2.9550-01	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 4...	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 5...	3.0989-01	3.3216-02	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 6...	2.9518-01	1.4756-01	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 7...	1.3596-01	3.3689-01	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 8...	1.6073-02	1.3529-01	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 9...	2.9902-06	3.9203-02	0.0000	0.0000	0.0000	0.0000	0.0000		
GROUP 10...	5.9748-06	9.9900-06	2.4805-02	3.7637-03	0.0000	0.0000	0.0000		
GROUP 11...	1.0621-02	1.7405-02	3.5019-01	3.1287+00	0.0000	0.0000	0.0000		

THE FASTER-III PROJECT \*\*\*\*\* UNIT SHIELD TEST PRE-LEN\*\*\*\*\*CASE 2  
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GROUP 12...	7.6051-04	1.1074-02	4.3864-02	5.0703-02	0.0000	0.0000	0.0000
GROUP 13...	1.6093-06	2.5172-05	1.6436-03	7.5465-04	0.0000	0.0000	0.0000
GROUP 14...	2.2691-07	8.7346-16	5.8418-05	3.0630-04	0.0000	0.0000	0.0000
GROUP 15...	1.1283-10	2.4829-16	1.9296-09	1.5353-09	0.0000	0.0000	0.0000
NUMBER FLUX	5.1626-01	3.6832-01	1.9078-01	1.4351+00	0.0000	0.0000	0.0000
ENERGY FLUX	1.9311+00	8.5152-01	1.7878-01	1.3667+00	0.0000	0.0000	0.0000
REM/HR	2.5100-06	1.1944-06	3.2751-07	2.5147-06	0.0000	0.0000	0.0000

\*\*\*\*\*SHIELD DERIVATIVES FOR DETECTOR 1 AFTER 16 PACKETS\*\*\*\*\*  
 SEGMENT 1 NORMAL 1 NORMAL 2 NORMAL 3 NORMAL 4 NORMAL 5

GROUP 1...	1.9223-01	-3.1870-02	-4.8454-02	-4.1399-02	-2.3684-02	-5.3197-03
GROUP 2...	9.7274-01	-1.4408-01	-2.5771-01	-2.1250-01	-1.2076-01	-3.0099-02
GROUP 3...	1.8659+00	-3.5276-01	-5.0672-01	-4.0624-01	-2.3180-01	-6.0689-02
GROUP 4...	2.1581+00	-3.1464-01	-5.7137-01	-4.7544-01	-2.7314-01	-7.4667-02
GROUP 5...	2.5190+00	-4.6470-01	-6.7062-01	-5.5324-01	-3.2080-01	-9.2747-02
GROUP 6...	2.1146+00	-4.0584-01	-5.5815-01	-4.6347-01	-2.7181-01	-8.3731-02
GROUP 7...	1.7944+00	-3.0479-01	-4.6797-01	-3.9223-01	-2.3183-01	-7.6581-02
GROUP 8...	4.3957-01	-7.5624-02	-1.0947-01	-9.7154-02	-6.0707-02	-2.3971-02
GROUP 9...	3.9207-02	-5.5226-03	-1.0360-02	-7.3871-03	-4.5507-03	-2.8436-03
GROUP 10...	2.8586-02	-3.2351-03	-6.9182-03	-4.8074-03	-2.7919-03	3.0314-03
GROUP 11...	3.5139+00	-5.1467-01	-6.6933-01	-9.0385-01	-6.4352-01	-2.7306-01
GROUP 12...	1.0624-01	-2.2039-02	-2.1962-02	-2.2676-02	-1.7477-02	4.3784-04
GROUP 13...	2.4253-03	-9.5934-04	-2.7032-04	-3.5919-04	-7.6228-04	-2.3783-04
GROUP 14...	3.7353-04	-1.4958-04	-3.3653-05	-2.9764-05	-3.7321-05	6.2403-05
GROUP 15...	2.9864-09	-8.3584-10	-1.9720-10	-2.0010-10	-1.6486-10	-4.9033-10
NUMBER FLUX	7.8526+00	-1.3196+00	-1.9542+00	-1.7779+00	-1.0869+00	-3.4694-01
ENERGY FLUX	2.6974+01	-4.5970+00	-7.0067+00	-5.9539+00	-3.4932+00	-1.0075+00
REM/HR	3.4958-05	-5.9509-06	-9.0221-06	-7.7497-06	-4.5795-06	-1.3502-06

\*\*\*\*\*SHIELD DERIVATIVES FOR DETECTOR 1 AFTER 16 PACKETS\*\*\*\*\*  
 SEGMENT 2

GROUP 1...	0.0000
GROUP 2...	0.0000
GROUP 3...	0.0000
GROUP 4...	0.0000
GROUP 5...	0.0000
GROUP 6...	0.0000
GROUP 7...	0.0000
GROUP 8...	0.0000

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GROUP 9... 0.0000  
GROUP 10... 0.0000  
GROUP 11... 0.0000  
GROUP 12... 0.0000  
GROUP 13... 0.0000  
GROUP 14... 0.0000  
GROUP 15... 0.0000  
NUMBER FLUX 0.0000  
ENERGY FLUX 0.0000  
REM/HR 0.0000

THE FASTER-III PROGRAM \*\*\*\*\*INIT SHIELD TEST PROFILE\*\*\*\*\*CASE 2  
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\*\*\*\*\*WICK PLOT OF Y = LOG(TOTAL FLUX - TYPE 0) VERSUS X = LOG(ENERGY)\*\*\*\*\*



X= -1.0000+00

1.0000+00=X

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 2  
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\*\*\*\*\*QUICK PLOT OF Y = LOG(TOTAL FLUX - TYPE 2) VERSUS X = LOG(ENERGY)\*\*\*\*\*

2.0000+00  
1.9118+00  
1.8235+00  
1.7353+00  
1.6471+00  
1.5588+00  
1.4706+00  
1.3824+00  
1.2941+00  
1.2059+00  
1.1176+00  
1.0294+00  
9.4118-01  
8.5294-01  
7.6471-01  
6.7647-01  
5.8824-01  
5.0000-01  
4.1176-01  
3.2353-01  
2.3529-01  
1.4706-01  
5.8824-02  
-2.9412-02  
-1.1765-01  
-2.0588-01  
-2.9412-01  
-3.8235-01  
-4.7059-01  
-5.5882-01  
-6.4706-01  
-7.3529-01  
-8.2353-01  
-9.1176-01  
-1.0000+00

X= -2.0000+00

1.0000+00=X

THE FASTER-III PROGRAM \*\*\*\* UNIT SHIELD TEST PROBLEM \*\*\*\* CASE 2  
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\*\*\*\*\*QUICK PLOT OF Y = LOG( SOURCE ENERGY FLUX) VERSUS X = COMPONENT INDEX\*\*\*\*\*

2.0000+00  
1.7647+00  
1.5294+00  
1.2941+00  
1.0588+00  
8.2353-01  
5.8824-01  
3.5294-01  
1.1765-01  
-1.1765-01  
-3.5294-01  
-5.8824-01  
-8.2353-01  
-1.0588+00  
-1.2941+00  
-1.5294+00  
-1.7647+00  
-2.0000+00 \*  
-2.2353+00  
-2.4706+00  
-2.7059+00  
-2.9412+00  
-3.1765+00  
-3.4118+00  
-3.6471+00  
-3.8824+00  
-4.1176+00  
-4.3529+00  
-4.5882+00  
-4.8235+00  
-5.0588+00  
-5.2941+00  
-5.5294+00  
-5.7647+00  
-6.0000+00

X= 1.0000+00

7.0000+00=X

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\*\*\*\*\*QUICK PLOT OF Y = LOG( REGION ENERGY FLUX) VERSUS X = COMPONENT INDEX\*\*\*\*\*

1.0000+00  
6.1765-01  
2.3529-01  
-1.4706-01  
-5.2941-01  
-9.1176-01  
-1.2941+00  
-1.6765+00  
-2.0588+00  
-2.4412+00  
-2.8235+00  
-3.2059+00  
-3.5882+00  
-3.9706+00  
-4.3529+00  
-4.7353+00  
-5.1176+00  
-5.5000+00  
-5.8824+00  
-6.2647+00  
-6.6471+00  
-7.0294+00  
-7.4118+00  
-7.7941+00  
-8.1765+00  
-8.5588+00  
-8.9412+00  
-9.3235+00  
-9.7059+00  
-1.0088+01  
-1.0471+01  
-1.0853+01  
-1.1235+01  
-1.1618+01 \*  
-1.2000+01

X= 3.0000+00

7.0000+00=X

THE FASTER-III PROGRAM \*\*\*\*INIT SHIELD TEST PROFILE \*\*\*\*CASE 2  
T.M.JORDAN-A.L.T.RESEARCHER \*\*\*\*SECONDARY PHOTO S \*\*\*\*PAGE 14

\*\*\*\*\*CUTCH PLOT OF Y = LOG( SCATTER ENERGY FLUX) VERSUS X = COMPONENT INDEX\*\*\*\*\*

2.0000+00  
1.9118+00  
1.8235+00  
1.7353+00  
1.6471+00  
1.5588+00  
1.4706+00  
1.3824+00 \*1.2941+00  
1.2059+00  
1.1176+00  
1.0294+00  
9.4118-01  
8.5294-01  
7.6471-01  
6.7647-01  
5.8824-01  
5.0000-01  
4.1176-01  
3.2353-01 \*  
2.3529-01 \*  
1.4706-01  
5.8824-02  
-2.9412-02  
-1.1765-01  
-2.0588-01  
-2.9412-01  
-3.8235-01  
-4.7059-01  
-5.5882-01  
-6.4706-01  
-7.3529-01  
-8.2353-01  
-9.1176-01  
-1.0000+00

X= 0.0000

4.0000+00=X

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\*\*\*\*\*SHIELD OPTIMIZATION FOR DETECTOP 1\*\*\*\*\*  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 1.5000+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 2.2075+07 1.6081+07 8.6718+07  
 DWDT(GM/CM) 4.4551+06 3.0261+06 2.5035+06 1.8727+06 1.1234+06  
 DDDT( /CM) -9.9406-06 -1.1723-05 -1.0218-05 -6.7649-06 -3.2131-06  
 DDDW( /GM) -2.2313-12 -3.8740-12 -4.0816-12 -3.6124-12 -2.8600-12  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 10 2.1025+08 2.4878-05 1.6184-05 4.1062-05 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 1.6587+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 2.4658+07 1.6375+07 8.7844+07  
 DWDT(GM/CM) 4.4922+06 3.0633+06 2.5407+06 1.8978+06 1.1354+06  
 DDDT( /CM) -9.5129-05 -1.1073-04 -9.6496-05 -6.4259-05 -3.1114-05  
 DDDW( /GM) -2.1176-11 -3.6148-11 -3.7981-11 -3.3860-11 -2.7404-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 20 2.1426+08 1.7586-05 1.3407-05 3.0992-05 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 1.8151+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 2.7252+07 1.6667+07 8.8961+07  
 DWDT(GM/CM) 4.5291+06 3.1001+06 2.5775+06 1.9227+06 1.1473+06  
 DDDT( /CM) -1.5954-04 -1.8348-04 -1.5987-04 -1.0705-04 -5.2747-05  
 DDDW( /GM) -3.5226-11 -5.9184-11 -6.2026-11 -5.5677-11 -4.5976-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 30 2.1826+08 1.2496-05 1.1137-05 2.3633-05 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 1.9693+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 2.9856+07 1.6957+07 9.0069+07  
 DWDT(GM/CM) 4.5658+06 3.1368+06 2.6142+06 1.9474+06 1.1590+06  
 DDDT( /CM) -2.0876-04 -2.3744-04 -2.0689-04 -1.3923-04 -6.9688-05  
 DDDW( /GM) -4.5722-11 -7.5694-11 -7.9140-11 -7.1496-11 -6.0128-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 40 2.2226+08 8.9234-06 9.2767-06 1.8200-05 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 2.1214+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 3.2470+07 1.7246+07 9.1169+07  
 DWDT(GM/CM) 4.6021+06 3.1732+06 2.6506+06 1.9719+06 1.1706+06  
 DDDT( /CM) -2.4673-04 -2.7783-04 -2.4210-04 -1.6368-04 -8.3081-05  
 DDDW( /GM) -5.3612-11 -8.7557-11 -9.1337-11 -8.3005-11 -7.0971-11

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROFILE \*\*\*\*\*CASE 2  
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\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 2.4163-06 7.7471-06 1.4150-05 0.0000  
 WEIGHT(GM) 1.0217+07 7.1161+07 3.5004+07 1.7533+07 9.2260+07  
 DWDT(GM/CM) 4.6383+06 3.2093+06 2.6e+06 1.9963+06 1.1822+06  
 DDDT( /CM) -2.7631-04 -3.0836-04 -2.6e+04 -1.8244-04 -9.3760-05  
 DDDW( /GM) -5.9572-11 -9.6092-11 -1.0002-10 -9.1390-11 -7.9312-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 2.4194+01 1.5000+01 1.1102-05 0.0000  
 WEIGHT(GM) 1.0217+07 7.1161+07 3.7728+07 1.7819+07 9.3344+07  
 DWDT(GM/CM) 4.6742+06 3.2453+06 2.7227+06 2.0205+06 1.1936+06  
 DDDT( /CM) -2.9957-04 -3.3163-04 -2.8903-04 -1.9697-04 -1.0234-04  
 DDDW( /GM) -6.4089-11 -1.0219-10 -1.0616-10 -9.7489-11 -8.5743-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 3.3430-06 5.4434-06 8.7864-06 0.0000  
 WEIGHT(GM) 1.0217+07 7.1161+07 4.0370+07 1.8104+07 9.4419+07  
 DWDT(GM/CM) 4.7099+06 3.2810+06 2.7584+06 2.0445+06 1.2049+06  
 DDDT( /CM) -3.1801-04 -3.4954-04 -3.0468-04 -2.0833-04 -1.0929-04  
 DDDW( /GM) -6.7518-11 -1.0654-10 -1.1046-10 -1.0190-10 -9.0703-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 2.4314-06 4.5792-06 7.0106-06 0.0000  
 WEIGHT(GM) 1.0217+07 7.1161+07 4.3022+07 1.8386+07 9.5487+07  
 DWDT(GM/CM) 4.7454+06 3.3165+06 2.7939+06 2.0683+06 1.2162+06  
 DDDT( /CM) -3.3275-04 -3.6345-04 -3.1665-04 -2.1729-04 -1.1495-04  
 DDDW( /GM) -7.0119-11 -1.0959-10 -1.1341-10 -1.0506-10 -9.4521-11  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 2.85e+01 1.5000+01 1.1700+02 0.0000  
 WEIGHT(GM) 1.0217+07 7.1161+07 4.56e3+07 1.8668+07 9.6548+07  
 DWDT(GM/CM) 4.7807+06 3.3517+06 2.8201+06 2.0920+06 1.2273+06  
 DDDT( /CM) -3.4462-04 -3.7433-04 -3.2638-04 -2.2442-04 -1.1960-04  
 DDDW( /GM) -7.2085-11 -1.1168-10 -1.1536-10 -1.0727-10 -9.7445-11

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\*\*\*\*\*ITERATION\*\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 100 2.4628+08 1.3023-06 3.2624-06 4.5643-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 2.9926+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 4.8352+07 1.8948+07 9.7601+07  
 DWDT(GM/CM) 4.8158+06 3.3868+06 2.8642+06 2.1156+06 1.2384+06  
 DDDT( /CM) -3.5425-04 -3.8292-04 -3.3391-04 -2.3013-04 -1.2343-04  
 DDDW( /GM) -7.3559-11 -1.1306-10 -1.1658-10 -1.0878-10 -9.9666-11  
 \*\*\*\*\*ITERATION\*\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 110 2.5028+08 9.5883-07 2.7626-06 3.7215-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 3.1315+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 5.1030+07 1.9227+07 9.8647+07  
 DWDT(GM/CM) 4.8507+06 3.4217+06 2.8991+06 2.1390+06 1.2494+06  
 DDDT( /CM) -3.6211-04 -3.8975-04 -3.3992-04 -2.3475-04 -1.2660-04  
 DDDW( /GM) -7.4651-11 -1.1390-10 -1.1725-10 -1.0975-10 -1.0133-10  
 \*\*\*\*\*ITERATION\*\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 120 2.5428+08 7.0862-07 2.3443-06 3.0529-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 3.2687+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 5.3715+07 1.9504+07 9.9686+07  
 DWDT(GM/CM) 4.8854+06 3.4564+06 2.9338+06 2.1622+06 1.2603+06  
 DDDT( /CM) -3.6857-04 -3.9522-04 -3.4473-04 -2.3850-04 -1.2924-04  
 DDDW( /GM) -7.5443-11 -1.1435-10 -1.1751-10 -1.1030-10 -1.0255-10  
 \*\*\*\*\*ITERATION\*\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 130 2.5829+08 5.2565-07 1.9932-06 2.5189-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 3.4043+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 5.6409+07 1.9780+07 1.0072+08  
 DWDT(GM/CM) 4.9198+06 3.4909+06 2.9683+06 2.1853+06 1.2711+06  
 DDDT( /CM) -3.7390-04 -3.9964-04 -3.4863-04 -2.4157-04 -1.3145-04  
 DDDW( /GM) -7.5998-11 -1.1448-10 -1.1745-10 -1.1054-10 -1.0342-10  
 \*\*\*\*\*ITERATION\*\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 140 2.6229+08 3.9132-07 1.6981-06 2.0894-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 3.5384+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 5.9111+07 2.0055+07 1.0174+08  
 DWDT(GM/CM) 4.9541+06 3.5252+06 3.0026+06 2.2083+06 1.2818+06  
 DDDT( /CM) -3.7833-04 -4.0324-04 -3.5180-04 -2.4409-04 -1.3331-04  
 DDDW( /GM) -7.6366-11 -1.1439-10 -1.1717-10 -1.1053-10 -1.0400-10

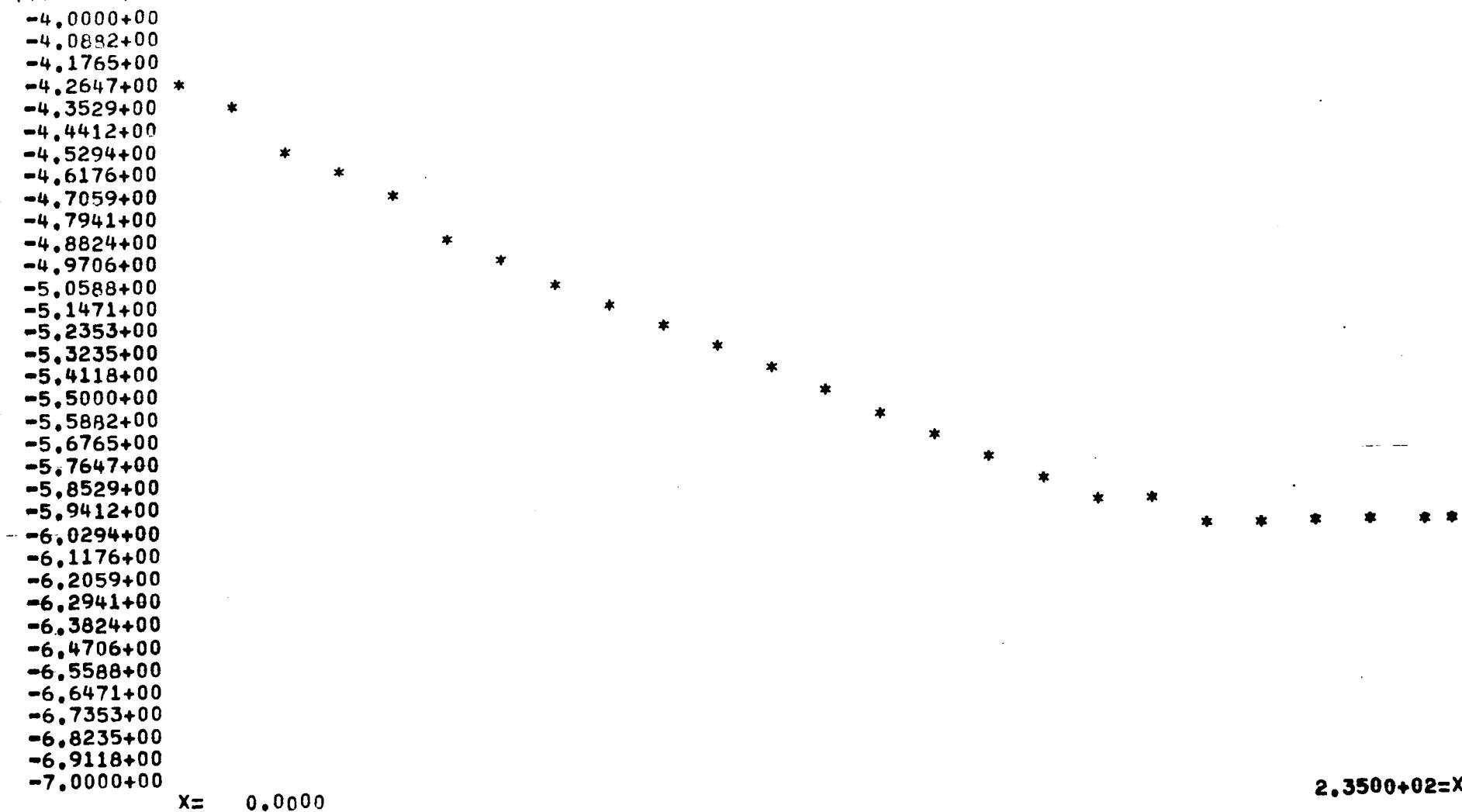
THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 2  
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\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 DIMENSIONS 5.0000+00 5.7000+01 3.6709+01 1.5000+01 1.1700+02 0.0000  
 WEIGHT(GM) 1.0217+07 7.1161+07 6.1920+07 2.0329+07 1.0276+08  
 DWDT(GM/CM) 4.9882+06 3.5593+06 3.0367+06 2.2312+06 1.2925+06  
 DDDT( /CM) -3.8202-04 -4.0617-04 -3.5440-04 -2.4618-04 -1.3487-04  
 DDDW( /GM) -7.6585-11 -1.1412-10 -1.1671-10 -1.1034-10 -1.0435-10  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 160 2.7029+08 2.1912-07 1.2393-06 1.4585-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 3.8020+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 6.4537+07 2.0601+07 1.0378+08  
 DWDT(GM/CM) 5.0222+06 3.5932+06 3.0706+06 2.2539+06 1.3031+06  
 DDDT( /CM) -3.8512-04 -4.0859-04 -3.5654-04 -2.4792-04 -1.3619-04  
 DDDW( /GM) -7.6684-11 -1.1371-10 -1.1611-10 -1.1000-10 -1.0452-10  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 170 2.7429+08 1.6478-07 1.0617-06 1.2264-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 3.9316+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 6.7261+07 2.0872+07 1.0478+08  
 DWDT(GM/CM) 5.0559+06 3.6269+06 3.1043+06 2.2764+06 1.3136+06  
 DDDT( /CM) -3.8773-04 -4.1059-04 -3.5831-04 -2.4938-04 -1.3731-04  
 DDDW( /GM) -7.6687-11 -1.1321-10 -1.1542-10 -1.0955-10 -1.0453-10  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 180 2.7830+08 1.2432-07 9.1104-07 1.0354-06 0.0000  
 DIMENSIONS 5.0000+00 5.7000+01 4.0599+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 1.0217+07 7.1161+07 6.9992+07 2.1142+07 1.0578+08  
 DWDT(GM/CM) 5.0895+06 3.6605+06 3.1379+06 2.2989+06 1.3240+06  
 DDDT( /CM) -3.8993-04 -4.1226-04 -3.5979-04 -2.5060-04 -1.3827-04  
 DDDW( /GM) -7.6614-11 -1.1262-10 -1.1466-10 -1.0901-10 -1.0443-10  
 \*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
 190 2.7910+08 1.1336-07 8.8498-07 9.9835-07 0.0000  
 DIMENSIONS 4.8039+00 5.7000+01 4.1171+01 1.5000+01 1.1700+02  
 WEIGHT(GM) 9.7953+06 7.0939+07 7.1063+07 2.1222+07 1.0608+08  
 DWDT(GM/CM) 5.0922+06 3.6691+06 3.1478+06 2.3055+06 1.3271+06  
 DDDT( /CM) -3.9191-04 -4.1374-04 -3.6111-04 -2.5170-04 -1.3913-04  
 DDDW( /GM) -7.6964-11 -1.1276-10 -1.1472-10 -1.0917-10 -1.0484-10

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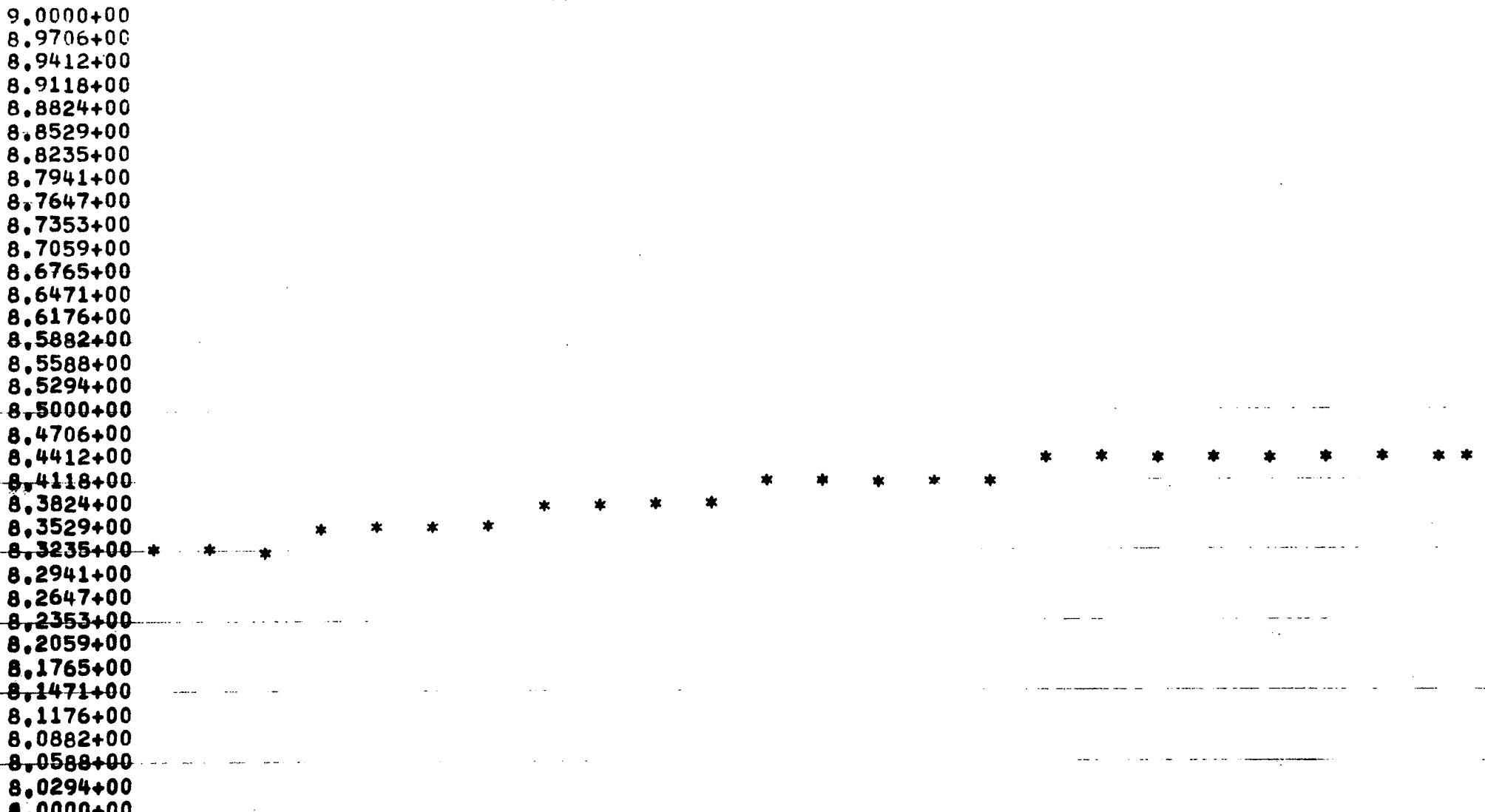
\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
DIMENSIONS 200 2.7699+08 1.1298-07 8.8918-07 1.0022-06 0.0000  
WEIGHT(GM) 4.7425+00 5.7000+01 4.1235+01 1.5000+01 1.1700+02  
DWDT(GM/CM) 9.6637+06 7.0869+07 7.1150+07 2.1222+07 1.0608+08  
DDDT( /CM) 5.0900+06 3.6687+06 3.1479+06 2.3055+06 1.3271+06  
DDDW( /GM) -3.9389-04 -4.1522-04 -3.6242-04 -2.5279-04 -1.3999-04  
DDDW( /GM) -7.7386-11 -1.1318-10 -1.1513-10 -1.0965-10 -1.0549-10  
\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
DIMENSIONS 210 2.7903+08 1.1259-07 8.8783-07 1.0004-06 0.0000  
WEIGHT(GM) 4.7395+00 5.7000+01 4.1253+01 1.5000+01 1.1700+02  
DWDT(GM/CM) 9.6571+06 7.0866+07 7.1186+07 2.1225+07 1.0609+08  
DDDT( /CM) 5.0902+06 3.6691+06 3.1483+06 2.3058+06 1.3273+06  
DDDW( /GM) -3.9587-04 -4.1669-04 -3.6372-04 -2.5388-04 -1.4085-04  
DDDW( /GM) -7.7770-11 -1.1357-10 -1.1553-10 -1.1011-10 -1.0612-10  
\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
DIMENSIONS 220 2.7903+08 1.1251-07 8.8757-07 1.0001-06 0.0000  
WEIGHT(GM) 4.7387+00 5.7000+01 4.1257+01 1.5000+01 1.1700+02  
DWDT(GM/CM) 9.6555+06 7.0865+07 7.1193+07 2.1226+07 1.0610+08  
DDDT( /CM) 5.0903+06 3.6692+06 3.1484+06 2.3058+06 1.3273+06  
DDDW( /GM) -3.9784-04 -4.1816-04 -3.6503-04 -2.5497-04 -1.4171-04  
DDDW( /GM) -7.8156-11 -1.1397-10 -1.1594-10 -1.1057-10 -1.0677-10  
\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
DIMENSIONS 230 2.7904+08 1.1250-07 8.8752-07 1.0000-06 0.0000  
WEIGHT(GM) 4.7385+00 5.7000+01 4.1257+01 1.5000+01 1.1700+02  
DWDT(GM/CM) 9.6551+06 7.0865+07 7.1195+07 2.1226+07 1.0610+08  
DDDT( /CM) 5.0903+06 3.6692+06 3.1484+06 2.3059+06 1.3273+06  
DDDW( /GM) -3.9981-04 -4.1963-04 -3.6633-04 -2.5606-04 -1.4257-04  
DDDW( /GM) -7.8544-11 -1.1437-10 -1.1636-10 -1.1105-10 -1.0742-10  
\*\*\*\*\*TERMINATION = 3 (0/1/2/3)=(DIMENSION CONSTRAINTS/ITERATIONS/UNSHIELDED/DOSE CONSTRAINT)\*\*\*\*\*  
\*\*\*\*\*ITERATION\*\*WEIGHT(GM)\*\*\*DOSE( 1 )\*\*\*DOSE( 2 )\*\*\*DOSE(TOT)\*\*UNSHIELDED\*\*\*\*\*  
DIMENSIONS 235 2.7904+08 1.1249-07 8.8750-07 1.0000-06 0.0000  
WEIGHT(GM) 4.7385+00 5.7000+01 4.1257+01 1.5000+01 1.1700+02  
DWDT(GM/CM) 9.6551+06 7.0865+07 7.1195+07 2.1226+07 1.0610+08  
DDDT( /CM) 5.0903+06 3.6692+06 3.1484+06 2.3059+06 1.3273+06  
DDDW( /GM) -4.0060-04 -4.2021-04 -3.6686-04 -2.5649-04 -1.4292-04  
DDDW( /GM) -7.8699-11 -1.1453-10 -1.1652-10 -1.1124-10 -1.0768-10

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\*\*\*\*\*QUICK PLOT OF Y = LOG(DOSE RATE) VERSUS X = ITERATION INDEX\*\*\*\*\*



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\*\*\*\*\*QUICK PLOT OF Y = LOG(WEIGHT-GRAMS) VERSUS X = ITERATION INDEX\*\*\*\*\*

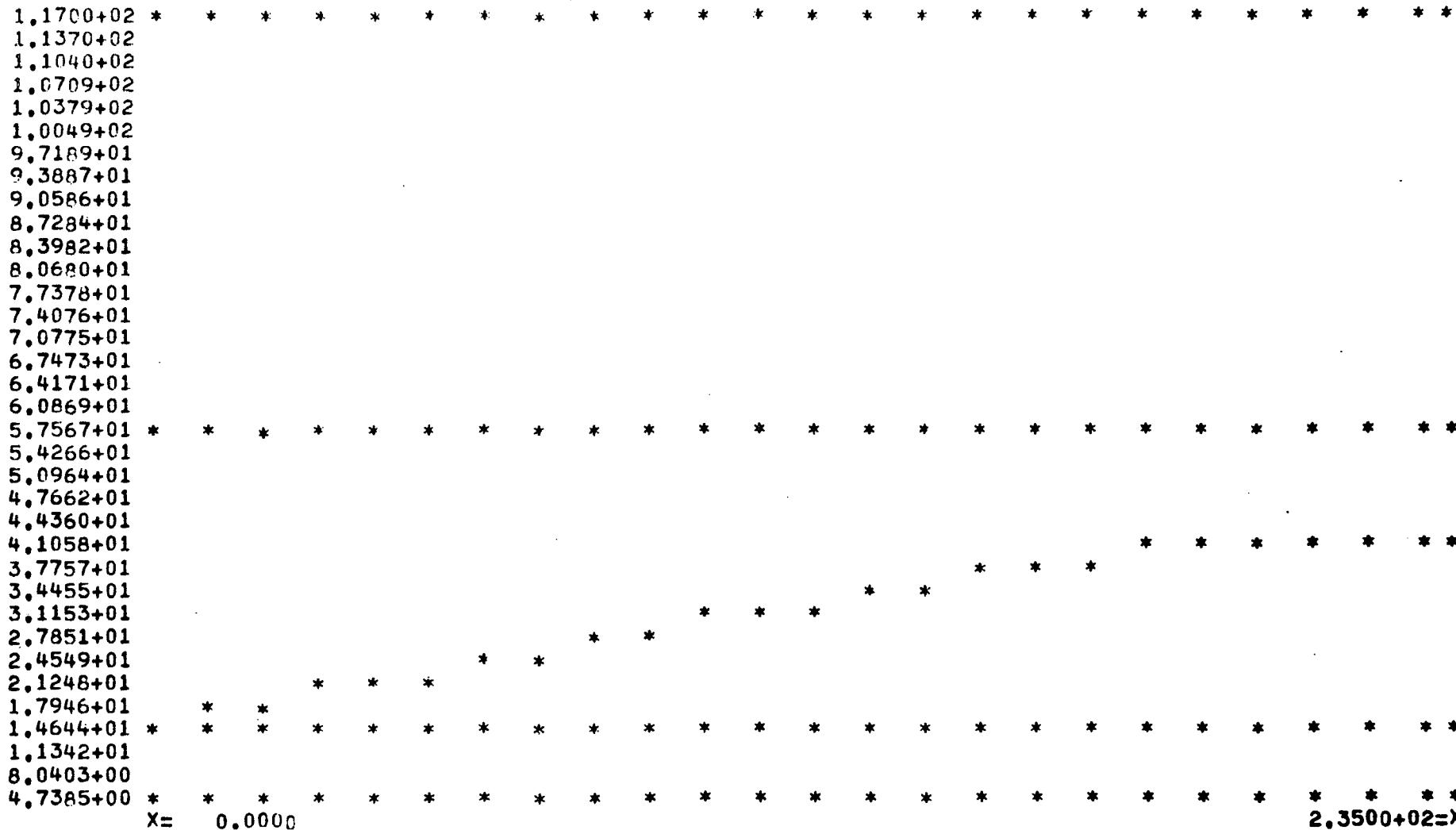


X= 0.0000

2.3500+02=X

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\*\*\*\*\*QUICK PLOT OF Y = SHIELD THICKNESS VERSUS X = ITERATION INDEX\*\*\*\*\*



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\*\*\*\*\*BOUNDARY SEARCH PARAMETERS, (SURFACE,MOST PROBABLE NEXT REGION)\*\*\*\*\*

REGION	1(	1,	2)		
REGION	2(	-1,	1)(	2,	3)
REGION	3(	-2,	2)(	3,	4)
REGION	4(	-3,	3)(	4,	5)
REGION	5(	-4,	4)(	5,	6)
REGION	6(	-5,	5)(	6,	7)
REGION	7(	-6,	6)(	7,	8)
REGION	8(	-7,	7)(	8,	-11)

THE FASTER-III PROGRAM \*\*\*\*\*UNIT SHIELD TEST PROBLEM\*\*\*\*\*CASE 3  
T.M.JORDAN-A.R.T.RESEARCH\*\*\*\*\*SECONDARY PHOTO IS\*\*\*\*\*PAGE 1

\*\*\*\*\*  
\*\*\*\*\*123456789012345678901234567890123456789012345678901234567890  
CARD IMAGE ST0.000.001.H STOP  
CARD IMAGE ST0.001.001.I C THE PROGRAM REACHED A STOP CARD AND WILL NOW GIVE A NORMAL TERMINATION  
CARD IMAGE ST0.001.002.I  
\*\*\*\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*STOP\*\*\*\*

## Appendix C

### FORTRAN VARIABLE DEFINITIONS

All variables, except for variable-dimensioned arrays, are stored in named common blocks. Variable-dimensioned arrays are all stored in blank common.

The fixed-location integer and real variables are listed and defined in Tables C.1, C.2, C.3, etc. corresponding to common block names CO1, CO2, CO3, etc. Many of the integer variables in these tables give the first location, in blank common, where variable-dimensioned arrays are stored. These array location integers all have a Fortran name starting with I followed by one, two, or three letters which are the array name, e.g., IA would be the first location in blank common occupied by the A array. In the tables, these location integers have been listed in the form:

I A(KMAX,JMAX,IMAX)                   definition of A array

i.e., the table gives the array name, the array dimensions, and the array definition. The variables in the named common blocks as well as the elements of the arrays stored in blank common can be dumped at specified control points in the program by input of the DUMP input section described in Appendix A.

Several of the variables listed in these tables are used only by versions of the program proprietary to A.R.T. Research Corporation.

TABLE C.1  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO1

M1	input unit logical designation
M2	output unit logical designation
M3	cross section tape unit logical designation
M4	restart tape unit logical designation
M5	collision tape unit logical designation
M6	source tape unit logical designation
M7	census tape unit logical designation
M8	scratch tape unit logical designation

TABLE C.2  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO2

KASE	problem index
NPAGE	printout page index
LINES	line count
LINEX	maximum lines per printout page
LINOUT	(0,1)=(print,no print) input cards
I LAB(24,2)	problem title

TABLE C.3  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO3

IBMCDC	machine dependency flag, not used
NSTPRE	length of blank common
NERROR	error count
NNEXT	next available location in blank common
NARRAY	maximum number of arrays
MARRAY	number of arrays in the directory
LENFLD	(1,2)=(single,double), floating point word length
LENBCD	integer (base 10) to overflow a byte (base computer)
I NAM(NARRAY)	names of arrays in the directory
I LOC(NARRAY)	first location occupied by array
I MXI(NARRAY)	dimension of third index of each array
I MXJ(NARRAY)	dimension of second index of each array
I MXK(NARRAY)	dimension of first index of each array
I IFB(NARRAY)	array type, (0,1,2)=(integer,real,BCD)

TABLE C.4  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO4

IN1	option for interpreting IN3 etc. from option card
IN2	option for input of subsequent data cards
IN3-IN24	definition depends on input section

TABLE C.5  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO5

IDRAND	index of last input section in subroutine <b>RANDØM</b>
IDRESU	index of last input section handled by subroutine <b>RESULT</b>
IDGEØM	index of last input section handled by subroutine <b>GEØMIN</b>
IDSZER	index of last input section handled by subroutine <b>SZERØ</b>
IDINSE	index of last input section handled by subroutine <b>INSECT</b>
MINPUT	maximum number of input sections
KARDID	index of the last input section input
I KAR(100)	input section identifiers
I INA(MINPUT)	input section indicator (0,1)=(never input,input)
I INB(MINPUT)	input section indicator, (0,1)=(no,yes), input this case
I INC(MINPUT)	input section indicator, value of IN2 for sections input

TABLE C.6  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO6

NIMAX	number of elements
NMMAX	number of materials
NUNITD	composition units (0,1)=( $10^{24}$ atoms/cc, gm/cc)
INDEXH	index of hydrogen in element list
I ATN(NIMAX)	atomic numbers of elements
I ATW(NIMAX)	atomic weights of elements
I ATD(NMMAX,NIMAX)	compositions in $10^{24}$ atoms/cc
MIXES	number of materials and mixtures with different hydrogen content
I MIX(MIXES)	index of material associated with the mixtures
I RHH(MIXES)	hydrogen density in the mixture
I RHM(NMMAX)	material density (gm/cc)
I DEN(3,MIXES)	sum of partial densities times atomic numbers to powers 1-3
NUNITX	composition units option
NVOLTS	internal EMP calculation flag
I PQT(8,NMMAX)	macroscopic materials properties
MIXED	number of hydrogen-material mixtures

TABLE C.7  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO7

NEPMAX	number of photon energy groups
NFØRM	number of tabulation points in form factors
NEDGES	maximum number of photoelectric edges per element
NEPMØD	NEPMAX+1
I ELP(NEPMØD)	photon energy group boundaries (Mev)
I EWP(NEPMAX)	photon energy group width (Mev)
I AEP(NEPMAX)	photon average group energy (Mev)
I VEP(NEPMAX)	photon average group velocity (cm/sec)
I PST(NEPMØD,NMMAX)	photon total cross section ( $\text{cm}^{-1}$ )
I PEA(NEPMØD,NMMAX)	photon energy absorption coefficient (Mev/cm)
I FXX(NFØRM)	form factor tabulation points
I FFC(NFØRM,NMMAX)	coherent scattering form factors
I FFI(NFØRM,NMMAX)	incoherent scattering form factors
I SPP(NEPMØD,NMMAX)	total pair production cross section ( $\text{cm}^{-1}$ )

TABLE C.7 (cont'd)

I SEL(NEPMØD,NIMAX)	microscopic photoelectric cross section (barns/atom)
I EDG(4,NEDGES,NIMAX)	photoelectric edge data
I PSH(NEPMØD)	microscopic total photon cross section for hydrogen

TABLE C.8  
DEFINITION OF VARIABLES STORED IN NAMED COMMON CO8

NEMMAX	energy groups for multigroup neutron cross sections
NØRDER	l + order of Legendre expansion of cross sections
NDØWN	l + maximum elastic down scatter
INELAS	groups initiating nonelastic transfer
NTRANS	l + maximum nonelastic transfer
LFIXUP	= 1
MGSLØW	number of diffusion groups, multigroup neutron cross sections
NEMMØD	NEMMAX+1
I ELM(NEMMØD)	multigroup energy group boundaries (Mev)
I EWM(NEMMAX)	multigroup width
I AEM(NEMMAX)	multigroup average energy
I VEM(NEMMAX)	multigroup average velocity
I STM(NEMMØD,NMMAX)	total multigroup cross section ( $\text{cm}^{-1}$ )
I EAM(NEMMØD,NMMAX)	elastic scattering energy absorption, multigroup neutron (Mev/cm)

TABLE C.8 (cont'd)

I SHM(NEMMØD)	total hydrogen cross section, multigroup neutron (barns/atom)
I SGS(max(3,NORDER), NEMMAX*NDØWN,NMMAX)	multigroup elastic scattering data
I SGI(NTRANS,INELAS, NMMAX)	nonelastic scattering multigroup cross sections ( $\text{cm}^{-1}$ )
NIDE	table length for $P_\ell$ histogram
I IDE	dummy variable

TABLE C.9

## DEFINITION OF VARIABLES STORED IN NAMED COMMON CO9

NNEMAX	number of neutron energy groups, point value cross sections
NAAMAX	number of c.m. cosines for anisotropic distributions
MAXANI	maximum number of groups with anisotropic elastic scattering
NANISØ	total number of anisotropic distributions
NØNELA	maximum number of groups with nonelastic scattering
NDRØPS	maximum transfer due to nonelastic scattering
NBSLØW	number of diffusion groups, point value neutron cross sections
NNEMØD	NNEMAX+1
I ELN(NNEMØD)	neutron energy group boundaries (Mev)
I EWN(NNEMAX)	neutron energy group widths (Mev)
I AEN(NNEMAX)	neutron average group energy
I VEN(NNEMAX)	neutron average group velocity
I CSA(NAAMAX)	tabulation cosines for anisotropic pdf's
I TSN(NNEMØD,NMMAX)	total neutron cross section ( $\text{cm}^{-1}$ )

TABLE C.9 (cont'd)

I EAN(NNEMØD,NMMAX)	energy absorption for neutron (Mev/cm)
I HSN(NNEMØD)	total hydrogen cross section (barns)
I ESN(NNEMØD,NIMAX)	elastic scattering cross section (barns)
I GSN(NDRØPS,NØNELA, NMMAX)	nonelastic transfer matrix ( $\text{cm}^{-1}$ )
I PAN(NAAMAX,NANISØ)	anistropic scattering distributions
I NAS(NØNELA,NIMAX)	indices of scattering distributions

TABLE C.10

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C10

NEEMAX	number of electron energy groups
NTABE	number of energies in input electron library
NTABZ	number of elements in input electron library
LØGANA	electron transport step size option
NESLØW	number of range-energy approximation groups
NEEMØD	NEEMAX+1
I ELE(NEEMØD)	electron energy group boundaries (Mev)
I EWE(NEEMAX)	electron energy group widths (Mev)
I AEE(NEEMAX)	average electron group energy
I VEB(NEEMAX)	average electron group velocity
I DET(NEEMØD,NMMAX)	total electron stopping power (Mev/cm)
I DER(NEEMØD,NMMAX)	radiative electron stopping power (Mev/cm)
I THS(NEEMØD,NMMAX)	mean square angular deflection per cm
I EST(NEEMØD,NMMAX)	total electron large-angle cross section ( $\text{cm}^{-1}$ )
I DEA(NEEMØD,NMMAX)	total small-angle stopping power (Mev/cm)

TABLE C.10 (cont'd)

I PEE(NEEMØD,NMMAX)	total electron-electron cross section (cm <sup>-1</sup> )
I HSE(NEEMØD)	dummy hydrogen electron total cross section (all zeros)

TABLE C.11  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C11

NGPMAX	number of photon flux groups
NGPMØD	NGPMAX+1
NFPMAX	number of photon response functions
I FLP(NGPMØD)	photon flux group boundaries
I FNP(NGPMAX)	photon flux group widths
I TDG(4,NFPMAX)	photon response titles
I RSG(NGPMØD,NFPMAX)	photon response functions

TABLE C.12  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C12

NGMMAX	number of multigroup flux groups
NGMMØD	NGMMAX+1
NFMMAX	number of multigroup response functions
I_FLM(NGMMØD)	multigroup flux boundaries
I_FW(M(NGMMAX)	multigroup flux group widths
I_TDM(4,NFMMAX)	multigroup response titles
I_RSM(NGMMØD,NFMMAX)	multigroup response functions

TABLE C.13  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C13

NGNMAX	number of neutron flux groups
NGNMØD	NGNMAX+1
NFNMAX	number of neutron response functions
I FLN(NGNMØD)	neutron flux group boundaries
I FWN(NGNMAX)	neutron flux group widths
I TDN(4,NFNMAX)	neutron response titles
I RSN(NGNMØD,NFNMAX)	neutron response functions

TABLE C.14  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C14

NGEMAX	number of electron flux groups
NGEMØD	NGEMAX+1
NFEMAX	number of electron response functions
I FLE(NGEMØD)	electron flux group boundaries
I FWE(NFEMAX)	electron flux group widths
I TDE(4,NFEMAX)	electron response titles
I RSE(NGEMØD,NFEMAX)	electron response functions

TABLE C.15  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C15

NVMAX	number of sources
NXMAX	maximum number of points per source distribution
NESMAX	maximum number of groups in any processed source spectrum
I NXS(NVMAX)	source particle type
I NSG(NVMAX)	source geometry type
I JSN(NVMAX)	index of first non-empty source group
I JSX(NVMAX)	index of last non-empty source group
I SUV(NVMAX)	total source intensity (Mev/sec)
I RSI(NVMAX)	relative source importance
I XTR(3,NVMAX)	source translation vector
I NPC(5,NVMAX)	number of tabulation points in the spatial and angular source distributions
I VMD(5,NVMAX)	preferred values of the spatial and angular source variables
I ALP(5,NVMAX)	slope of exponential for selecting spatial and angular variables
I VEE(NXMAX,5,NVMAX)	tabulation points for source distributions

TABLE C.15 (cont'd)

I VAL(NXMAX,5,NVMAX)	value of source distribution at tabulation points
I SPW(NESMAX,NVMAX)	particles in each source group
I SPE(NESMAX,NVMAX)	average energy of particles in each source group

TABLE C.16

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C16

NPFMAX	number of source time profiles
NPTMAX	number of histogram sections in each time profile
I TTB(NPTMAX,NPFMAX)	tabulation times for time profiles
I TSP(NPTMAX,NPFMAX)	value of time distribution

TABLE C.17  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C17

NSMAX	number of surfaces
NAMAX	maximum number of coefficients in the quadric surface equation
I NPT(NSMAX)	number of coefficients in each surface
I AZ(NSMAX)	$a_0$ term in surface equation
I A(NAMAX,NSMAX)	other terms in surface equation
I ND(NSMAX)	status of ray tracing calculation by surface
I XD(NSMAX)	dummy array for selecting source or collision point
I U(NSMAX)	constant term in quadratic equation for distance to surface
I V(NSMAX)	linear coefficient term in quadratic equation for distance to surface; also data in calculation of distance to collision
I W(NSMAX)	quadratic coefficient in equation for distance to a surface
I SI(2,NSMAX)	roots of equation for distance to a surface; also data in calculation of distance to collision

TABLE C.18  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C18

NRMAX	number of regions
NBMAX	maximum number of boundaries per region
I MTL(NRMAX)	index of material in region
I ISV(NRMAX)	index of volume source overlying a region
I RHO(NRMAX)	relative material density of region
I RIM(NRMAX)	relative scattering importance of region
I SGM(NRMAX)	average cross section (except hydrogen) by region
I SGH(NRMAX)	average cross section for hydrogen by region
I ALT(NRMAX)	average logarithm of the ratio of forward-to-backward scattering
I SGA(NRMAX)	total cross section for the average energy group
I BIG(NRMAX)	region volume
I XR(3,NRMAX)	coordinates of a point in region
I NS(NBMAX,NAMAX)	surface index of boundary
I NXT(NBMAX,NAMAX)	index of most probable next region

TABLE C.19

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C19

NCCMAX	number of correlated calculations
NCCMOD	NCCMAX+1
NCSMAX	number of correlated sources
NCRMAX	number of correlated regions
I ICS(NCSMAX)	indices of correlated sources
I JCS(NCCMAX,NCSMAX)	indices of replacement sources
I ICR(NCRMAX)	indices of correlated regions
I JCR(NCCMAX,NCRMAX)	indices of replacement regions
I KCS(NVMAX)	correlated source table index
I KCR(NRMAX)	correlated region table index

TABLE C.20  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C20

NDMAX	number of detectors
NFDMAX	number of point detectors
NVDMAX	number of volume detectors
NSDMAX	number of surface detectors
NVDMØD	number of surface and volume detectors
I IDR(NDMAX)	region index of detector
I IDS(NDMAX)	surface index of detector
I VØL(NDMAX)	area, volume, or scale factor for detector
I STD(NDMAX)	translation time for detector
I CDT(3,NDMAX)	fixed direction for detector
I XDT(3,NDMAX)	point detector coordinates
NDMØD	number of detectors for which fluxes are being calculated
NDMUD	NDMØD*NCCMØD

TABLE C.21  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C21

NSHELL	number of spherical zones in the atmosphere
I RAD(NSHELL)	spherical zone boundaries (cm)
NAIRPT	number of points in the tabulated air density
I AIR(NAIRPT)	air density tabulation points (cm)
I REL(NAIRPT)	relative air densities
I AAD(NSHELL)	constant term in linear air density curve
I BAD(NSHELL)	slope of linear air density curve

TABLE C.22  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C22

NRRMAX	number of radial intervals in cylindrical geometry option
NRRMØD	NRRMAX+1
I ARE(NRRMAX+1)	radii of intervals
NZZMAX	number of axial zones in the cylindrical geometry
NZZMØD	NZZMAX+1
I ZEE(NZZMØD)	axial zone boundaries (cm)
I CUE(NRRMAX,NZZMAX,4)	initial value of charge and current
I CUP(NRRMAX,NZZMAX, 4*MVØLTS)	charge and current on current time step
I VØT(NRRMAX,NZZMAX, 4*MVØLTS)	scalar and vector potentials for finite difference solution
I WØT(NRRMAX,NZZMAX, 4*MVØLTS)	scalar and vector potentials for finite difference solution
I VJH(NRRMØD,NZZMAX)	boundary potentials, radial
I VIH(NRRMAX,NZZMØD)	boundary potentials, axial
I DIE(NRRMAX,NZZMAX)	dielectric constant by cell

TABLE C.22 (cont'd)

I PER(NRRMAX,NZZMAX)	permeability by cell
I VTP(NRRMAX,NZZMAX, 4*MVØLTS)	scalar and vector potentials last time step
I VPP(NRRMAX,NZZMAX, 4*MVØLTS)	scalar and vector potentials last-1 time step
I CUR(NRRMAX,NZZMAX, 4*MVØLTS)	total charge and current by mesh cell

TABLE C.23

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C23

NDUMPS	number of dump requests
NLISTS	number of dump requests
NVAMAX	maximum number of arrays per dump request
NCBMAX	maximum number of named commons to be dumped
I NVA(NDUMPS)	number of arrays in each dump
I IDA(NVAMAX,NDUMPS)	lists of arrays to be dumped
I SUB(2,NDUMPS)	subprogram names for dumps
I IFN(NDUMPS)	point in subprogram at which dump is taken
I KAL(NDUMPS)	number of passes through dump point
I NDN(NDUMPS)	index of pass on which first dump occurs
I NDX(NDUMPS)	index of pass on which last dump occurs
I LST(NDUMPS)	LST(I) = I
I KBN(NCBMAX+1,NDUMPS)	indices of named commons to be dumped

TABLE C.24  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C24

MØDEL_P	biasing model, initial particle source point
MØDEL_Q	biasing model, initial particle direction
MØDEL_U	biasing model, distance to collision
MØDEL_V	biasing model, scattered direction
MØDELE	energy importance model
MØDELM	discrete particle-packet model
I GIM(NEXMAX)	cross section group importance
I AIM(NEXMAX)	linear buildup coefficients
I ALM(NEXMAX)	forward-backward scattering ratio
I ALH(NEXMAX)	forward-backward scattering ratio for hydrogen
MØDEL_R	Russian roulette model

TABLE C.25  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C25

NPØINT	0, fluxes at all detectors simultaneously 1, fluxes at point detectors individually
NPRINT	number of prints per cycle
NUNITS	number of packets per print
KALIDE	maximum number of collisions per history
NPDRUN	number of point detectors which have been run
IIIØUT	cycle index
IØUTER	number of cycles
IPRINT	print loop index
NTØTAL	number of packets generated
MTØTAL	number of histories run on previous print

TABLE C.26  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C26

NPEMAX	number of primary energy groups yielding secondaries
NSEMAX	number of secondary energy groups which receive secondaries
I SEC(NSEMAX,NPEMAX, NMMAX)	macroscopic secondary production cross sections
I SHA(MAXO(NEMMAX, MEMAX))	hydrogen capture cross section
NREACT	primary-secondary combination indicator
IREACT	reaction indicator
MXSECT	index of primary producing the secondary

TABLE C.27  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C27

NPL $\emptyset$ T	plot option flag
MPL $\emptyset$ T	number of plots generated
IPL $\emptyset$	location of plot buffer

TABLE C.28  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C28

IXSECT	NXSECT+1 for particle type being run
JXSECT	MXSECT+1 for particle type of prior run
NXSECT	(0,1,2,3)=(photons,multigroup neutrons, point cross section neutrons, electrons)
NEXMAX	number of cross section groups for particle being run
NEXMOD	NEXMAX+1
IELX	location of cross section group boundaries
IEWX	location of cross section group widths
ISSH	location of cross section for hydrogen
IESB	location of average group energy
TVEL	location of average group velocity
ISGT	location of total cross section
IEAC	location of energy absorption cross section
NSLOW	number of groups treated by approximate slowing down
LSLOW	(NSLOW*(NSLOW+1))/2
NFAST	number of neutron groups undergoing explicit slowing down
I D0N(LSLOW,NMMAX+1)	neutron slowing down cross sections

TABLE C.29

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C29

NEMAX	number of energy groups for particle type being run
NEMOD	NEMAX+1
IELL	location of energy group boundaries
IELW	location of energy group widths
I JWN(NCCMØD)	index of the first non-empty group out of collision or source
I JWX(NCCMØD)	index of the last non-empty group out of collision or source
I KWN(NCCMØD)	index of the first non-empty group into collision
I KWX(NCCMØD)	index of the last non-empty group into collision
I WS(NEMAX,NCCMØD)	packet weights out of collision or source
I TS(NEMAX,NCCMØD)	average time of flight out of collision or source
I ES(NEMAX,NCCMØD)	average energies out of collision or source
I WC(NEMAX,NCCMØD)	packet weights into collision
I EC(NEMAX,NCCMØD)	average energies into collision

TABLE C.29 (cont'd)

I	TC(NEMAX,NCCMØD)	average times into collision
I	XMP(NEMØD,NCCMØD)	mean free paths traversed by particle
I	SGR(NEMØD,NCCMØD)	total cross section in the last region traversed
I	SGB(NEMØD,NCCMØD)	mean free paths from source point
I	VAF(NEMAX,NCCMØD)	path length-averaged weight
I	VAE(NEMAX,NCCMØD)	path length-averaged energy
I	VAT(NEMAX,NCCMØD)	path length-averaged time
I	XAS(NEMAX)	mean square electron deflection, integrated
I	AJJ(NEMAX)	dummy array for electron transport kernel

TABLE C.30  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C30

NGMAX	number of flux groups for particle type being run
NGMØD	NGMAX+1
NFMAX	number of response functions for particle type being run
IELF	location of flux group boundaries
IFGW	location of flux group widths
ITDS	location of response titles
IRSP	location of response functions
I FXA(NGMAX,MØMENT, NDMUD)	optional flux moments storage
I FXT(NGMAX,NDMØD, NCCMØD)	total number flux
I FXE(NGMAX,NDMØD, NCCMØD)	total energy flux
I FXS(NGMAX,NDMØD, NCCMØD)	sum of flux squared
I FXP(NGMAX,NDMØD, NCCMØD)	flux from current history
I IDØ(MØMENT)	indices of flux moments
I TLE(3,MØMENT)	title of flux moments
MØMENT	total number of optional flux edits

TABLE C.31  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C31

NLEAKS	number of leakage boundaries
NDEPØS	region energy deposition option (0,1)
I ILR(NLEAKS,NCCMØD)	index of leakage boundary region
I ILS(NLEAKS,NCCMØD)	index of leakage boundary surface
I ØUL(NLEAKS,NCCMØD)	energy leakage from boundary
I ØUS(NLEAKS,NCCMØD)	energy leakage squared for boundary
I ØUP(NLEAKS,NCCMØD)	energy leakage for current particle
I DEV(NRMAX,NCCMØD, NDEPØS)	energy deposition in regions
I DES(NRMAX,NCCMØD, NDEPØS)	energy deposition squared
I DEP(NRMAX,NCCMØD, NDEPØS)	energy deposition for current particle
I CUT(NRMAX,NCCMØD, NDEPØS)	energy deposition, collision cutoff
I EUT(NRMAX,NCCMØD, NDEPØS)	energy deposition, energy cutoff
I WUT(NRMAX,NCCMØD, NDEPØS)	energy deposition, weight cutoff

TABLE C.32

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C32

NUMVØL	number of channel detectors
NUMTØT	= NUMVØL
I NUM(NUMREG,NUMVØL)	indices of regions comprising channel detector
NUMREG	maximum number of regions per channel detector
NCEMAX	number of channels
I ELC(NCEMAX)	channel boundaries (Mev)
I ETT(NCEMAX,NUMTØT, NCCMØD*DEPØS)	channel detector counts
I ETP(NCEMAX,NUMTØT, NCCMØD*NDEPØS)	channel detector counts, current particle
I ETS(NCEMAX,NUMTØT, NCCMØD*NDEPØS)	channel detector counts squared
NØISE	number of Gaussian noise functions
I GAU(NCEMAX,NCEMAX, NØISE)	Gaussian transfer function
I WHM(NØISE)	full widths at half maximum (Mev)
I WST(NCCMØD)	initial total weight of secondary particles

TABLE C.33  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C33

NCHECK	number of outer region-boundary combinations
MCHECK	maximum number of ray trace errors
LCHECK	count of ray trace errors
I NRC(NCHECK)	indices of outer regions
I NBC(NCHECK)	indices of boundaries of outer regions

TABLE C.34  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C34

NRØTRA	total number of rotation-translation inputs
I IRN(NRØTRA)	index of first source to be rotated-translated
I IRX(NRØTRA)	index of last source to be rotated-translated
I RZP(3,NRØTRA)	translation component of rotation-translation
I RZM(3,3,NRØTRA)	rotation component of rotation-translation

TABLE C.35  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C35

NCMAX	number of order-of-scatter edits
NVMØD	number of birth region edits
I IDV(NVMØD)	indices of birth regions for edits
NSRMAX	number of scattering region edits
I ISR(NSRMAX)	indices of scattering regions for edits
NBCMAX	number of boundary crossing edits
I IRB(NBCMAX)	region index for boundary crossing
I JRB(NBCMAX)	boundary crossing flag
I KRB(NBCMAX)	surface index for boundary crossing
NLMAX	number of angular flux Legendre moment edits
NAFMAX	number of cosines at which Legendre angular fluxes will be calculated
NABMAX	number of solid angle intervals for angular flux edits
I AFB(4,NABMAX)	solid angle interval boundaries
NTAMAX	number of times at which the time dependence will be evaluated
NTMØD	NTMAX+1

TABLE C.35 (cont'd)

NTBMAX	number of time bins
I TBB(NTBMAX)	time bin boundaries
NGRØUP	number of groups for edit by initial group
I DUE(NEMAX*NEMØD/2, NCCMØD,min(1, NGRØUP))	weight contribution by initial group
I FRQ(NEMAX*NEMØD/2, NCCMØD,min(1, NGRØUP))	weight contribution by initial group at collision

TABLE C.36  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C36

KINMAX	number of skin depth biasing locations
I KIN(KINMAX)	region index for skin depth bias
I KIM(KINMAX)	surface index for skin depth bias
I SKD(KINMAX)	skin depth
I SKI(KINMAX)	importance factor

TABLE C.37  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C37

LENINT	integers per collision tape record
LENGTH	reals per collision tape record
MENINT	integers per source tape record
MENGTH	number of reals per source tape record
MGMAX	number of flux groups for primary particle
MRSP	location of primary response data
MAXPAR	number of biasing parameters for primaries
MALIDE	collisions per primary particle
MFLW	location of primary flux group widths
I KNS(NCCMØD)	first non-empty group for primary particles from tape
I KXS(NCCMØD)	last non-empty group for primary particles from tape
I ISS(NØRMLD)	shield crossing flags for primaries
I WSS(MEMAX,NCCMØD)	packet weights for primary particles from tape
I ESS(MEMAX NCCMØD)	packet energies for primary particles from tape
I TSS(MEMAX,NCCMØD)	packet times for primary particles from tape

TABLE C.37 (cont'd)

I DSS(NORMLD,<sup>MEMAX</sup>,  
NCCM<sup>MD</sup>)

shield worth derivatives for primaries

MEMAX

number of primary particle energy groups

TABLE C.38

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C38

I DFN(NØRMLD+1, MGMAX, NØRCØM*NDMUD)	detector dose derivatives, present particle
I ISN(NØRMLD)	shield dependence, source packet
I ICN(NØRMLD)	shield dependence, collision packet
I DWS(NØRMLD, NEMAX, NCCMØD)	shield derivatives for source packet
I DWC(NØRMLD, NEMAX, NCCMØD)	shield derivatives for collision packet
I WGJ(NØRMLD)	shield weights
I WGD(NØRMLD)	shield weight derivatives
I DFS(NØRMLD+1, MGMAX, NØRCØM)	detector dose derivatives, primary particle
I DØS(NØRCØM, 2)	dose by component and particle type
I DDØ(NØRMLD, NØRCØM, 2)	dose derivative by shield, component, and particle
I DDT(NØRMLD)	dose derivatives
I QAL(NØRMLD)	dose/weight derivatives
I IPN(NØRMLD)	tally shield dependence

TABLE C.39  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C39

MVØLTS	time steps in the internal EMP calculation
MAXWEL	iterations in the solution of Poisson's equation
MINØRS	number of small time steps per time step
I XXB(3,NSTMAX,MVØLTS)	coordinates of particle at a region boundary
I CCB(3,NSTMAX,MVØLTS)	direction of particle at a region boundary
I BVW(NSTMAX,MVØLTS)	weight of particle at a boundary
I BVE(NSTMAX,MVØLTS)	energy of particle at a boundary
I BVT(NSTMAX,MVØLTS)	time of particle at a boundary
I JGB(NSTMAX,MVØLTS)	group of particle at a boundary

TABLE C.40

DEFINITION OF VARIABLES STORED IN NAMED COMMON C40

NMB

random number iteration counter

TABLE C.41  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C41

I T(NTMØD)	flight time raised to powers
I P(max(2,NLMAX)NØRDER)	evaluated Legendre polynomials
I AN(NTMØD)	temporary storage of transformed time moments
I BN(NTMØD)	temporary storage of transformed time moments
I CN(NTMØD)	temporary storage of transformed time moments
I DN(NTMØD)	temporary storage of transformed time moments
I AII(2*NTMØD)	factorials
I BJI(NTMØD,NTMØD)	inverted coefficient matrix for time moments
I CJI(NTMØD,NTMØD)	original coefficient matrix for time moments
I XIN(NTMØD)	temporary storage of time moments
I FLX(NTAMAX)	time dependence output array
I PAG(8,NFMAX)	output array for responses
I EMD(NFMAX,NDMØD)	sum of response squared for variance calculation

TABLE C.41 (cont'd)

I TDC(NTMØD,NGMAX)	time dependence polynomial coefficients
I AE(NGMAX)	upper boundary coefficient for flux group interpolation
I BE(NGMAX)	lower boundary coefficient
I TDA(NGMAX)	time dependence exponential slopes
I ERR(NGMAX)	variance by flux group
I PFE(NGMAX)	average energies for plots

TABLE C.42  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C42

NZERO	index of region containing the preferred point
JZERO	average source energy group index
JMIN	=1
JMAX	>0 if any packets have non-zero weights
JBAR	average energy group index
IIII	point detector index
KKKK	collision index
MN	index of source in optional edit request
INSR	index of scattering region in optional edit request
NTALLY	number of significant flux contributions from current collision
LLREG	index of the source from which the particle started
NN	index of the region in which the particle is located
NNNN	index on primary collision which generated a secondary
MMMM	dummy variable

TABLE C.42 (cont'd)

IIIDET	detector index for tallying
NNC	index of region in which the particle collides

TABLE C.43  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C43

RADIUS	radius of pseudo spherical source (cm)
XCT(3)	center of pseudo spherical source (cm)
ATA	cosine selection parameter
ATB	azimuthal angle selection parameter
ATC	distance selection parameter
ATD	fractional weight cutoff
STZERØ	distance from preferred point to center of pseudo spherical source
PHIMIN	l-cosine of angle subtended by pseudo spherical source
ATX	cosine selection parameter
RØZ(3,3)	rotation matrix from coordinate system used in sampling pseudo spherical source

TABLE C.44  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C44

DELTA	radius of sphere containing the preferred point (cm)
BDC(3)	preferred point coordinate (cm)
AT	distance to collision selection parameter, from particle position
BT	distance to collision selection parameter, from preferred point
AS	scattered direction selection parameter, towards preferred point
BS	scattered direction selection parameter, in original direction
CUTANG	cosine of small angle-large angle division

TABLE C.45  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C45

DIM	radius of "short circuit" sphere
COR(3)	center of "short circuit" sphere
PTH(4)	minimum probabilities for backwards selection of scattering point

TABLE C.46

DEFINITION OF VARIABLES STORED IN NAMED COMMON C46

XQ(9)	coordinates of particle	set aside for future elimina- tion of arguments from the ray tracing call sequence
CQ(9)	direction cosines of particle	
CXQ(9)		

TABLE C.47  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C47

DPDFDA	partial derivative of importance functions, this pass
DPDFDB	partial derivative of importance functions, last pass
PSØRS	value of fixed source pdf
PDFCØL	value of pdf used in selecting collision point
CØSDET	cosine of angle at which particle crosses detector
VØLDET	scale factor for all detector tallies
TØTALN	total weighted number flux tallied at detector
TØTALE	total weighted energy flux tallied at detector
SNØRM	= 1.0
XC(3)	coordinates of particle at collision
CC(3)	direction of particle at collision
CAB(3)	direction cosines of detector fixed direction
CØP(3)	cosines of the particle as it crosses the detector

TABLE C.47 (cont'd)

BUILDN

weighted sum of number flux tallied  
at detector

TABLE C.48

## DEFINITION OF VARIABLES STORED IN NAMED COMMON C48

NSTMAX	maximum number of regions which can be traversed by a ray
I NRG(NSTMAX)	indices of regions traversed
I NSC(NSTMAX)	indices of surfaces crossed
I NRP(NSTMAX)	alternate array for regions traversed
I NSP(NSTMAX)	alternate array for surfaces crossed
I ST(NSTMAX)	partial path lengths in the regions traversed
I STP(NSTMAX)	alternate array for partial path lengths
NSTLIM	total number of regions traversed by a ray
I RMU(NSTMAX)	distance to preferred point from ray boundary crossing
I ØME(NSTMAX)	cosine of angle to preferred point from ray boundary crossing
I DNM(NSTMAX)	derivative of collision pdf with respect to left boundary
I DNP(NSTMAX)	derivative of collision pdf with respect to right boundary

TABLE C.49

## DEFINITION OF VARIABLES STORES IN NAMED COMMON C49

NØRMLD	number of shields
NØRCØM	number of flux components seeing different shield combinations
IPRESP	index of response for shield optimization of last particle type
ISRESP	index of response for shield optimization of first (if any) particle type
ITERMX	maximum iterations in shield optimization
ITPRIN	iterations per print in shield optimization
I DRC(NDMAX)	dose rate constraint by detector
I IGS(NØRMLD)	shield geometry
I IDF(NØRMLD)	effect of shield on adjacent shield
I TIN(NØRMLD)	initial thickness of shield
I TMN(NØRMLD)	minimum thickness of shield
I TMX(NØRMLD)	maximum thickness of shield
I RIN(NØRMLD)	inner radius of shield
I RSH(NØRMLD)	shield weight coefficient except geometry factor

TABLE C.49 (cont'd)

I DWX(NORMLD)	maximum shield weight increment per iteration
I INR(NORMLD)	region index of shield
I INS(NORMLD)	surface index of shield
I IDN(NORMLD)	not used
I TVL(NORMLD)	current shield thickness

TABLE C.50

DEFINITION OF VARIABLES STORED IN NAMED COMMON C50

NOBIAS	(0,1)=(no,yes) calculate variance derivatives with respect to importance parameters
NAXPAR	total number of importance parameters
I DDB(NFMAX,NAXPAR, NDMUD)	parameter derivatives, sum
I DSB(NFMAX,NAXPAR, NDMUD)	parameter derivatives, weighted sum
I SDB(NAXPAR)	parameter derivatives
I DPB(NFMAX,NAXPAR, NDMUD)	parameter derivatives, current packet

TABLE C.51  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C51

PSI	cosine of scattering angle
RH $\phi$	density scale factor for scattering region
RHH	hydrogen density for scattering region
PDS	pdf scale factor
MM	mixture number for scattering region
MTL	material number for scattering region
JDEN	location of electron density for scattering region
LCC	dummy variable
JWS	location of source packet weights
JES	location of source packet energies
JTS	location of source packet times
JDWS	location of source packet shield derivatives
JWC	location of collision packet weights
JEC	location of collision packet energies
JTC	location of collision packet times
JDWC	location of collision packet shield derivatives

TABLE C.51 (cont'd)

KMIN	first non empty collision group
KMAX	last non empty collision group
JMINB	first non empty primary particle group
JMAXB	last non empty primary particle group
JWSS	primary particle packet weight
JESS	primary particle packet energies
JTSS	primary particle packet times
JDSS	primary particle packet shield derivatives

TABLE C.52  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C52

NQUICK	number of quick plots
I IQU(NQUICK)	quick plot primary identifier
I JQU(NQUICK)	quick plot secondary identifier
I XQU(MAXP)	abscissa of quick plot
I YQU(MAXP)	ordinate of quick plot
I KWI(95)	storage for quick plot output line

TABLE C.53  
DEFINITION OF VARIABLES STORED IN NAMED COMMON C53

MODELC	0, normal biasing 1, altered biasing for neutron capture
I CAP(NRMAX)	capture biasing probability
I ELR(NEEMOD,NMMAX)	residual electron range
IAD1	source index modifier
IAD2	surface index modifier
IAD3	region index modifier
IAD4	detector index modifier
IAD5	composition index modifier

## Appendix D

### PROGRAM LOGIC

The functions performed by the program are divided into three categories; data input and preparation, particle tracking, and output of results. These operations are controlled by the main program as shown schematically in Figure D.1.

- The data input and preparation operations are controlled by subroutine DEFINE. The basic flow of this subroutine is shown in Figure D.2. This subroutine controls all the input functions described in Appendix A.

The particle tracking may be controlled by one of two subroutines. Subroutine SØBER controls the tracking if the same particle histories are used to calculate point, surface and volume detector fluxes. The flow of this subroutine is shown in Figure D.3. Alternatively, if particle histories are generated specifically for a particular point detector, the particle tracking is controlled by subroutine SØLVER as sketched in Figure D.4.

The output of calculated fluxes is controlled by subroutine ANSWER. The output process is not complicated by any logical decisions worthy of a flow diagram.

The remainder of this appendix is devoted to a brief description of the subprograms. Since each subprogram performs a very specific task, the definitions of the named common variables in conjunction with the subprogram function should be sufficient for anyone capable of modifying the program to do so.

FIGURE D.1  
BASIC PROGRAM LOGIC

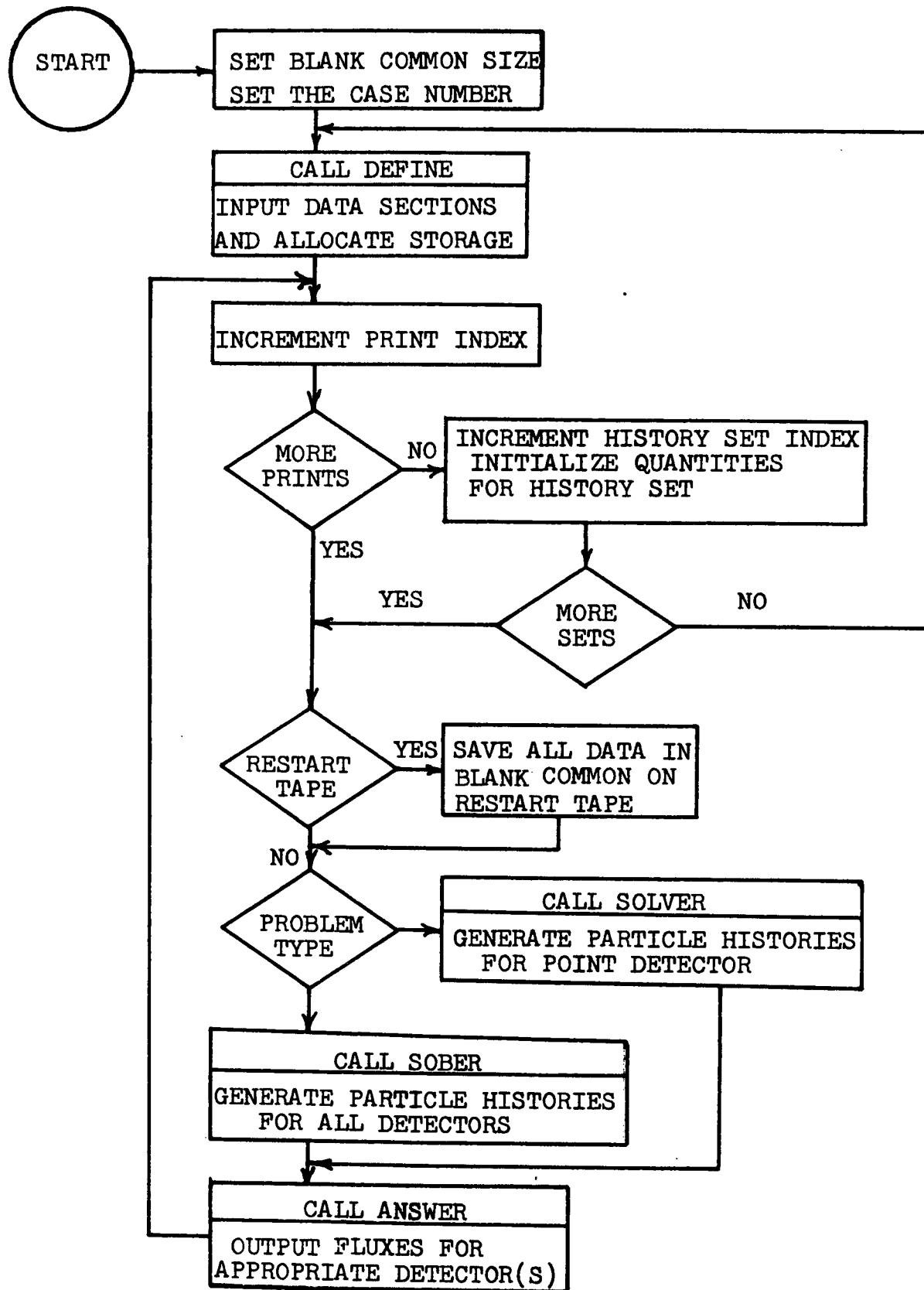


FIGURE D.2  
DATA INPUT LOGIC

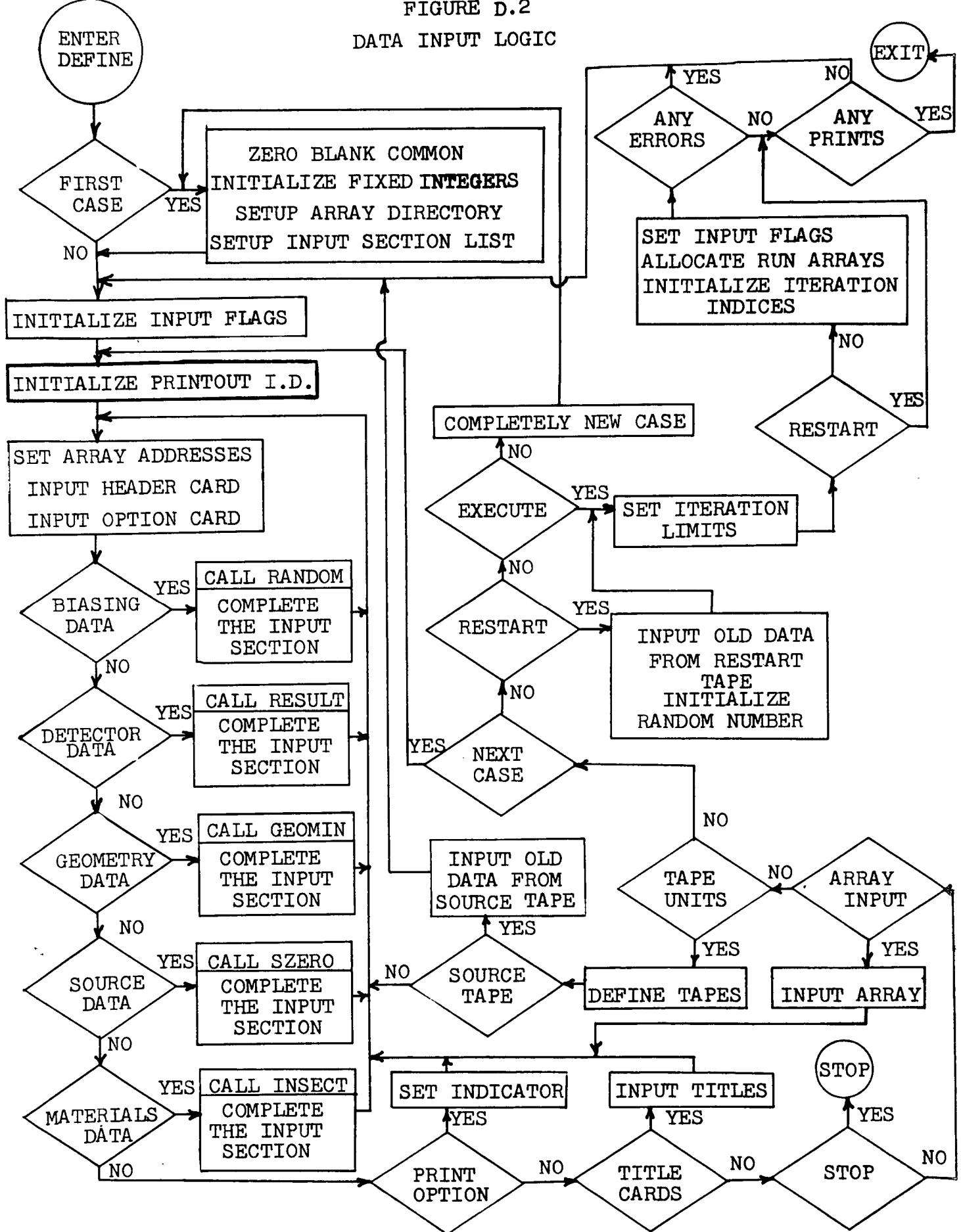


FIGURE D.3

PARTICLE TRACKING FOR MULTIPLE DETECTORS

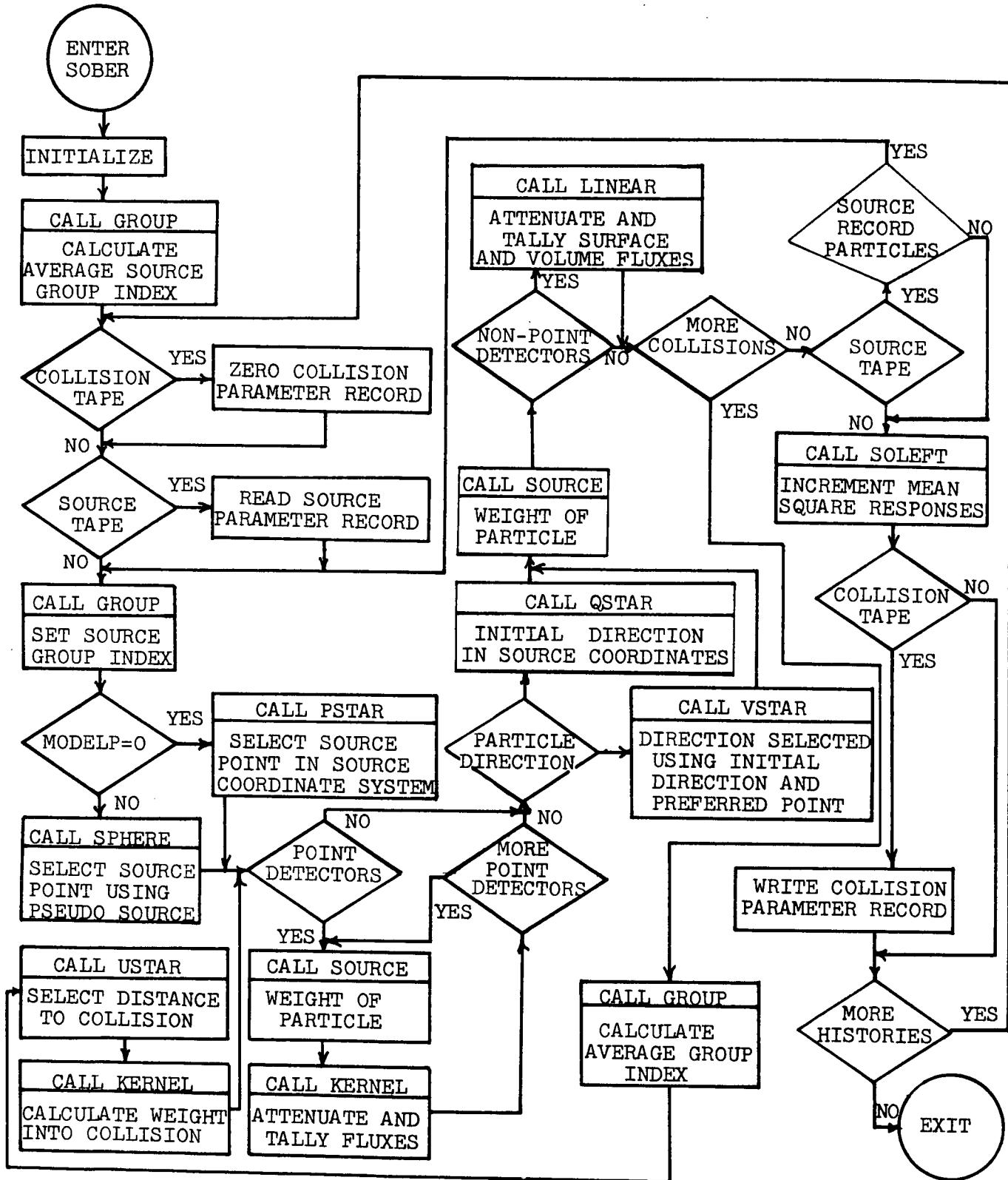
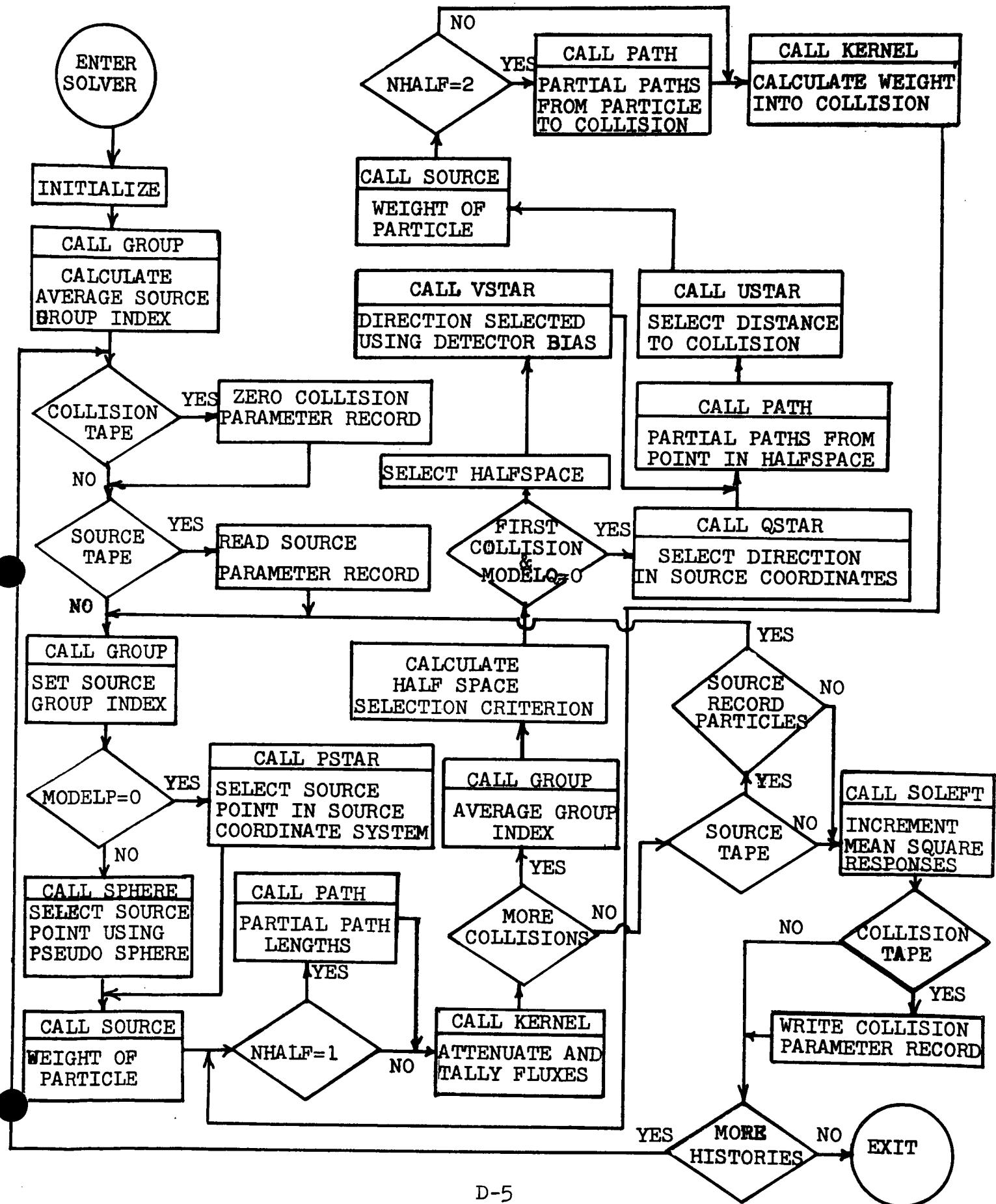


FIGURE D.4  
PARTICLE TRACKING FOR INDIVIDUAL POINT DETECTORS



A tabulation of each subprogram along with a brief description,  
is presented in Table D.1.

TABLE D.1

## SUBPROGRAMS

<u>Subprogram</u>	<u>Function</u>
MAIN	Provides the calling sequence to the subprograms which control the input, particle tracking and output of results.
INTZ	Calculates the largest integer $\leq$ the absolute value of the argument.
ZMIN1	Calculates the minimum of two arguments.
AMAX1	Calculates the maximum of two arguments.
ZBS	Calculates the absolute value of an argument.
ZQRT	Computes the square root of the argument.
ZXP	Exponentiates the argument (base e).
ZLOG	Computes the natural logarithm of the argument.
ZTAN2	Calculates the arctangent of the arguments.
ZIN	Computes the sine of the argument.
ZOS	Calculates the cosine of the argument.
VECTOR	Calculates the distance and direction between two points.

ROTATC	Calculates the sine and cosine of two rotation angles given the direction cosines.
ROTATE	Calculates the direction vector rotation matrix given the sines and cosines of the rotation angles.
CENTER	Controls the rotation-translation of source coordinates.
ROTATX	Performs the rotation-translation of source coordinates.
COSINE	Computes the cosine of the angle between two direction vectors.
RANNØ	Generates pseudo random numbers uniformly distributed on the open interval (0,1).
SAMPLE	Selects points at random from a truncated exponential distribution.
LABEL	Counts printout lines and inserts printout headings at the top of each page.
DUMPIT	Prints the elements of variable-dimensioned arrays and named common blocks as requested by input data.
KØMMØN	Controls the initialization, input and output of named common blocks.
INTCØM	Performs the initialization, input and output of named common blocks.

LOCATE	Calculates the index of the region in which a particle is located.
HELIX	Calculates quantities related to helical and toroidal surfaces.
DEFINE	Controls the input and data preparation phases of a problem.
INDEX	Allocates storage for variable-dimensioned arrays.
ICHECK	Checks order of ordered arrays.
JCHECK	Checks index against permissible range.
KCHECK	Checks input-section input order.
READH	Inputs H format data (header card).
READA	Inputs A format (24A3) hollerith data.
READI	Inputs I format (24I3) integer data.
READIS	Inputs IS format (12(2I3)) indices and integer data.
READE	Inputs E format (8E9.0) decimal data.
READEE	Inputs EE format (4(2E9.0)) logical pair decimal data.
READIE	Inputs IE format (6(I3,E9.0)) logical pair integer-decimal data.

READES	Inputs ES format (6(I3,E9.0)) indices and decimal data.
READS	Inputs S format (3I3,7E9.0) integer and decimal data.
READR	Inputs R format (12I3,4E9.0) integer and decimal data.
READF	Inputs F format (6(I2,A1,E9.0)) DTF-IV cross section data.
READL	Inputs L format (14X,6E10.0) LRL photon cross section data.
READIT	Inputs all data cards in a variable field length format
tARRAY	Allocates storage for input arrays.
ARRAY	Inputs elements of a specified array.
INSECT	Inputs materials compositions and controls microscopic cross section inputs.
MULTIX	Forms macroscopic cross sections from microscopic multigroup neutron cross sections.
MATRIX	Inputs multigroup neutron cross sections.
GAMMAX	Inputs photon cross sections and calculates macroscopic cross sections.

BASICX	Inputs and prepares point value neutron cross sections.
SLØWER	Inputs and prepares electron cross sections.
SZERØ	Controls the input and normalization of the spatial, angular, and energy distributions of the source distributions.
GEØMIN	Inputs both simple geometries and the more general surface-region descriptions.
RESULT	Controls the input of detectors and output requests.
REXTRA	Inputs optional output requests.
RANDOM	Inputs biasing options and biasing parameters.
RLIMIT	Sets limits used during particle tracking.
RARRAY	Allocates storage for run arrays.
DØWN	Calculates coefficients for neutron slowing down model.
REGION	Checks the input geometry
ASKFØR	Sets up data for flux output.
BIASIT	Sets the values of all biasing options and parameters not input.

SØLVER	Controls the generation and tracking of particle histories for individual point detectors.
SØBER	Controls the generation and tracking of particles for point, surface and volume detectors.
DØSES	Calculates the sums of the mean square responses at each detector from each particle. Writes collision records on tape.
LINEAR	Controls the calculation of surface-and volume-averaged fluxes along a particle path.
SØURCE	Controls the calculation of particle weights from the independent source, from scattering events, and from secondary interactions.
SINPUT	Calculates packet weights from input sources.
CAPTUR	Calculates secondary gamma ray weights.
CØMPTN	Calculates secondary electron weights
BREMSS	Calculates secondary bremsstrahlung weights
SCATTR	Performs the calculation of scattered particle weights from pre-collision weights using multigroup cross sections.

PHOTON	Performs the calculation of scattered photon weights from the pre-collision weights.
NEUTRN	Calculates scattered neutron weights using point value cross sections.
BETAS	Calculates scattered electron weights.
THERML	Calculates slow neutron weights using approximate slowing down model.
UNITRA	Calculates scattered components of shield derivative worth, etc.
PATH	Calculates the partial path lengths from an initial position along a specified direction up to a maximum total distance.
NORMAL	Calculates the surface normal at a specified point on a surface.
KERNEL	Calculates the particle attenuation along the particle path and generates the pre-collision particle weights.
AHEAD	Calculates the electron attenuation and slowing down along segments of the particle path.
DETECT	Performs all the tallies of particle fluxes for all the detector types.
GROUP	Calculates the group index to be used in the biased selection of scattering points and direction for all the particles.

SPHERE	Selects the initial particle position from the fixed sources in a spherical coordinate system centered at a preferred point.
PSTAR	Selects the initial particle position by first selecting the source and then selecting the spatial coordinates in the source coordinate system.
QSTAR	Selects the initial particle direction in the coordinate system for the originating source.
USTAR	Selects the distance to collision from the exponential transformation or from a curve fit of an approximation to the optimal distribution for collision points.
VSTAR	Selects the initial or scattered particle direction in a rotated coordinate system which forces particles both in their pre-collision direction and in the direction of the preferred point.
ANSWER	Controls the output of fluxes and other quantities for all of the detectors.
DEPOS	Outputs energy deposition by region, energy leakage, and channel detector tallies
FLUXES	Outputs basic flux quantities and optional edits.

PLØTNE	Generates plotted and/or punched output.
TIMER	Calculates time-dependent fluxes from time moments.
DERIVE	Outputs flux components and derivatives with respect to surface normals.
ØPTIMA	Adjusts shield dimensions to give the minimum weight shield which meets a specified dose constraint.
TEMPER	Controls the time-dependent tracking of electrons for internal EMP calculations.
VØLTS	Controls the finite difference solution of Maxwell's equations for the scalar and vector potentials.
PØTENT	Solves Maxwell's equation by iterative finite difference techniques.
LØØKC	Controls output of most quick plots.
QUICKP	Prints quick plot output.

## Appendix E

### MACHINE CONSIDERATIONS

This appendix outlines the differences in the program source deck when used on the IBM 7090, IBM 360, UNIVAC 1108 and CDC 6600 series computers.

#### 1. General Considerations

##### BLANK COMMON SIZE

It may be necessary on various computers to increase or decrease the size of blank common. The necessary changes are made in the main program and consist of changing two Fortran statements. To change the size to N locations, the following cards should be substituted.

```
DIMENSION      LA(N)
NSTØRE = N
```

##### DOUBLE PRECISION

The program can be converted to double precision in a routine manner on the IBM 360 and UNIVAC 1108 computers by use of the following implicit statement in the main program and each subprogram

```
IMPLICIT      REAL*8(A-H,Ø-Z)
```

In addition, the single precision function calls in subprograms INTZ, ZMIN1, ZMAX1, ZBS, ZQRT, ZX<sub>P</sub>, ZLØG, ZTAN2, ZIN, and ZØS should be changed to their double precision equivalents. Finally, one Fortran statement in the main program must be changed to read

```
IBMCDC = 5
```

### PRINTOUT

The number of printout lines per page can be changed for different paper sizes by altering one card in the main program to read

LINEX = L

where L is the desired maximum line count.

### INPUT AND OUTPUT UNITS

The logical designation of the input unit can be changed from 5 to I by substituting the following card in the main program

M1=I

where I denotes the desired logical designation. Similarly, the logical designation of the output tape can be changed from 6 to J by substituting the following card in the main program

M2=J

### EBCDIC DATA COMPATIBILITY

There is a DATA statement in subroutine READIT which allows the program to interpret both BCD and EBCDIC data cards. Some compilers will not accept this statement, and the following change (BCD) should be made:

replace DATA JEBCDP/1H<sup>12</sup>6/ by DATA JEBCDP/1H+/8

## CALCOMP PLOTTING

The program interfaces with the Calcomp plot package through four entry points PL $\emptyset$ T, PL $\emptyset$ TS, SYMB $\emptyset$ L, and NUMBER. If plotting is required, the dummy subprograms with these names should be removed. The plot output is generated on logical unit 10. If a different unit, I, is used at a particular installation the following card should be changed in the main program

M9=I

## 2. Program Segmentation

Segmentation of the program permits the execution of much larger problems since the size of blank common can be adjusted to its maximum. The maximum degree of segmentation for efficient operation is shown in Figure E.1 and the various subprograms included in each segment (link, overlay) are listed in Table E.1. This degree of segmentation (if any) is not used on all computer systems.

## 3. IBM 360 OS Control Cards

The program should use overlays on the 360 to minimize storage requirements for the object deck. The maximum level of overlaying is not required, however. For some problems it is best to use the double precision conversion described above. The necessary control cards for a compile and execute are given in Table E.2.

## 4. IBM 7090 Control Cards

The program will run problems on a 7094 with a direct couple operating system. The maximum amount of overlaying is used.

FIGURE E.1  
OVERLAY STRUCTURE

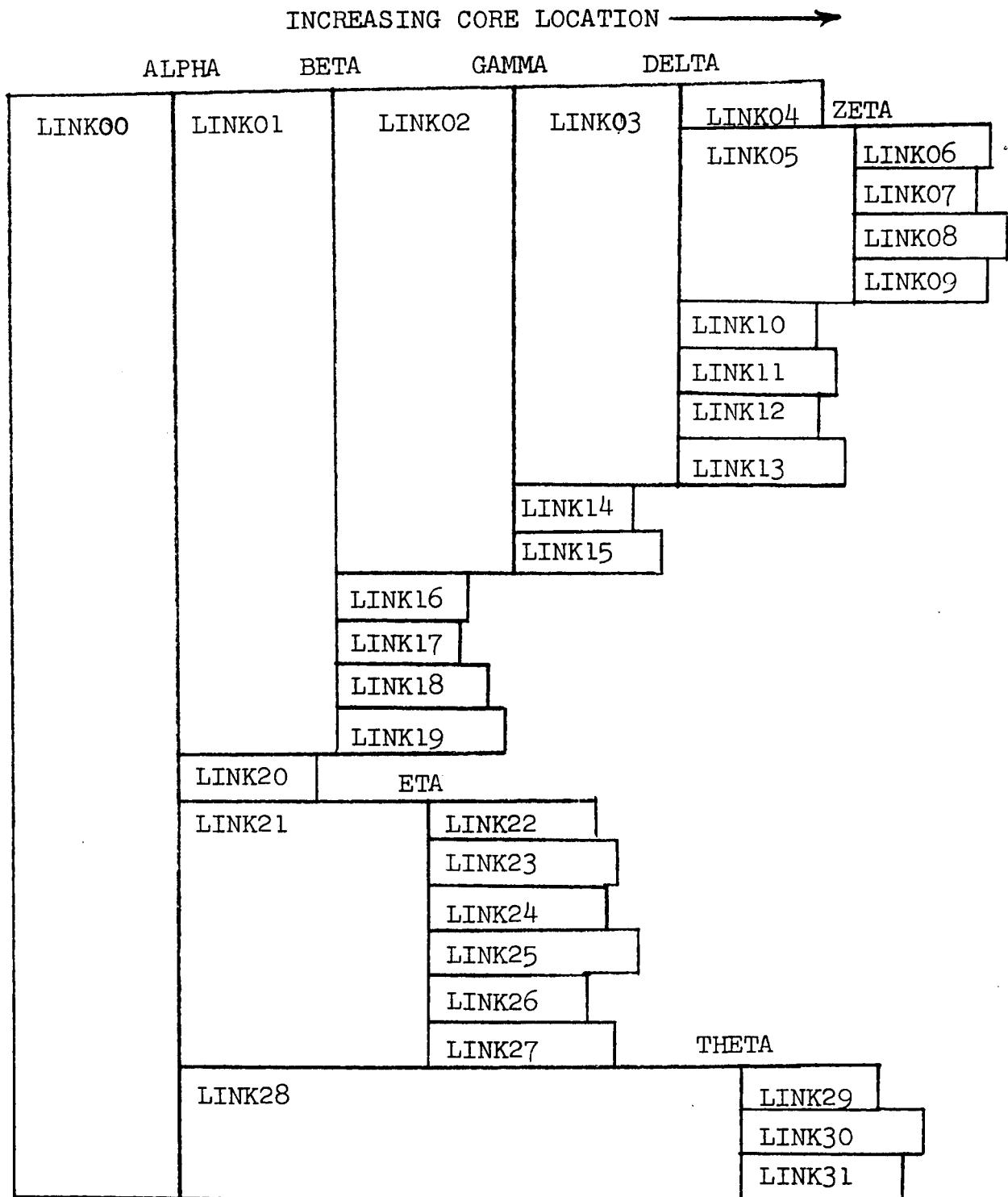


TABLE E.1  
OVERLAY DEFINITION

<u>Segment</u>	<u>Subprogram</u>	<u>IBM Deck Name</u>
LINKOO	MAIN	MAIN
	INTZ	INTL
	ZBS	ZBSL
	ZQRT	ZQRL
	ZXP	ZXPL
	ZLØG	ZLØL
	ZIN	ZINL
	ZØS	ZØSL
	ZMIN1	ZMIL
	ZMAX1	ZMAL
	ZTAN2	ZTAL
	LABEL	LADE
	DUMPIT	DUML
	KØMMØN	KØMM
	INTCØM	INTC
	CØSINE	CØSI
	VECTØR	VECT
	RØTATE	RØTA
	RØTATC	RØTC
	CENTER	CENT
	RØTATX	RØTX
	LØCATE	LØCA
	HELIX	HELI
	SAMPLE	SAMP
	RANNØ	RANN
	PLØTS	PLØM
	PLØT	PLØN
	SYMBØL	SYMB
	NUMBER	NUMB

TABLE E.1 (Cont'd)

<u>Segment</u>	<u>Subprogram</u>	<u>IBM Deck Name</u>
LINK01	DEFINE	DEFI
LINK02	INDEX	INDE
	ICHECK	ICHE
	JCHECK	JCHE
	KCHECK	KCHE
LINK03	READIT	READ
	READH	HREA
	READA	AREA
	READI	IREA
	READII	IIRE
	READIS	ISRE
	READE	EREA
	READEE	EERE
	READIE	IERE
	READES	ESRE
	READS	SREA
	READR	RREA
	READF	FREA
	READL	LREA
	IARRAY	IARR
LINK04	ARRAY	ARRA
LINK05	INSECT	INSE
LINK06	MULTIX	MULT
	MATRIX	MATR
LINK07	GAMMAX	GAMM
LINK08	BASICX	BASI
LINK09	SLØWER	SLØW
LINK10	SZERØ	SZER
LINK11	GEØMIN	GEØM

TABLE E.1 (Cont'd)

<u>Segment</u>	<u>Subprogram</u>	<u>IBM Deck Name</u>
LINK12	RESULT	RESU
	REXTRA	REXT
LINK13	RANDOM	RAND
LINK14	RLIMIT	RLIM
LINK15	RARRAY	RARR
LINK16	DØWN	DØWL
LINK17	REGION	REGI
LINK18	ASKFOR	ASKF
LINK19	BIASIT	BIAS
LINK20	VØLTS	VØLT
	PØTENT	PØTE
LINK21	ANSWER	ANSW
	LØØKC	LØØK
	QUICKP	QUIC
LINK22	DEPØS	DEPØ
LINK23	FLUXES	FLUX
LINK24	PLØTNE	PLØL
LINK25	DERIVE	DERI
LINK26	TIMER	TIME
LINK27	ØPTIMA	ØPTI
LINK28	SØURCE	SØUR
	SINPUT	SINP
	CAPTUR	CAPT
	BREMSS	BREM
	CØMPTN	CØMP
	PHØTØN	PHØT
	SCATTR	SCAT
	NEUTRN	NEUT
	BETAS	BETA
	THERML	THER
	UNITRA	UNIT
	PATH	PATL

TABLE E.1 (Cont'd)

<u>Segment</u>	<u>Subprogram</u>	<u>IBM Deck Name</u>
	NØRMAL	NØRM
	KERNEL	KERN
	AHEAD	AHEA
	DETECT	DETE
	DØSES	DØSE
	GRØUP	GRØU
	SPHERE	SPHE
	PSTAR	PSTA
	QSTAR	QSTA
	USTAR	USTA
	VSTAR	VSTA
LINK29	TEMPER	TEMP
LINK30	SØLVER	SØLV
LINK31	SØBER	SØBE
	LINEAR	LINE

TABLE E.2

## IBM SYSTEM 360/OPERATING SYSTEM CONTROL CARDS

```

JOB-ACCOUNTING CARD
// EXEC ZFORTG,PARM=BCD (OMIT PARM=BCD IF DECK IS IN EBCDIC)
//FORT.SYSIN DD *
      SOURCE DECK FOR THE MAIN PROGRAM AND ALL SUBPROGRAMS
/*
// EXEC ZLINKFRT,PARM,LKEDT=,LIST,MAP,OVLY,LET,SIZE(200K,100K)*, *
//           COND.GO=(8,LT)
//LKEDT.SYSIN DD *
      INSERT MAIN,INTZ,ZBS,ZQRT,ZXP,ZLOG,ZIN,ZOS,ZMIN1,ZMAX1,ZTAN2,LABEL
      INSERT DUMPIT,KCOMMON,INTCOM,COSINE,VECTOR,ROTATE,ROTATC,CENTER,ROTATX
      INSERT LOCATE,HELIX,SAMPLE,RANNO,PLOTS,PLOT,NUMBER,SYMBOL
      OVERLAY ALPHA
      INSERT DEFINE
      OVERLAY BETA
      INSERT INDEX,ICHECK,JCHECK,KCHECK
      OVERLAY GAMMA
      INSERT READIT,READH,READA,PEADI,READII,READIS,READE,READEE,READIE
      INSERT READES,READS,READR,READF,READL,IARRAY
      OVERLAY DELTA
      INSERT AARRAY
      OVERLAY DELTA
      INSERT INSECT
      OVERLAY ZETA
      INSERT MULTIX,MATRIX
      OVERLAY ZETA
      INSERT GAMMAX
      OVERLAY ZETA
      INSERT BASICX
      OVERLAY ZETA
      INSERT SLOWER
      OVERLAY DELTA
      INSERT SZERO
      OVERLAY DELTA
      INSERT GEOMIN
      OVERLAY DELTA
      INSERT RESULT,REXTA
      OVERLAY DELTA
      INSERT RANDOM
      OVERLAY GAMMA
      INSERT RLIMIT
      OVERLAY GAMMA
      INSERT RARRAY
      OVERLAY BETA
      INSERT DOWN
      OVERLAY BETA
      INSERT REGION
      OVERLAY BETA
      INSERT ASKFOR
      OVERLAY BETA
      INSERT BIASIT

```

TABLE E.2 (Cont'd)

OVERLAY ALPHA  
INSERT VOLTS,POTENT  
OVERLAY ALPHA  
INSERT ANSWER,LOOKC,QUICKP  
OVERLAY ETA  
INSERT DEPOS  
OVERLAY ETA  
INSERT FLUXES  
OVERLAY ETA  
INSERT PLOTNE  
OVERLAY ETA  
INSERT DERIVE  
OVERLAY ETA  
INSERT TIMER  
OVERLAY ETA  
INSERT OPTIMA  
OVERLAY ALPHA  
INSERT SOURCE,SINPUT,CAPTUR,BREMSS,COMPTN,PHOTON,SCATTR,NEUTRN,BETAS  
INSERT THERML,UNITRA,PATH,NORMAL,KERNEL,AHEAD,DETECT,DOSES,GROUP  
INSERT SPHERE,PSTAR,QSTAR,USTAR,VSTAR  
OVERLAY THETA  
INSERT TEMPER  
OVERLAY THETA  
INSERT SOLVER  
OVERLAY THETA  
INSERT SOBER,LINEAR  
ENTRY MAIN  
/\*  
//GO.SYSIN DD \*  
DATA DECKS  
/\*  
//

For some installations, it may be necessary to include a unit routine. The control cards for this computer are given in Table E.3.

#### 5. UNIVAC 1108 Control Cards

The program is run on the 1108 in single precision. The control cards for a compile and execute run under the EXEC-2 operating system are given in Table E.4. The control cards for EXEC-8 are given in Table E.5.

#### 6. Control Data 6600 Control Cards

The program is normally run in single precision on the 6600. The control cards for running without overlays are shown in Table E.6. Overlaying on the 6600 would require several minor source program changes.

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TABLE E.3  
IBM 7090 CONTROL CARDS

\$JOB-ACCOUNTING CARD	
SIBSYS	IBJOB
SIBJOB	GO,MAP,SOURCE,FIOCS
SIBFTC MAIN	DECK
	SOURCE DECK FOR MAIN PROGRAM
SIBFTC INTL	DECK
	SOURCE DECK FOR SUBPROGRAM INTZ, ETC.
SIBFTC ZBSL	DECK
SIBFTC ZQRL	DECK
SIBFTC ZXPL	DECK
SIBFTC ZLOL	DECK
SIBFTC ZINL	DECK
SIBFTC ZOSL	DECK
SIBFTC ZMIL	DECK
SIBFTC ZMAL	DECK
SIBFTC ZTAL	DECK
SIBFTC LABE	DECK
SIBFTC DUML	DECK
SIBFTC KOMM	DECK
SIBFTC INTC	DECK
SIBFTC COSI	DECK
SIBFTC VECT	DECK
SIBFTC ROTA	DECK
SIBFTC ROTC	DECK
SIBFTC CENT	DECK
SIBFTC ROTX	DECK
SIBFTC LOCA	DECK
SIBFTC HELI	DECK
SIBFTC RANN	DECK
SIBFTC SAMP	DECK
SIBFTC PLOM	DECK
SIBFTC PLON	DECK
SIBFTC SYMB	DECK
SIBFTC NUMB	DECK
SORIGIN	ALPHA
SIBFTC DEFI	DECK
SORIGIN	BETA
SIBFTC INDE	DECK
SIBFTC ICHE	DECK
SIBFTC JCHE	DECK
SIBFTC KCHE	DECK
SORIGIN	GAMMA
SIBFTC READ	DECK
SIBFTC HREA	DECK
SIBFTC AREA	DECK
SIBFTC IREA	DECK
SIBFTC IIRE	DECK
SIBFTC ISRE	DECK
SIBFTC EREA	DECK
SIBFTC EERE	DECK

TABLE E.3 (Cont'd)

\$IBFTC IERE	DECK
\$IBFTC ESRE	DECK
\$IBFTC SREA	DECK
\$IBFTC RREA	DECK
\$IBFTC FREA	DECK
\$IBFTC LREA	DECK
\$IBFTC IARR	DECK
\$ORIGIN	DELTA
\$IBFTC ARRA	DECK
\$ORIGIN	DELTA
\$IBFTC INSE	DECK
\$ORIGIN	ZETA
\$IBFTC MULT	DECK
\$IBFTC MATR	DECK
\$ORIGIN	ZETA
\$IBFTC GAMM	DECK
\$ORIGIN	ZETA
\$IBFTC BASI	DECK
\$ORIGIN	ZETA
\$IBFTC SLOW	DECK
\$ORIGIN	DELTA
\$IBFTC SZER	DECK
\$ORIGIN	DELTA
\$IBFTC GEOM	DECK
\$ORIGIN	DELTA
\$IBFTC RESU	DECK
\$IBFTC REXT	DECK
\$ORIGIN	DELTA
\$IBFTC RAND	DECK
\$ORIGIN	GAMMA
\$IBFTC RLIM	DECK
\$ORIGIN	GAMMA
\$IBFTC RARR	DECK
\$ORIGIN	BETA
\$IBFTC DOWL	DECK
\$ORIGIN	BETA
\$IBFTC REGI	DECK
\$ORIGIN	BETA
\$IBFTC ASKF	DECK
\$ORIGIN	BETA
\$IBFTC BIAS	DECK
\$ORIGIN	ALPHA
\$IBFTC VOLT	DECK
\$IBFTC POTE	DECK
\$ORIGIN	ALPHA
\$IBFTC ANSW	DECK
\$IBFTC LOOK	DECK
\$IBFTC QUIC	DECK
\$ORIGIN	ETA
\$IBFTC DEPO	DECK

TABLE E.3 (Cont'd)

\$ORIGIN	ETA
\$IBFTC FLUX	DECK
\$ORIGIN	ETA
\$IBFTC PLOL	DECK
\$ORIGIN	ETA
\$IBFTC DERI	DECK
\$ORIGIN	ETA
\$IBFTC TIME	DECK
\$ORIGIN	ETA
\$IBFTC OPTI	DECK
\$ORIGIN	ALPHA
\$IBFTC SOUR	DECK
\$IBFTC SINP	DECK
\$IBFTC CAPT	DECK
\$IBFTC BREM	DECK
\$IBFTC COMP	DECK
\$IBFTC PHOT	DECK
\$IBFTC SCAT	DECK
\$IBFTC NEUT	DECK
\$IBFTC BETA	DECK
\$IBFTC THER	DECK
\$IBFTC UNIT	DECK
\$IBFTC PATL	DECK
\$IBFTC NORM	DECK
\$IBFTC KERN	DECK
\$IBFTC AHEA	DECK
\$IBFTC DETE	DECK
\$IBFTC DOSE	DECK
\$IBFTC GROU	DECK
\$IBFTC SPHE	DECK
\$IBFTC PSTA	DECK
\$IBFTC QSTA	DECK
\$IBFTC USTA	DECK
\$IBFTC VSTA	DECK
\$ORIGIN	THETA
\$IBFTC TEMP	DECK
\$ORIGIN	THETA
\$IBFTC SOLV	DECK
\$ORIGIN	THETA
\$IBFTC SOBE	DECK
\$IBFTC LINE	DECK
\$DATA	

DATA DECK

TABLE E.4

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## UNIVAC 1108, EXEC-2 CONTROL CARDS

@JOB-ACCOUNTING CARD

@I FOR MAIN,MAIN

SOURCE DECK FOR MAIN PROGRAM

@I FOR INTZ,INTZ

SOURCE DECK FOR SUBPROGRAM INTZ

•

•

•

@I FOR LINEAR,LINEAR

SOURCE DECK FOR SUBPROGRAM LINEAR

@ MAP PROGRM

SEG MAIN-INTZ-LABEL-DUMPIT-KCOMMON-INTCOM-COSINE-VECTOR-ROTATE-  
ROTATC-RANNO-ZBS-ZQRT-ZXP-ZLOG-ZIN-ZOS-ZMIN1-ZMAX1-ZTAN2-CENTER-  
ROTATX-LOCATE-HELIX-SAMPLE-\* (DEFINE-\* (INDEX-ICHECK-JCHECK-KCHECK-\* (;  
READIT-READH-READA-READI-READII-READIS-READE-READEE-READIE-READES-;  
READS-READR-READF-READL-IARRAY-\* (ARRAY, INSECT-\* (MULTIX-MATRIX,  
GAMMAX,BASICX,SLOWER),SZERO,GEOMIN,RESULT-REXTRA,RANDOM),RLIMIT,  
RAPRAY),DOWN,REGION,ASKFOR,BIASIT),VOLTS-POTENT,ANSWER-LOOKC-  
QUICKP-\* (DEPOS,FLUXES,PLOTNE,DERIVE,TIMER,OPTIMA),SOURCE-SINPUT-  
CAPTUR-BREMSS-COMPTN-PHOTON-SCATTR-NEUTRN-BETAS-THERML-UNITRA-PATH-  
NORMAL-KERNEL-AHEAD-DETECT-DOSES-GROUP-SPHERE-PSTAR=QSTAR=USTAR-  
VSTAR-\* (TEMPER,SOLVER,SOBER-LINEAR))

@ XQT PROGRM

DATA DECK

TABLE E.5      PRECEDING PAGE BLANK NOT FILMED  
UNIVAC 1108, EXEC-8 CONTROL CARDS

@JOB-ACCOUNTING CARD  
@FREE TPFS  
@ASG,T TPFS,///2000  
@FOR,IS MAIN,MAIN  
    SOURCE DECK FOR MAIN PROGRAM  
@FOR,IS INTZ,INTZ  
    SOURCE DECK FOR SUBPROGRAM INTZ  
    •  
    •  
    •  
@FOR,IS LINEAR,LINEAR  
    SOURCE DECK FOR SUBPROGRAM LINEAR  
@MAP,I RUNIT  
SEG LINK00\*  
IN MAIN,INTZ,ZBS,ZQRT,ZXP,ZLOG,ZIN,ZOS,ZMIN1,ZMAX1,ZTAN2,LABEL,DUMPIT  
IN KOMMON,INTCOM,COSINE,VECTOR,ROTATE,ROTATC,CENTER,ROTATX,LOCATE,HELIX  
IN SAMPLE,RANNO,PLOTS,PLOT,NUMBER,SYMBOL  
SEG LINK01\*,(LINK00)  
IN DEFINE  
SEG LINK02\*,(LINK01)  
IN INDEX,ICHECK,JCHECK,KCHECK  
SEG LINK03\*,(LINK02)  
IN READIT,READH,READA,READI,READII,READIS,READE,READEE,READIE,READES  
IN READS,READR,READF,READL,IARRAY  
SEG LINK04\*,(LINK03)  
IN ARRAY  
SEG LINK05\*,(LINK03)  
IN INSECT  
SEG LINK06\*,(LINK05)  
IN MULTIX,MATRIX  
SEG LINK07\*,(LINK05)  
IN GAMMAX  
SEG LINK08\*,(LINK05)  
IN BASICX  
SEG LINK09\*,(LINK05)  
IN SLOWER  
SEG LINK10\*,(LINK03)  
IN SZERO  
SEG LINK11\*,(LINK03)  
IN GEOMIN  
SEG LINK12\*,(LINK03)  
IN RESULT,REXTA  
SEG LINK13\*,(LINK03)  
IN RANDOM  
SEG LINK14\*,(LINK02)  
IN RLIMIT  
SEG LINK15\*,(LINK02)  
IN RARRAY  
SEG LINK16\*,(LINK01)  
IN DOWN

TABLE E.5 (Cont'd)

SEG LINK17\*,(LINK01)  
IN REGION  
SEG LINK18\*,(LINK01)  
IN ASKFOR  
SEG LINK19\*,(LINK01)  
IN BIASIT  
SEG LINK20\*,(LINK00)  
IN VOLTS,POTENT  
SEG LINK21\*,(LINK00)  
IN ANSWER,LOOKC,QUICKP  
SEG LINK22\*,(LINK21)  
IN DEPOS  
SEG LINK23\*,(LINK21)  
IN FLUXES  
SEG LINK24\*,(LINK21)  
IN PLOTNE  
SEG LINK25\*,(LINK21)  
IN DERIVE  
SEG LINK26\*,(LINK21)  
IN TIMER  
SEG LINK27\*,(LINK21)  
IN OPTIMA  
SEG LINK28\*,(LINK00)  
IN SOURCE,SINPUT,CAPTUR,BREMSS,COMPTN,PHOTON,SCATTR,NEUTRN,BETAS,THERML  
IN UNITRA,PATH,NORMAL,KERNEL,AHEAD,DETECT,DOSES,GROUP,SPHERE,PSTAR  
IN QSTAR,USTAR,VSTAR  
SEG LINK29\*,(LINK28)  
IN TEMPER  
SEG LINK30\*,(LINK28)  
IN SOLVER  
SEG LINK31\*,(LINK28)  
IN SOBER,LINEAR  
BXQT

DATA DECK

TABLE E.6

CDC 6600 SCOPE CONTROL CARDS

JOB-ACCOUNTING CARD

FASTER,PRIORITY,TIME LIMIT,FIELD LENGTH. FORMAT VARIES  
RUN(S,,,,,,777777,1) ASA OPTION  
LGO.

7 (END OF RECORD)

8 PROGRAM FASTER(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)  
SOURCE DECK FOR THE MAIN PROGRAM  
SOURCE DECKS FOR ALL SUBPROGRAMS

9 (END OF RECORD)

10 DATA DECKS

11 (END OF FILE)